

## SECTION 2 STRUCTURE AND FUNCTION

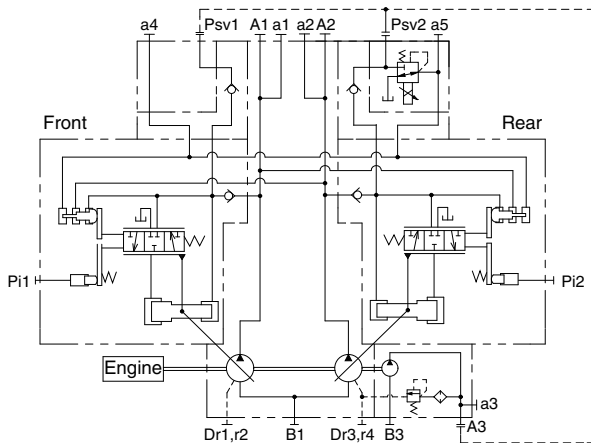
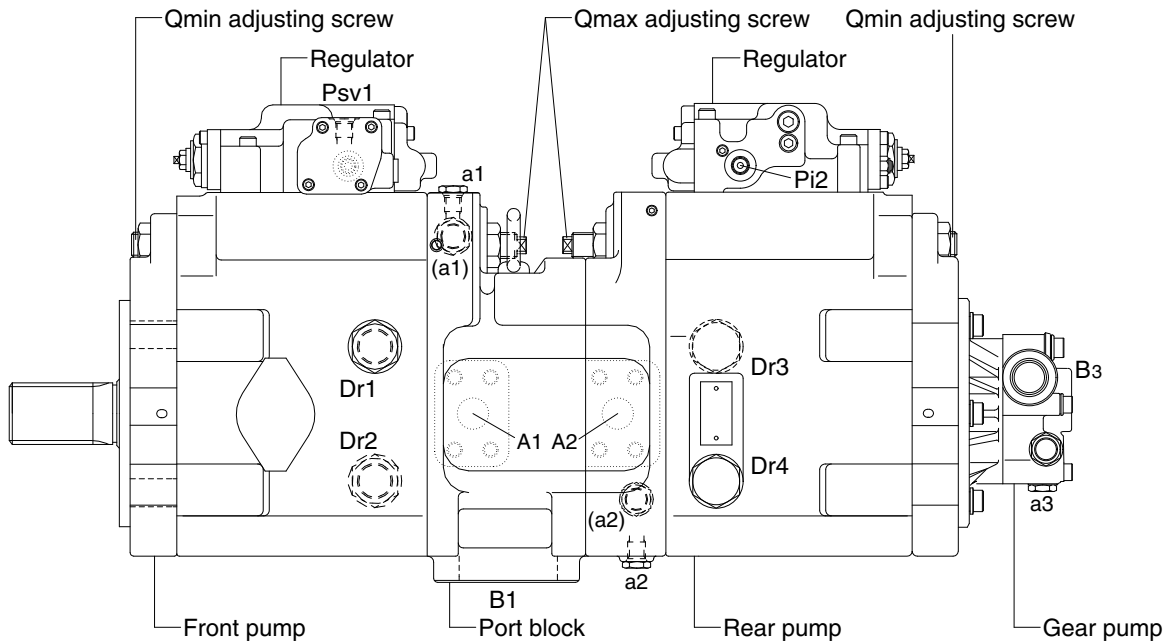
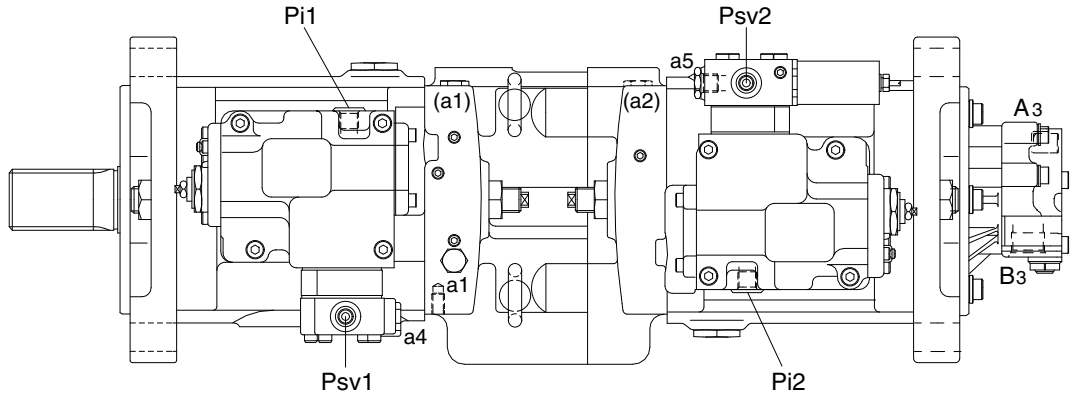
Group 1 Pump Device .....	2-1
Group 2 Main Control Valve .....	2-22
Group 3 Swing Device .....	2-56
Group 4 Travel Device .....	2-70
Group 5 RCV Lever .....	2-83
Group 6 RCV Pedal .....	2-90

# SECTION 2 STRUCTURE AND FUNCTION

## GROUP 1 PUMP DEVICE

### 1. STRUCTURE

The pump device consists of main pump, regulator and gear pump.



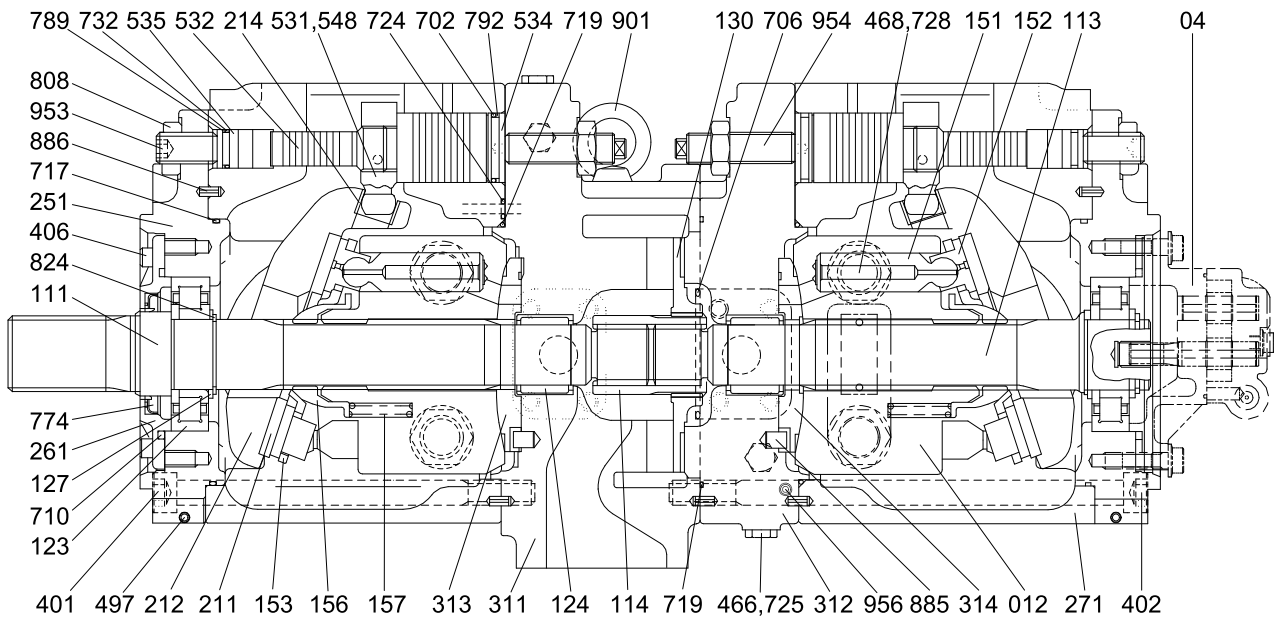
Hydraulic circuit

400SA2MP01

Port	Port name	Port size
A1, 2	Delivery port	SAE 6000 psi 1"
B1	Suction port	SAE 2500 psi 3"
Dr	Drain port	PF 3/4 - 23
Pi1, i2	Pilot port	PF 1/4 - 15
Psv1, sv2	Servo assist port	PF 1/4 - 15
a1, 2, 4, 5	Gauge port	PF 1/4 - 15
a3	Gauge port	PF 1/4 - 14
A3	Gear pump delivery port	PF 1/2 - 19
B3	Gear pump suction port	PF 3/4 - 20.5

## 1) MAIN PUMP (1/2)

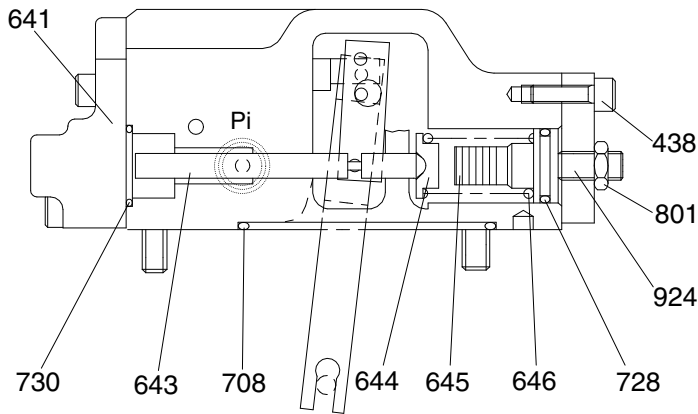
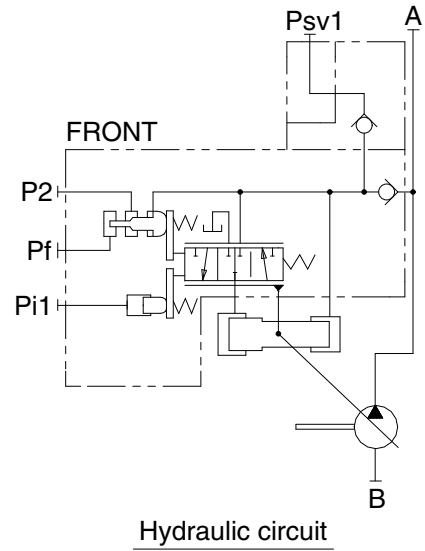
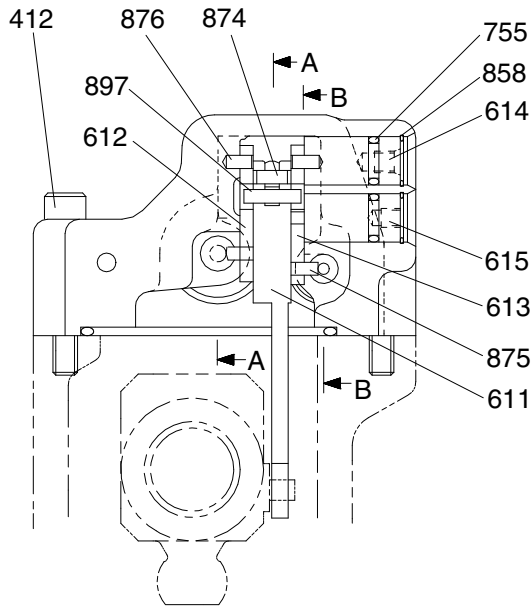
The main pump consists of two piston pumps (front & rear) and valve cover.



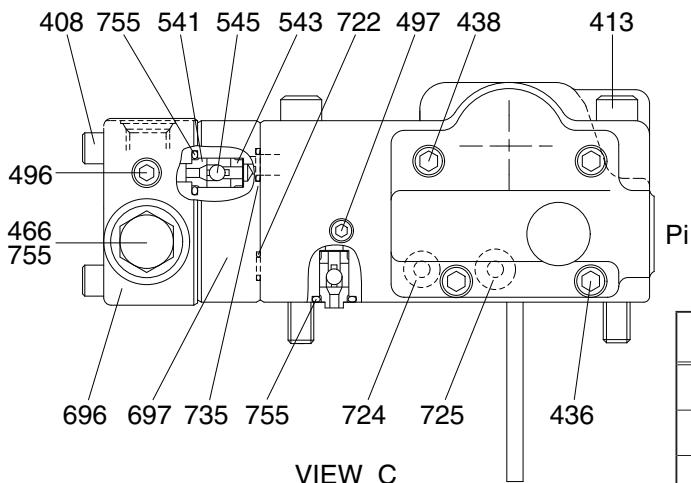
400SA2MP02

04	Gear pump	271	Pump casing	717	O-ring
111	Drive shaft (F)	311	Valve cover (F)	719	O-ring
113	Drive shaft (R)	312	Valve cover (R)	724	Square ring
114	Spline coupling	313	Valve plate (R)	725	O-ring
123	Roller bearing	314	Valve plate (L)	728	O-ring
124	Needle bearing	401	Hexagon socket bolt	732	O-ring
127	Bearing spacer	402	Hexagon socket bolt	774	Oil seal
130	Booster	406	Hexagon socket bolt	789	Back up ring
012	Cylinder block	466	Plug	792	Back up ring
151	Piston	468	Plug	808	Hexagon head nut
152	Shoe	497	MH Plug	824	Snap ring
153	Set plate	531	Tilting pin	885	Pin
156	Bushing	532	Servo piston	886	Spring pin
157	Cylinder spring	534	Stopper (L)	901	Eye bolt
211	Shoe plate	535	Stopper (S)	953	Set screw
212	Swash plate	548	Feedback pin	954	Set screw
214	Bushing	702	O-ring	956	Set screw
251	Support plate	706	O-ring		
261	Seal cover (F)	710	O-ring		

## 2) FRONT REGULATOR (1/2)



SECTION B-B

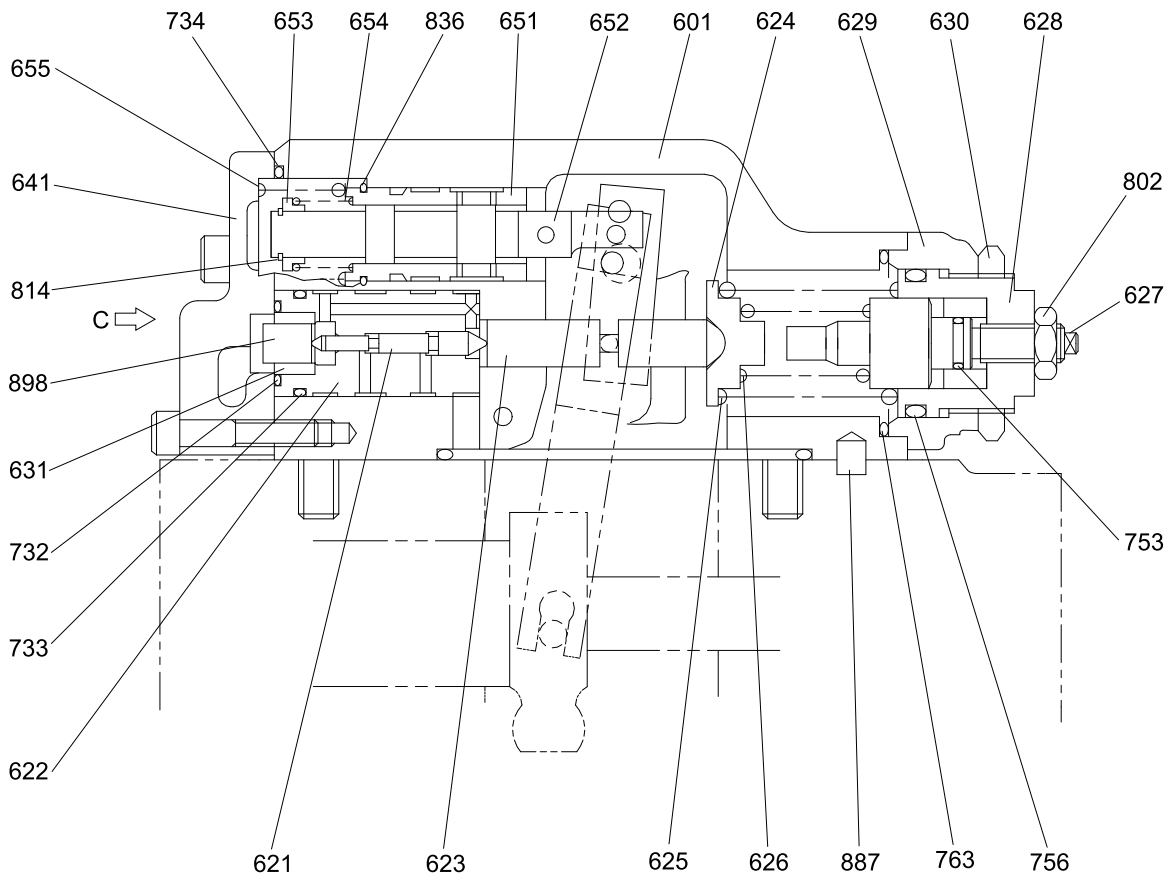


VIEW C

Port	Port name	Port size
Pi1	Pilot port	PF 1/4-15
Psv1	Servo assist port	PF 1/4-15
Pf	Power shift port	-
P2	Companion delivery port	-

400SA2RG01

## FRONT REGULATOR (2/2)

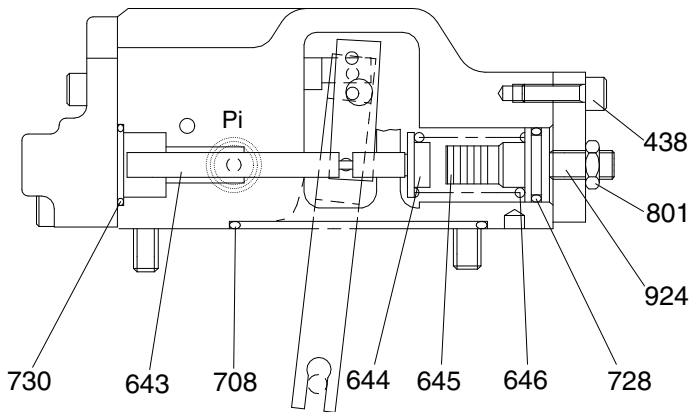
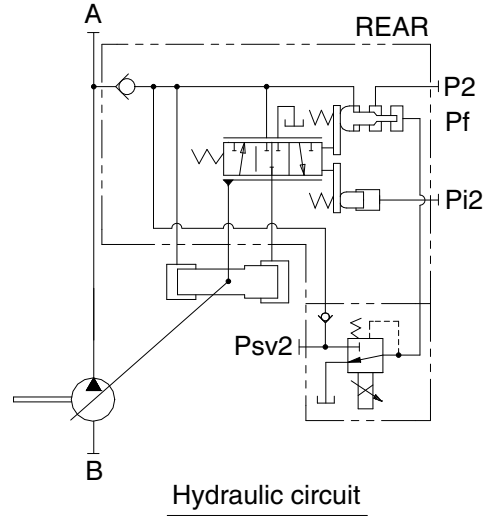
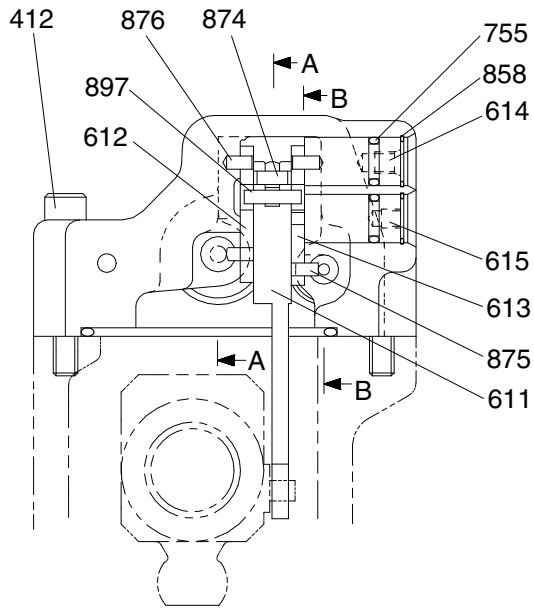


SECTION A-A

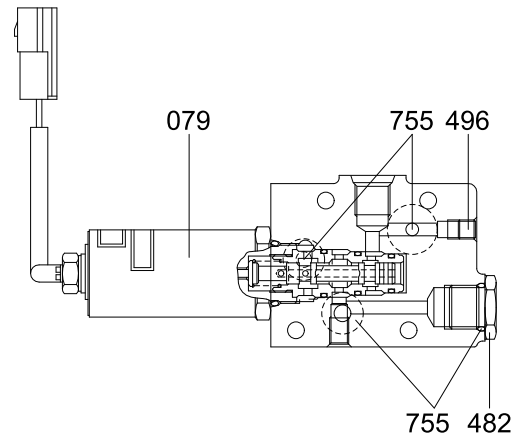
400SA2RG03

408 Hexagon socket bolt	626 Inner spring	728 O-ring
412 Hexagon socket bolt	627 Adjust stem (C)	730 O-ring
413 Hexagon socket bolt	628 Adjust screw (C)	732 O-ring
436 Hexagon socket bolt	629 Cover (C)	733 O-ring
438 Hexagon socket bolt	630 Lock nut	734 O-ring
466 Plug	631 Sleeve, pf	735 O-ring
496 Plug	641 Pilot cover	753 O-ring
497 Plug	643 Pilot piston	755 O-ring
541 Seat	644 Spring seat (Q)	756 O-ring
543 Stopper	645 Adjust stem (Q)	763 O-ring
545 Steel ball	646 Pilot spring	801 Hexagon nut
601 Casing	651 Sleeve	802 Hexagon nut
611 Feedback lever	652 Spool	814 Snap ring
612 Lever(1)	653 Spring seat	836 Stop ring
613 Lever(2)	654 Return spring	858 Snap ring
614 Center plug	655 Set spring	874 Pin
615 Adjust plug	696 Port cover	875 Pin
621 Compensator piston	697 Check valve plate	876 Pin
622 Piston case	708 O-ring	887 Pin
623 Compensator rod	722 O-ring	897 Pin
624 Spring seat (C)	724 Square ring	898 Pin
625 Outer spring	725 O-ring	924 Set screw

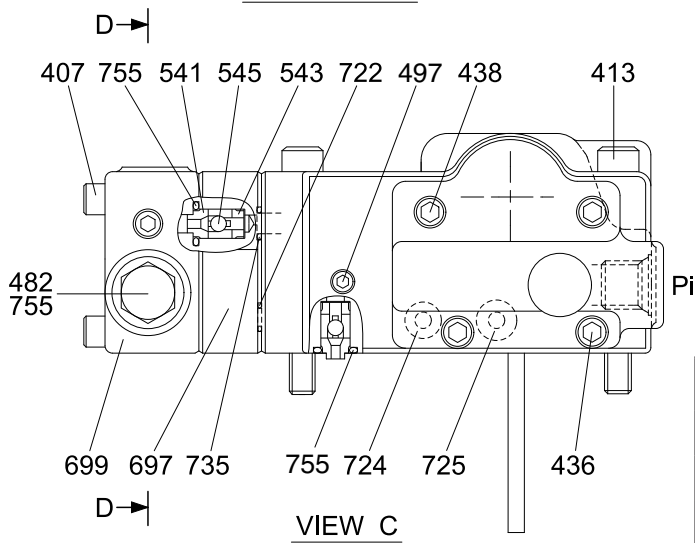
### 3) REAR REGULATOR (1/2)



**SECTION B-B**



**SECTION D-D**

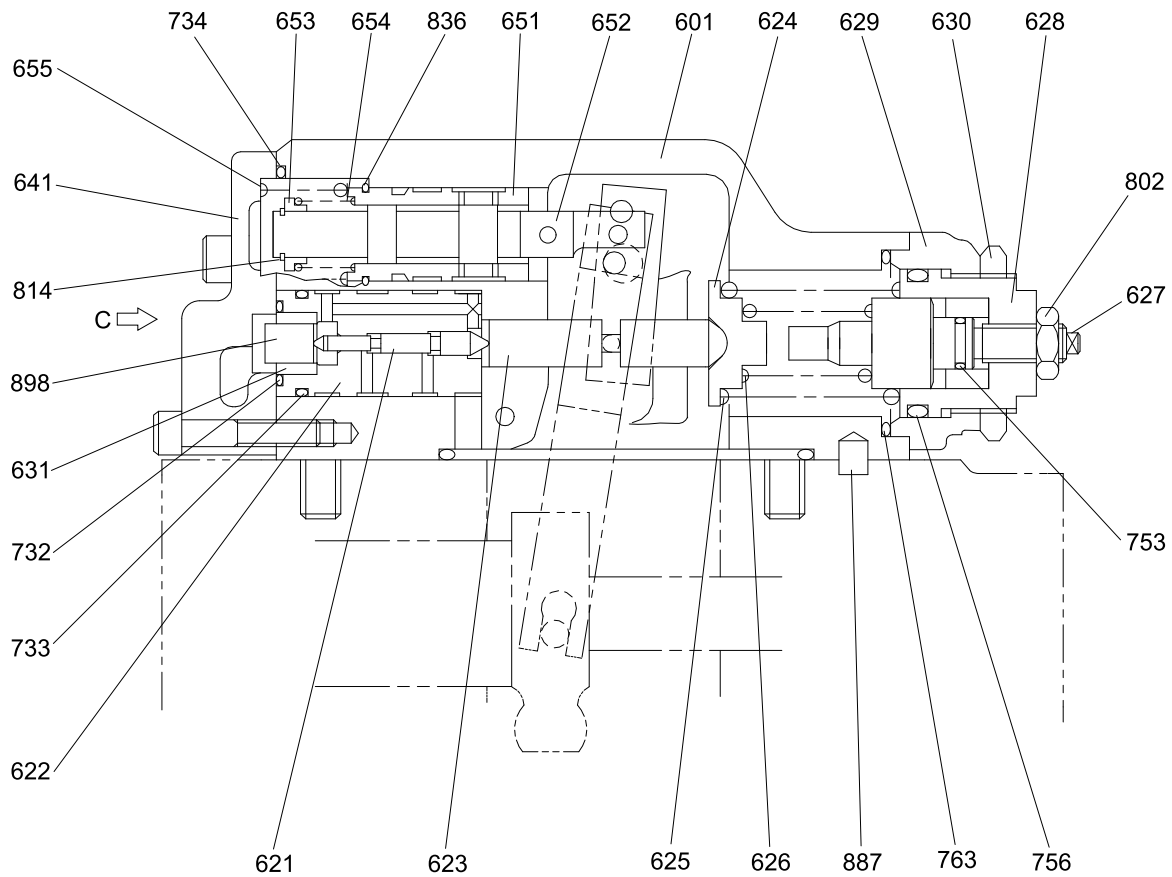


**VIEW C**

Port	Port name	Port size
Pi1	Pilot port	PF 1/4-15
Psv1	Servo assist port	PF 1/4-15
Pf	Power shift port	-
P2	Companion delivery port	-

400SA2RG02

## REAR REGULATOR (2/2)

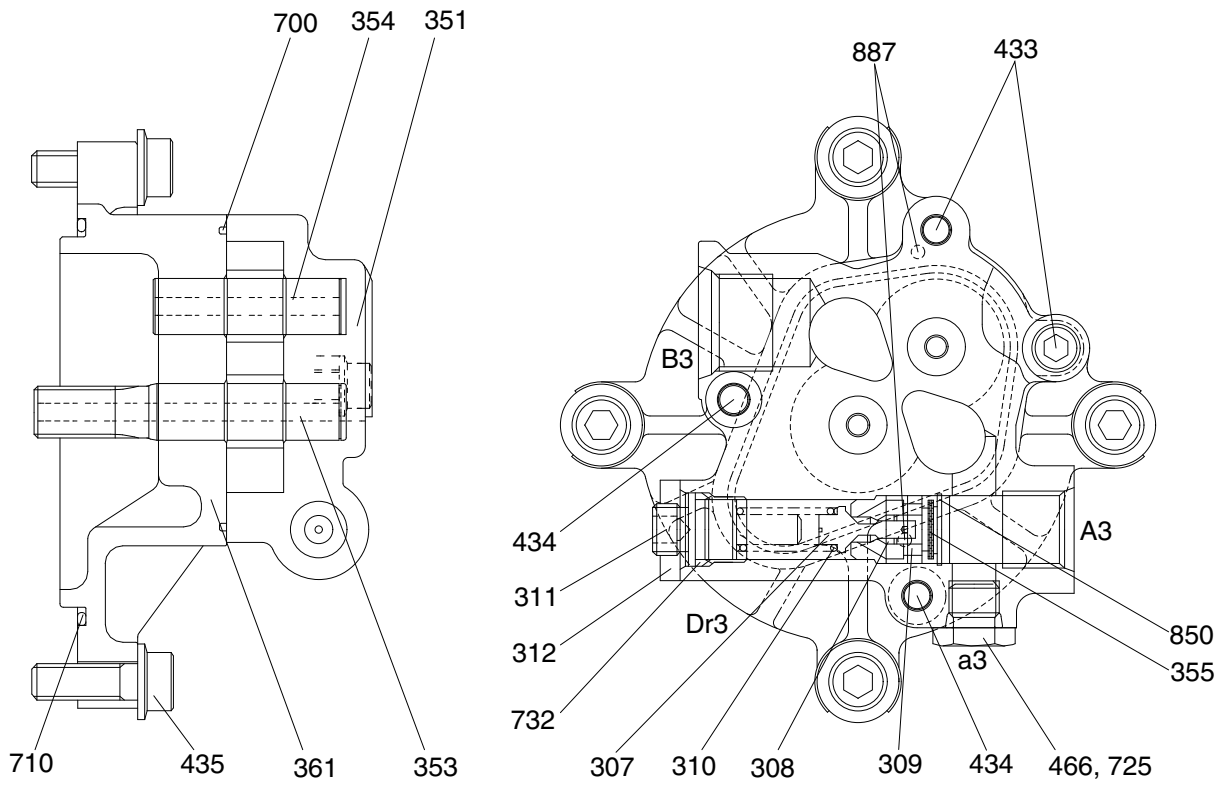


SECTION A-A

400SA2RG03

407 Hexagon socket bolt	626 Inner spring	728 O-ring
412 Hexagon socket bolt	627 Adjust stem (C)	730 O-ring
413 Hexagon socket bolt	628 Adjust screw (C)	732 O-ring
436 Hexagon socket bolt	629 Cover (C)	733 O-ring
438 Hexagon socket bolt	630 Lock nut	734 O-ring
482 Plug	631 Sleeve, pf	735 O-ring
496 Plug	641 Pilot cover	753 O-ring
497 Plug	643 Pilot piston	755 O-ring
541 Seat	644 Spring seat (Q)	756 O-ring
543 Stopper	645 Adjust stem (Q)	763 O-ring
545 Steel ball	646 Pilot spring	801 Hexagon nut
601 Casing	651 Sleeve	802 Hexagon nut
611 Feedback lever	652 Spool	814 Snap ring
612 Lever(1)	653 Spring seat	836 Stop ring
613 Lever(2)	654 Return spring	858 Snap ring
614 Center plug	655 Set spring	874 Pin
615 Adjust plug	697 Check valve plate	875 Pin
621 Compensator piston	699 Valve casing	876 Pin
622 Piston case	708 O-ring	887 Pin
623 Compensator rod	722 O-ring	897 Pin
624 Spring seat (C)	724 Square ring	898 Pin
625 Outer spring	725 O-ring	924 Set screw

#### 4) GEAR PUMP



400SA2MP05

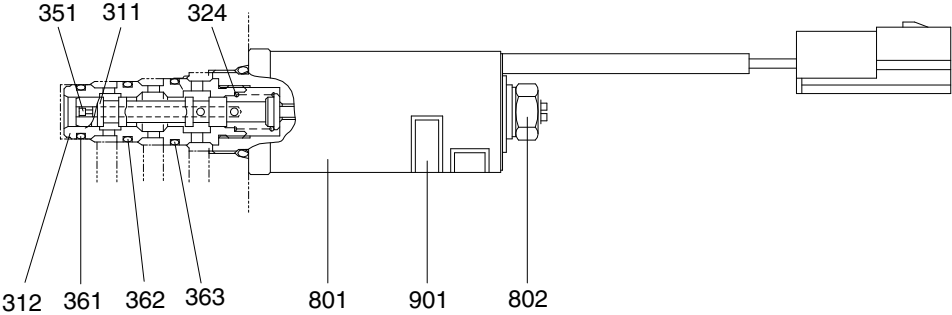
- 307 Poppet
- 308 Seat
- 309 Ring
- 310 Spring
- 311 Screw
- 312 Nut
- 351 Gear case

- 353 Drive gear
- 354 Driven gear
- 355 Filter
- 361 Front case
- 433 Flange socket
- 434 Flange socket
- 435 Flange socket

- 466 Plug
- 700 Ring
- 710 O-ring
- 725 O-ring
- 732 O-ring
- 850 Snap ring
- 887 Pin



5) EPPR VALVE ASSY



400SA2MP08

- |             |              |                 |
|-------------|--------------|-----------------|
| 311 Spool   | 361 O-ring   | 802 Hexagon nut |
| 312 Sleeve  | 362 O-ring   | 901 Name plate  |
| 324 Spring  | 363 O-ring   |                 |
| 351 Orifice | 801 Solenoid |                 |

## 2. FUNCTION

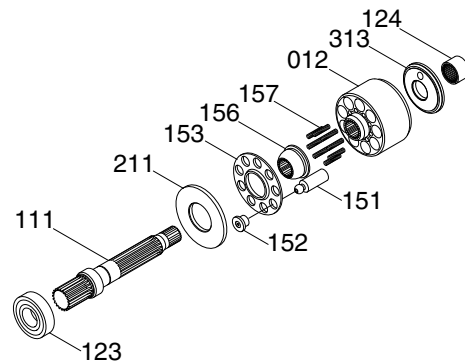
### 1) MAIN PUMP

The pumps may be classified roughly into the rotary group performing a rotary motion and working as the major part of the whole pump function: the swash plate group that varies the delivery rates: and the valve cover group that changes over oil suction and discharge.

#### (1) Rotary group

The rotary group consists of drive shaft (F)(111), cylinder block (012), piston shoes (151,152), set plate (153), spherical bush (156) and cylinder spring (157). The drive shaft is supported by bearing (123,124) at its both ends.

The shoe is caulked to the piston to form a spherical coupling. It has a pocket to relieve thrust force generated by loading pressure and to take hydraulic balance so that it slides lightly over the shoe plate (211). The sub group composed by a piston and a shoe is pressed against the shoe plate by the action of the cylinder spring via a retainer and a spherical bush. Similarly, the cylinder block is pressed against valve plate (313) by the action of the cylinder spring.



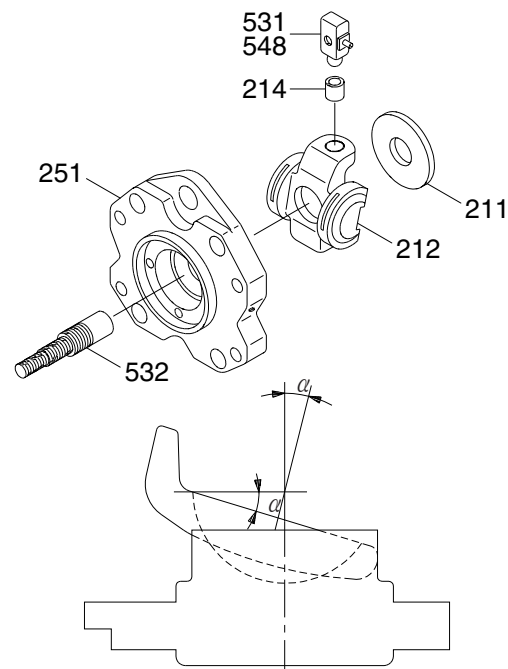
32092MP03

#### (2) Swash plate group

The swash plate group consists of swash plate (212), shoe plate (211), swash plate support (251), tilting bush (214), tilting pin (531) and servo piston (532).

The swash plate is a cylindrical part formed on the opposite side of the sliding surface of the shoe and is supported by the swash support.

If the servo piston moves to the right and left as hydraulic force controlled by the regulator is admitted to hydraulic chamber located on both sides of the servo piston, the swash plate slides over the swash plate support via the spherical part of the tilting pin to change the tilting angle ( $\alpha$ )



3607A2MP10

### (3) Valve block group

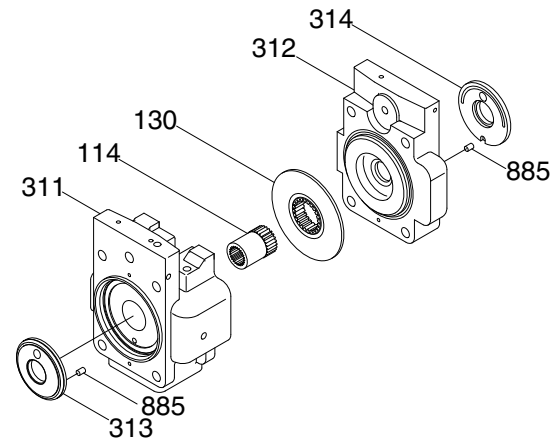
The valve block group consists of valve cover (F, 311), valve cover (F, 312), valve plate (313, 314), spline coupling (114), booster (130) and valve plate pin (885).

The valve plate having two melon-shaped ports is fixed to the valve block and feeds and collects oil to and from the cylinder block.

The oil changed over by the valve plate is connected to an external pipeline by way of the valve block.

Now, if the drive shaft is driven by a prime mover (electric motor, engine, etc), it rotates the cylinder block via a spline linkage at the same time. If the swash plate is tilted as in Fig (previous page) the pistons arranged in the cylinder block make a reciprocating motion with respect to the cylinder block, while they revolve with the cylinder block.

If you pay attention to a single piston, it performs a motion away from the valve plate (oil sucking process) within 180 degrees, and makes a motion towards the valve plate (or oil discharging process) in the rest of 180 degrees. When the swash plate has a tilting angle of zero, the piston makes no stroke and discharges no oil.



38092MP04

## 2) REGULATOR

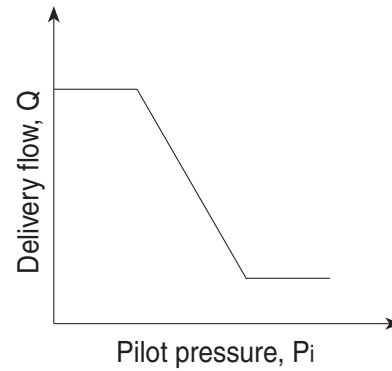
Regulator consists of the negative flow control, total horse power control and power shift control function.

### (1) Negative flow control

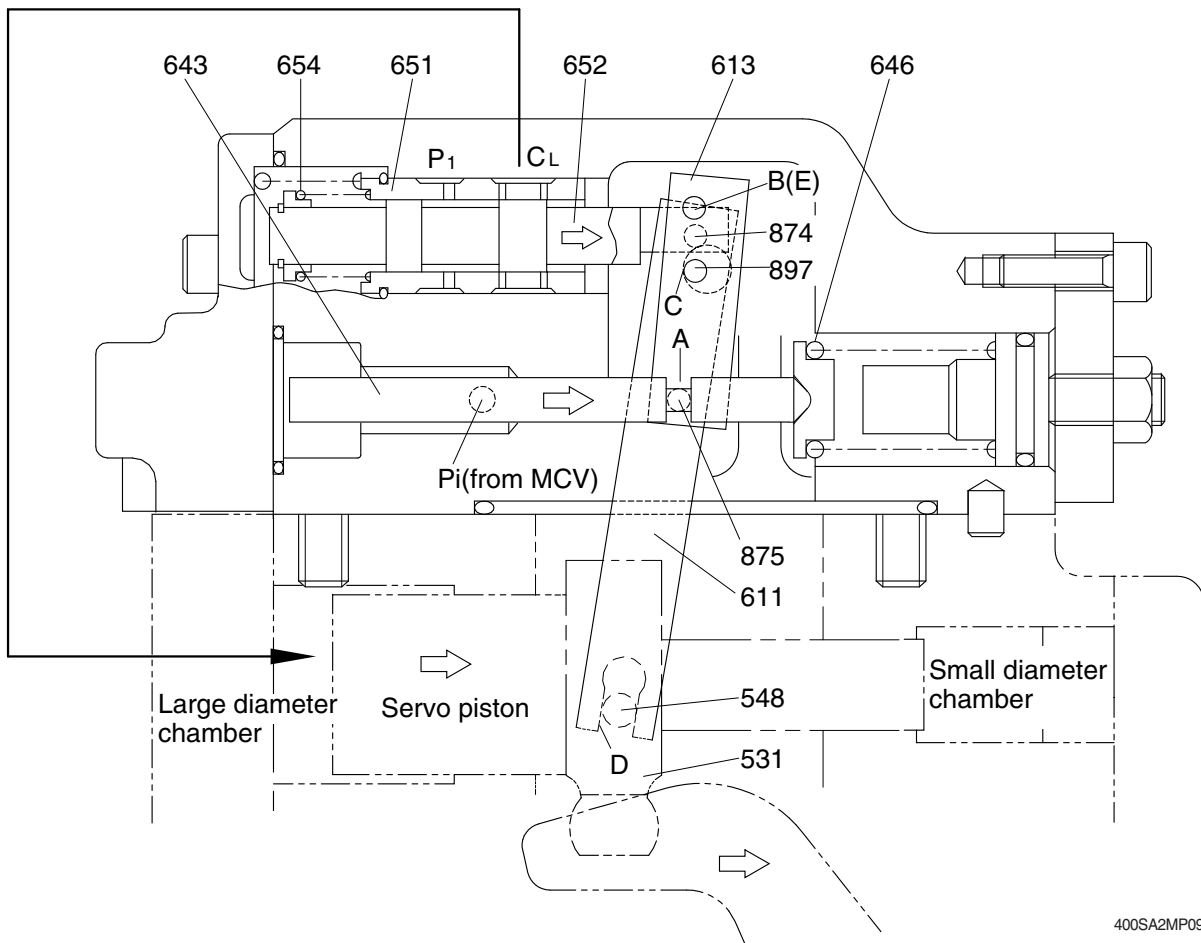
By changing the pilot pressure  $P_i$ , the pump tilting angle (delivery flow) is regulated arbitrarily, as shown in the figure.

This regulator is of the negative flow control in which the delivery flow  $Q$  decreases as the pilot pressure  $P_i$  rises.

With this mechanism, when the pilot pressure corresponding to the flow required for the work is commanded, the pump discharges the required flow only, and so it does not consume the power uselessly.



## ① Flow reducing function



400SA2MP09

As the pilot pressure  $P_i$  rises, the pilot piston (643) moves to the right to a position where the force of the pilot spring (646) balances with the hydraulic force.

The groove (A) in the pilot piston is fitted with the pin (875) that is fixed to lever 2 (613). Therefore, when the pilot piston moves, lever 2 rotates around the fulcrum of point B [Fixed by the fulcrum plug (614) and pin (875)]. Since the large hole section (C) of lever 2 contains a protruding pin (897) fixed to the feedback lever (611), the pin (897) moves to the right as lever 2 rotates. Since the opposing-flat section (D) of the feedback lever is fitted with the pin (548) fixed by the tilting pin (531) that swings the swash plate, the feedback lever rotates around the fulcrum of point D, as the pin (897) moves.

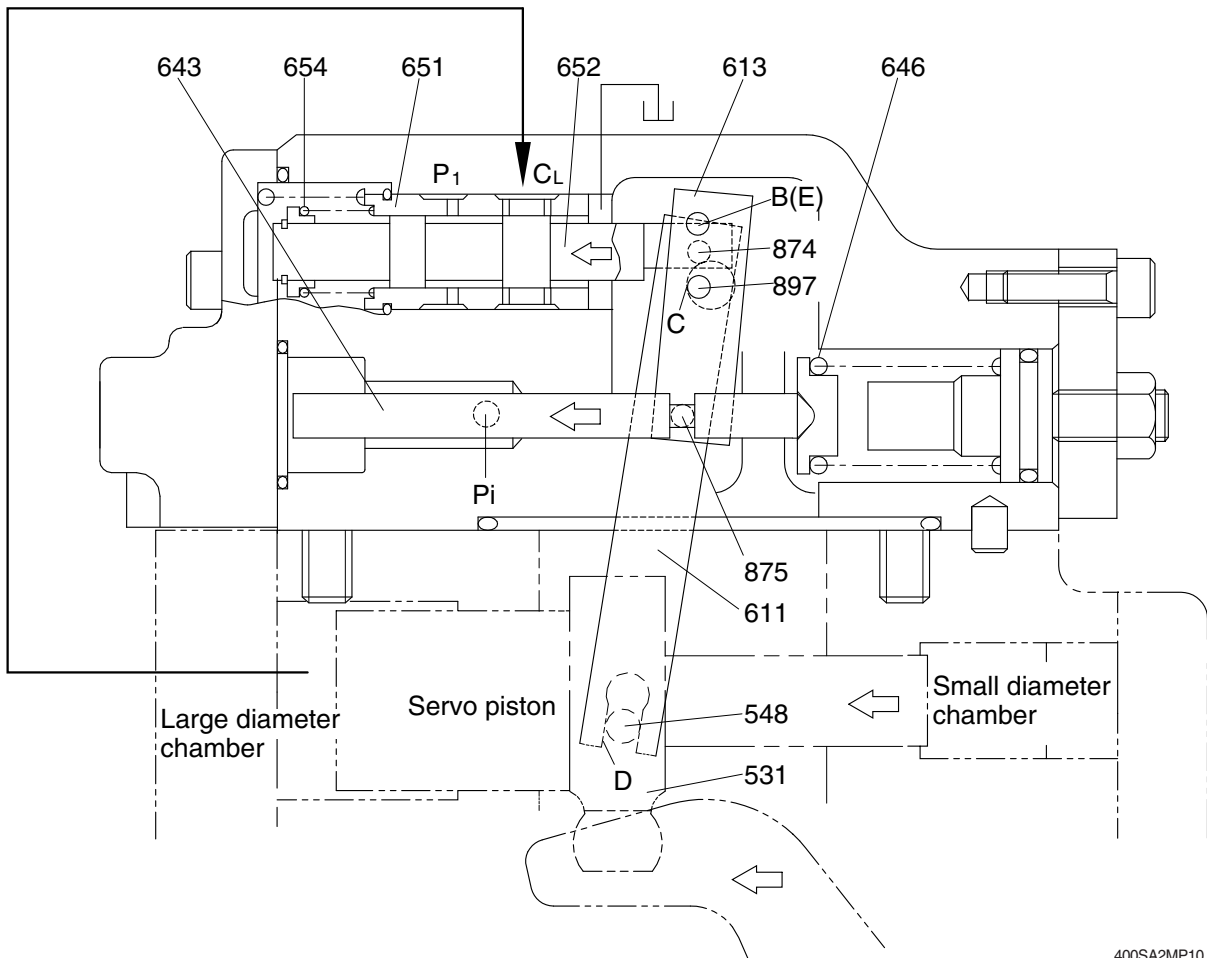
Since the feedback lever is connected with the spool (652) via the pin (874), the spool moves to the right.

The movement of the spool causes the delivery pressure  $P_1$  to connect to port CL through the spool and to be admitted to the large diameter section of the servo piston. The delivery pressure  $P_1$  that is constantly admitted to the small diameter section of the servo piston moves the servo piston to the right due to the area difference, resulting in decrease of the tilting angle.

When the servo piston moves to the right, point D also moves to the right. The spool is fitted with the return spring (654) and is tensioned to the left at all times, and so the pin (897) is pressed against the large hole section (C) of lever 2.

Therefore, as point D moves, the feedback lever rotates around the fulcrum of point C, and the spool is shifted to the left. This causes the opening between the sleeve (651) and spool (652) to close slowly, and the servo piston comes to a complete stop when it closes completely.

## ② Flow increasing function



As the pilot pressure  $P_i$  decreases, the pilot piston (643) moves to the left by the action of the pilot spring (646) and causes lever 2 (613) to rotate around the fulcrum of point B. Since the pin (897) is pressed against the large hole section (C) of lever 2 by the action of the return spring (654) via the spool (652), pin (874), and feedback lever (611), the feedback lever rotates around the fulcrum of point D as lever 2 rotates, and shifts the spool to the left. Port CL opens a way to the tank port as the spool moves. This deprives the large diameter section of the servo piston of pressure, and shifts the servo piston to the left by the discharge pressure  $P_1$  in the small diameter section, resulting in an increase in the flow rate.

As the servo piston moves, point D also moves to the left, the feedback lever rotates around the fulcrum of point C, and the spool moves to the right till the opening between the spool and sleeve is closed.

### ③ Adjustment of flow control characteristic

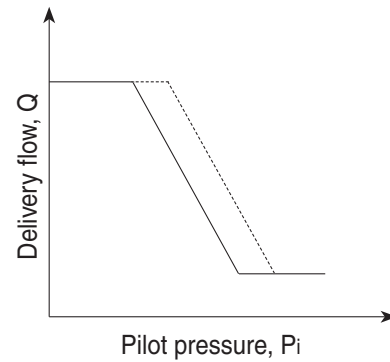
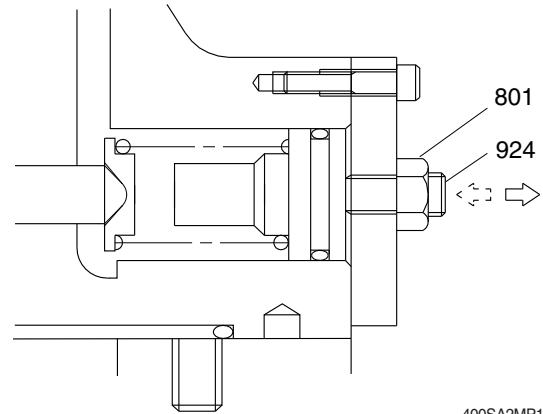
The flow control characteristic can be adjusted with the adjusting screw.

Adjust it by loosening the hexagon nut (801) and by tightening (or loosening) the hexagonal socket head screw (924).

Tightening the screw shifts the control chart to the right as shown in the figure.

※ Adjusting values are shown in table.

Speed (min <sup>-1</sup> )	Adjustment of flow control characteristic		
	Tightening amount of adjusting screw (924) (Turn)	Flow control starting pressure change amount (kgf/cm <sup>2</sup> )	Flow change amount (l/min)
1800	+1/4	+1.0	+18.9



## (2) Total horsepower control

The regulator decreases the pump tilting angle (delivery flow) automatically to limit the input torque within a certain value with a rise in the delivery pressure P1 of the self pump and the delivery pressure P2 of the companion pump.

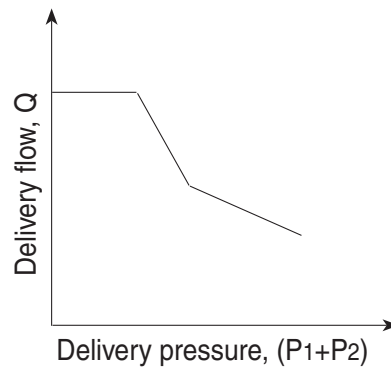
(The input horsepower is constant when the speed is constant.)

Since the regulator is of the simultaneous total horsepower type that operates by the sum of load pressures of the two pumps in the tandem double-pump system, the prime mover is automatically prevented from being overloaded, irrespective of the load condition of the two pumps, when horsepower control is under way.

Since this regulator is of the simultaneous total horsepower type, it controls the tilting angles (displacement volumes) of the two pumps to the same value as represented by the following equation :

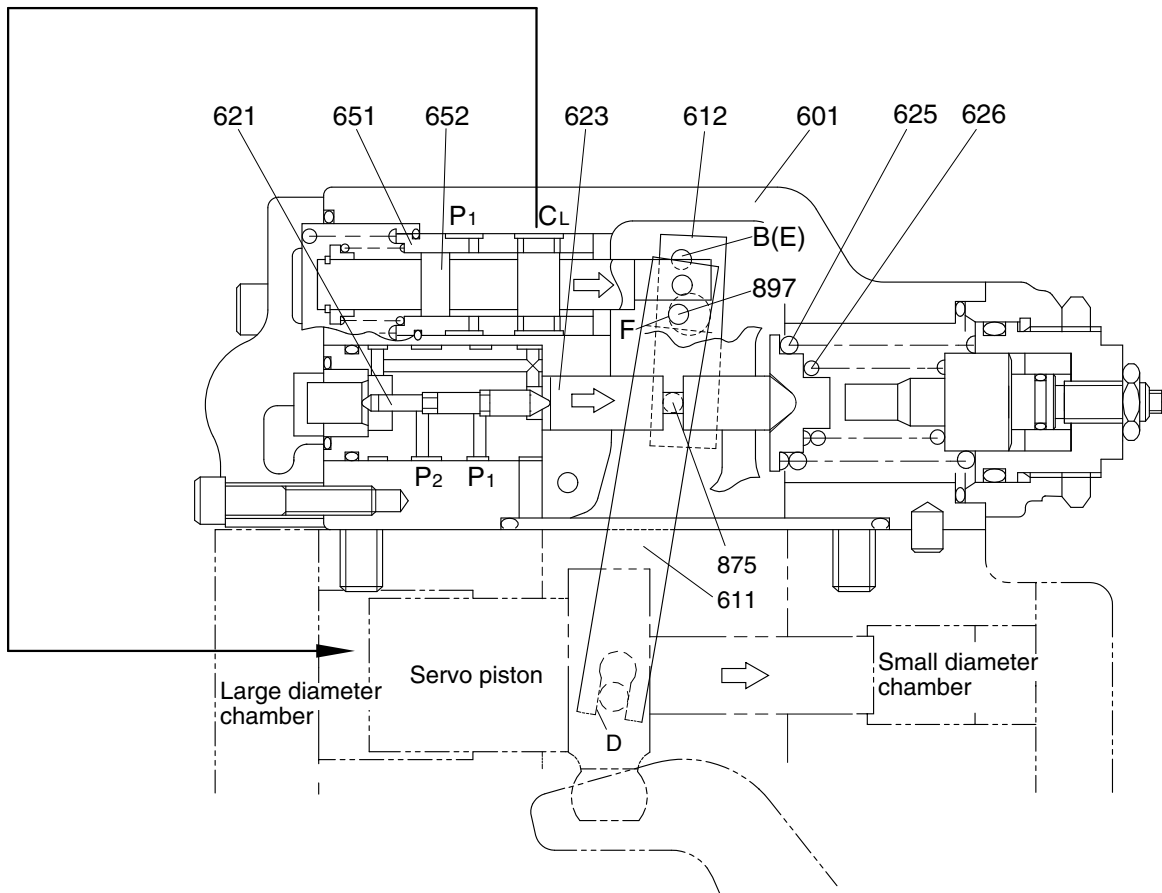
$$\begin{aligned} T_{in} &= P1 \times q / 2 \pi + P2 \times q / 2 \pi \\ &= (P1+P2) \times q / 2 \pi \end{aligned}$$

The horsepower control function is the same as the flow control function and is summarized in the following. (for detailed behaviors of respective parts, refer to the section of flow control).





## ① Overload preventive function

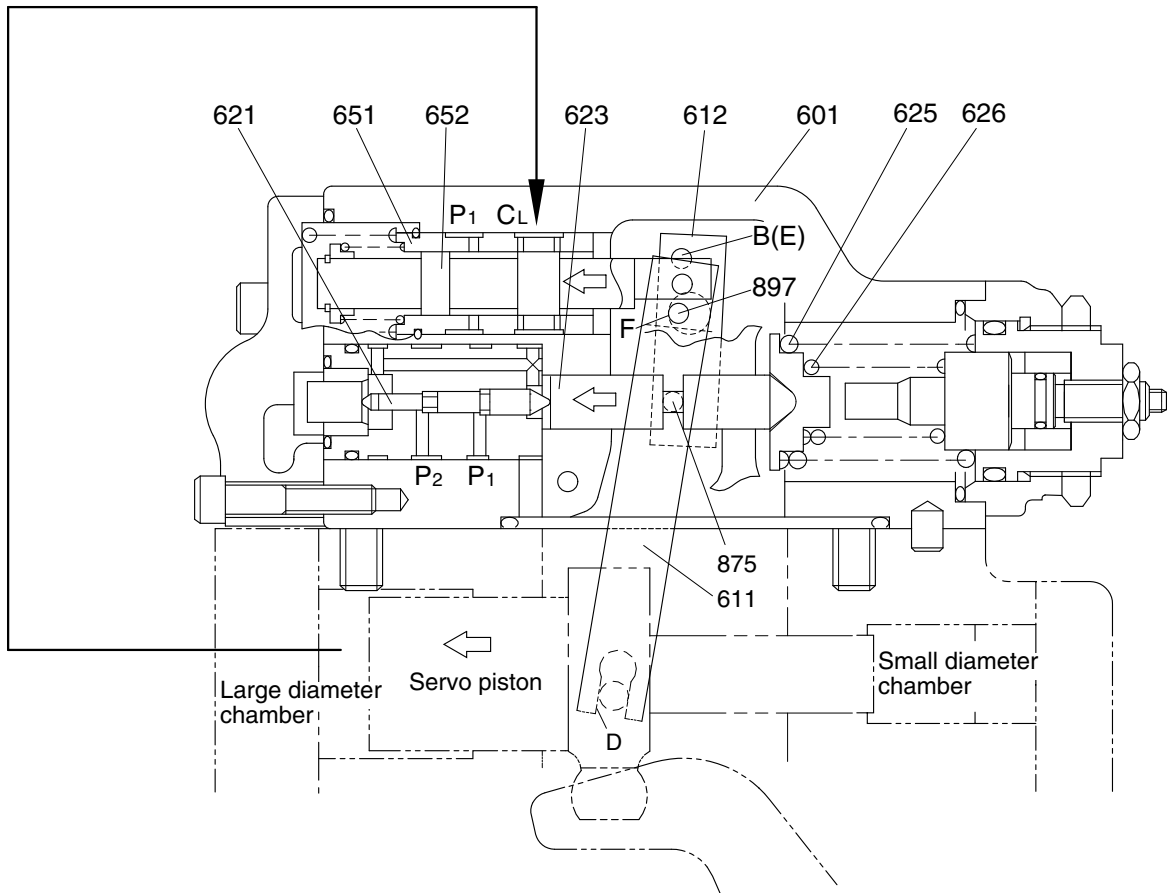


400SA2MP12

When the self pump delivery pressure  $P_1$  or the companion pump delivery pressure  $P_2$  rises, it acts on the stepped part of the compensating piston (621). It presses the compensating rod (623) to the right till the force of the outer spring (625) and inner spring (626) balances with the hydraulic force. The movement of the compensating rod is transmitted to lever 1 via pin (875). Lever 1 rotates around the pin (875) (E) fixed to the casing (601).

Since the large hole section (F) of lever 1 contains a protruding pin (897) fixed to the feedback lever (611), the feedback lever rotates around the fulcrum of point D as lever 1 rotates, and then the spool (652) is shifted to the right. As the spool moves, the delivery pressure  $P_1$  is admitted to the large diameter section of the servo piston via port CL, causes the servo piston move to the right, reduces the pump delivery flow rate, and prevents the prime mover from being overloaded. The movement of the servo piston is transmitted to the feedback lever via point D. Then the feedback lever rotates around the fulcrum of point F and the spool is shifted to the left. The spool moves till the opening between the spool (652) and sleeve (651) is closed.

## ② Flow reset function



400SA2MP13

As the self pump delivery pressure  $P_1$  or the companion pump delivery pressure  $P_2$  decreases, the compensating rod (623) is pushed back by the action of the springs (625 & 626) to rotate lever 1 (612) around point E. Rotating of lever 1 (612) causes the feedback lever (611) to rotate around the fulcrum of point D and then the spool (652) to move to the left. As a result, port CL opens a way to the tank port.

This causes the servo piston to move to the left and the pump's delivery rate to increase.

The movement of the servo piston is transmitted to the spool by the action of the feedback mechanism to move it till the opening between the spool and sleeve is closed.

③ **Low tilting angle (low flow) command preferential function**

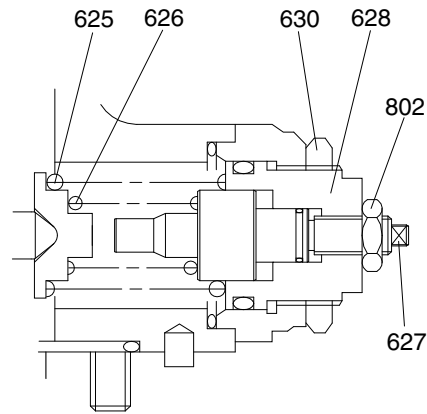
As mentioned above, flow control and horsepower control tilting angle commands are transmitted to the feedback lever and spool via the large-hole sections (C & F) of levers 1 and 2. However, since sections C and F have the pins (∅4) protruding from the large hole (∅8), only the lever lessening the tilting angle contacts the pin (897); the hole (∅8) in the lever of a larger tilting angle command is freed without contacting the pin (897). Such a mechanical selection method permits preference of the lower tilting angle command of the flow control and horsepower control.

④ **Adjustment of input horsepower**

Since the regulator is of total cumulative horsepower type, adjust the adjusting screws of both the front and rear pumps, when changing the horsepower set values. The pressure change values by adjustment are based on two pumps pressurized at the same time, and the values will be doubled when only one pump is loaded.

a. **Adjustment of outer spring**

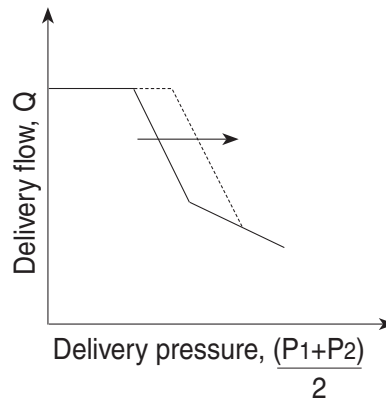
Adjust it by loosening the hexagon nut (630) and by tightening (or loosening) the adjusting screw C (628). Tightening the screw shifts the control chart to the right and increases the input horsepower as shown in the figure. Since turning the adjusting screw C by N turns changes the setting of the inner spring (626), return the adjusting screw QI (627) by  $N \times A$  turns at first. ( $A=1.48$ )



※ **Adjusting values are shown in table.**

Speed	Adjustment of outer spring		
	Tightening amount of adjusting screw (C) (628)	Compensating control starting pressure change amount	Input torque change amount
(min <sup>-1</sup> )	(Turn)	(kgf/cm <sup>2</sup> )	(kgf · m)
1800	+1/4	+15.9	+6.6

400SA2MP14



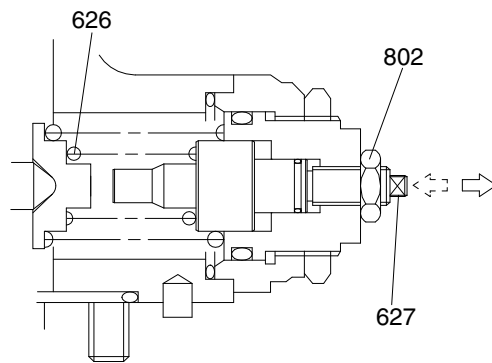
**b. Adjustment of inner spring**

Adjust it by loosening the hexagon nut (802) and by tightening (or loosening) the adjusting screw QI (627).

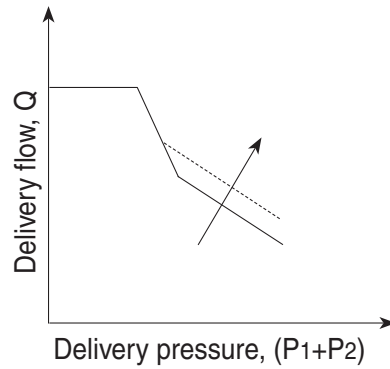
Tightening the screw increases the flow and then the input horsepower as shown in the figure.

※ Adjusting valves are shown in table.

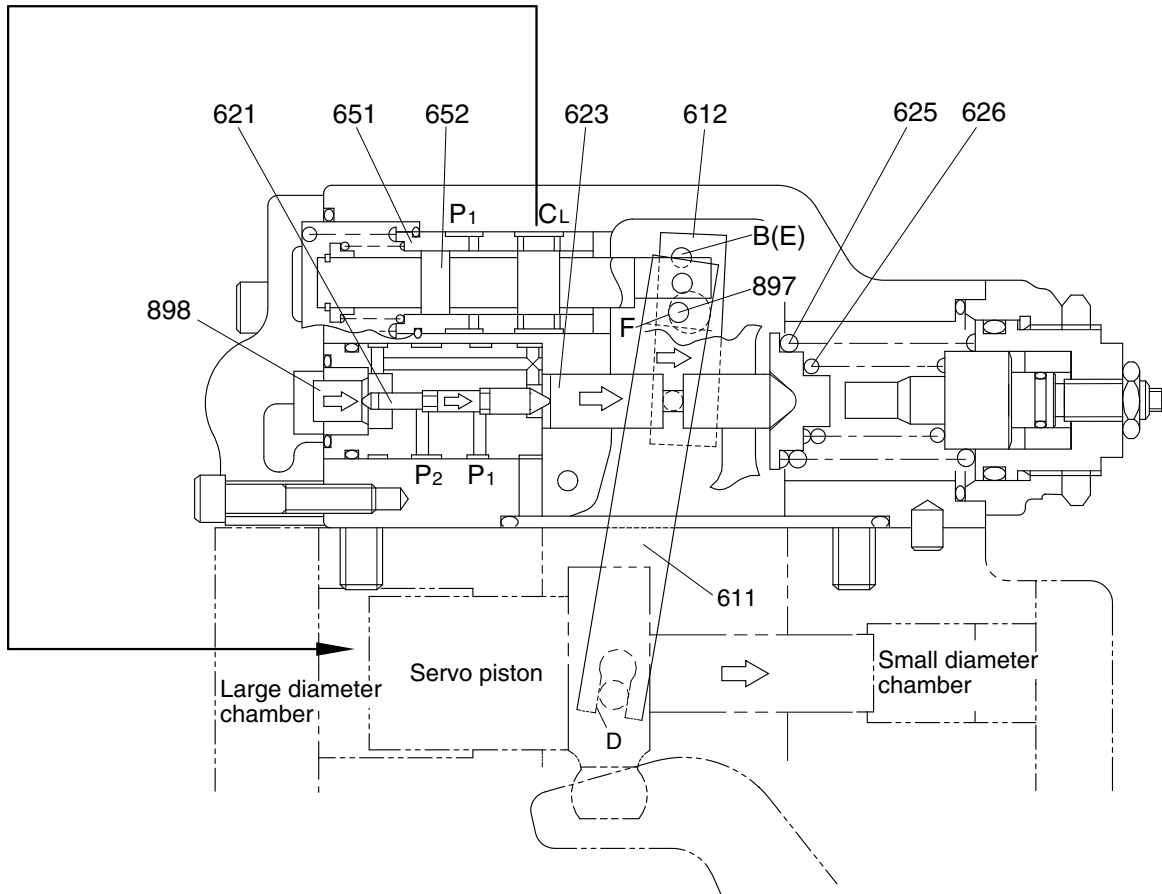
Speed	Adjustment of inner spring		
	Tightening amount of adjusting screw (QI) (627)	Flow change amount	Input torque change amount
(min <sup>-1</sup> )	(Turn)	(lpm)	(kgf · m)
1800	+1/4	+17.4	+7.7



400SA2MP15



### (3) Power shift control



400SA2MP16

The set horsepower valve is shifted by varying the command current level of the proportional pressure reducing valve attached to the pump. Only one proportional pressure reducing valve is provided.

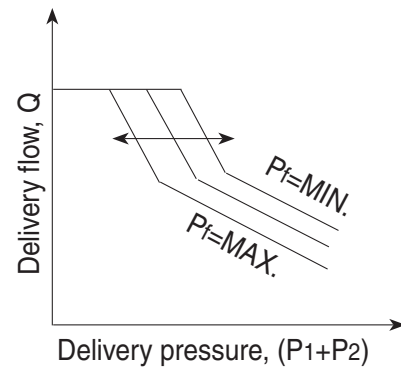
However, the secondary pressure  $P_f$  (power shift pressure) is admitted to the horsepower control section of each pump regulator through the pump's internal path to shift it to the same set horsepower level.

This function permits arbitrary setting of the pump output power, thereby providing the optimum power level according to the operating condition.

The power shift pressure  $P_f$  controls the set horsepower of the pump to a desired level, as shown in the figure.

As the power shift pressure  $P_f$  rises, the compensating rod (623) moves to the right via the pin (898) and compensating piston (621).

This decreases the pump tilting angle and then the set horsepower in the same way as explained in the overload preventive function of the horsepower control. On the contrary, the set horsepower rises as the power shift pressure  $P_f$  falls.



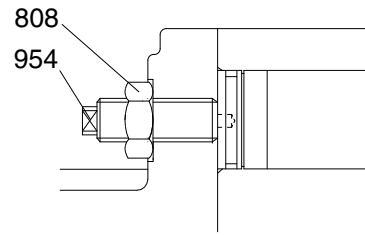
#### (4) Adjustment of maximum and minimum flows

##### ① Adjustment of maximum flow

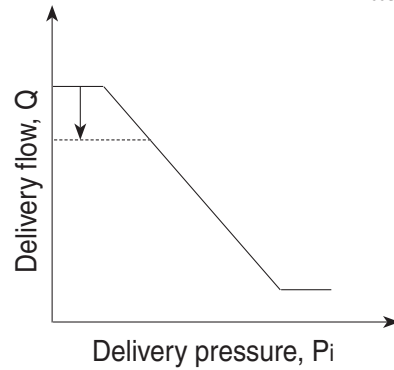
Adjust it by loosening the hexagon nut (808) and by tightening (or loosening) the set screw (954).

The maximum flow only is adjusted without changing other control characteristics.

Speed	Adjustment of max flow spring	
	Tightening amount of adjusting screw (954)	Flow change amount
(min <sup>-1</sup> )	(Turn)	(ℓ/min)
1800	+1/4	-6.9



400SA2MP17

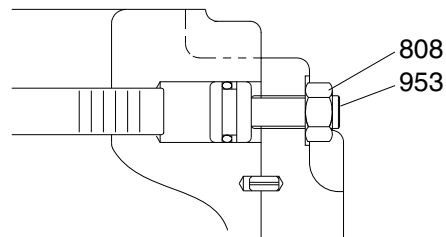


##### ② Adjustment of minimum flow

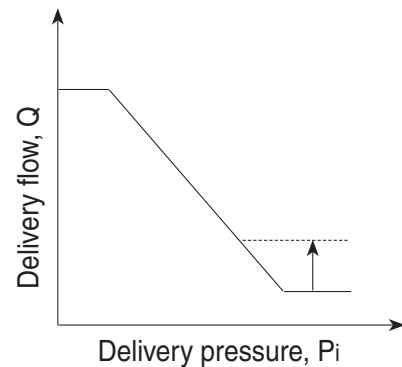
Adjust it by loosening the hexagon nut (808) and by tightening (or loosening) the hexagonal socket head set screw (953). Similarly to the adjustment of the maximum flow, other characteristics are not changed.

However, remember that, if tightened too much, the required horsepower during the maximum delivery pressure (or during relieving) may increase.

Speed	Adjustment of min flow spring	
	Tightening amount of adjusting screw (953)	Flow change amount
(min <sup>-1</sup> )	(Turn)	(ℓ/min)
1800	+1/4	+6.9

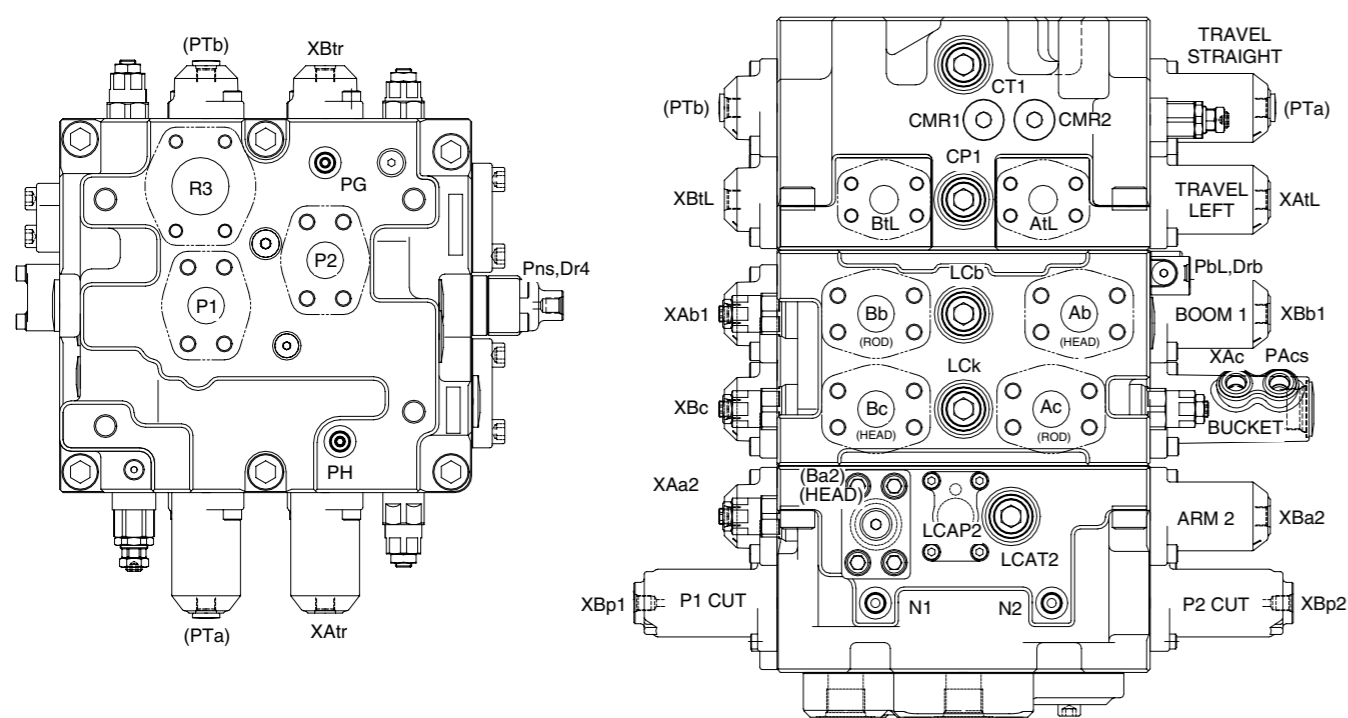


400SA2MP18

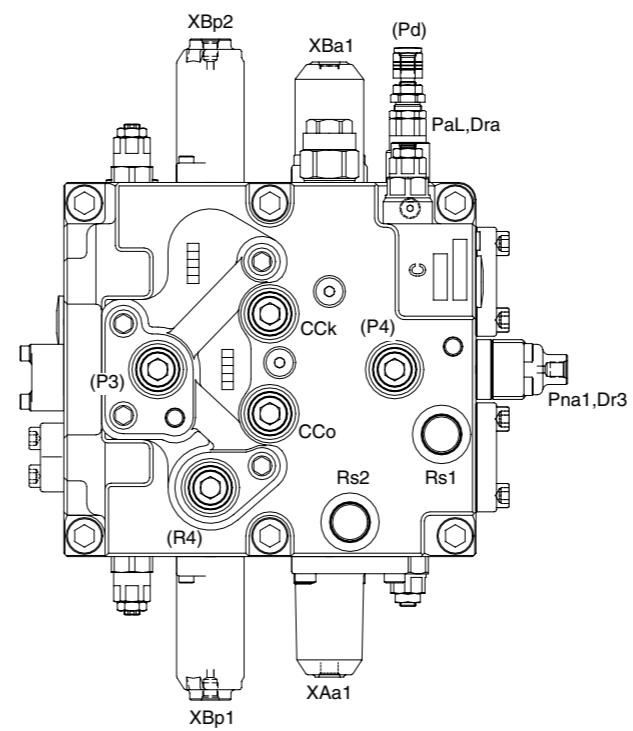


# GROUP 2 MAIN CONTROL VALVE

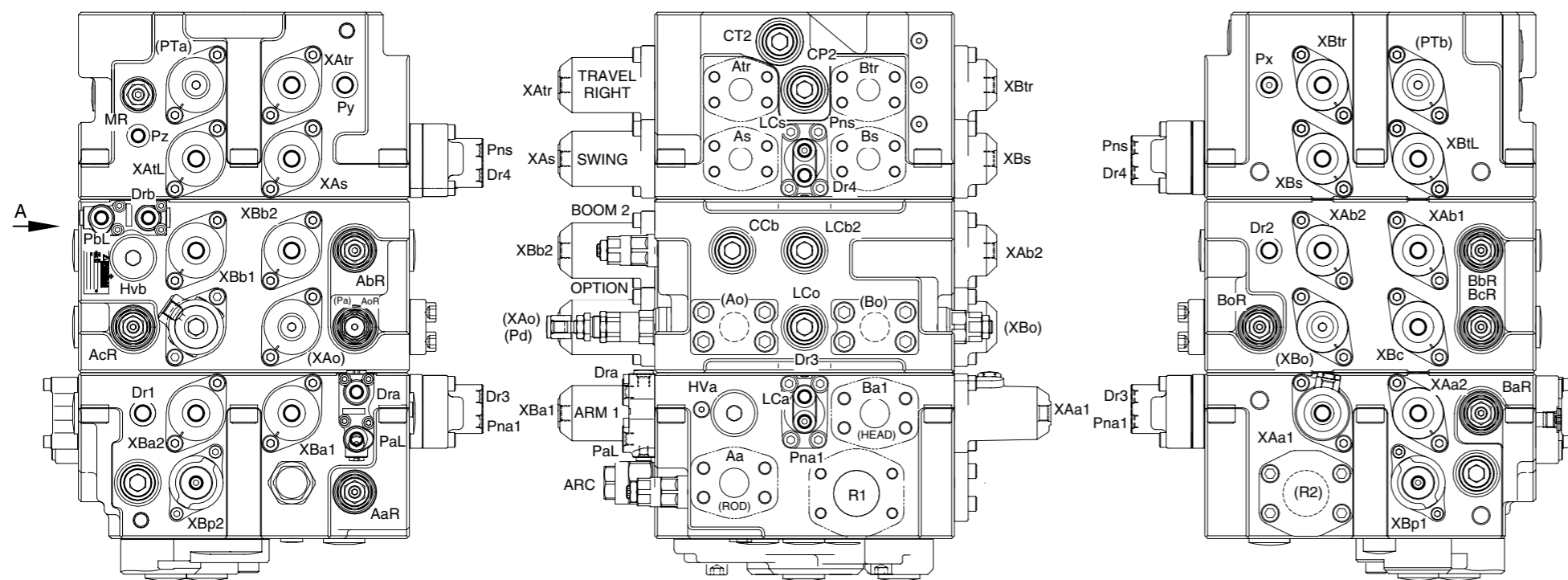
## 1. STRUCTURE (1/2)



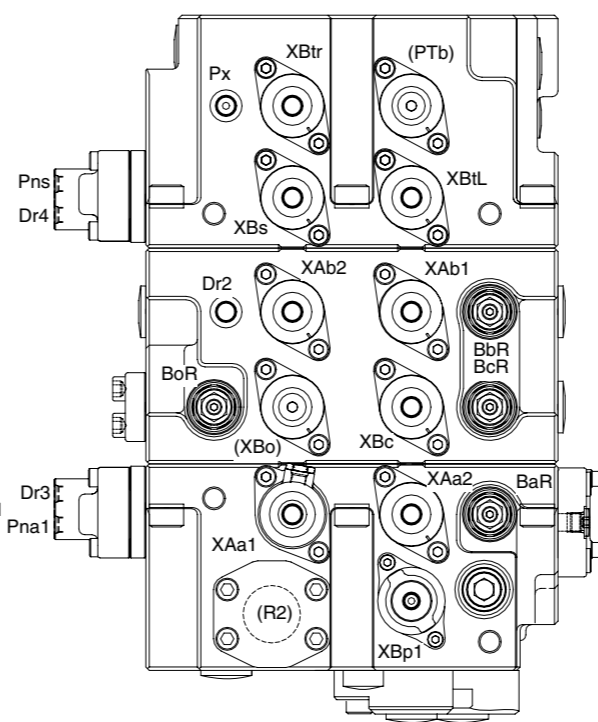
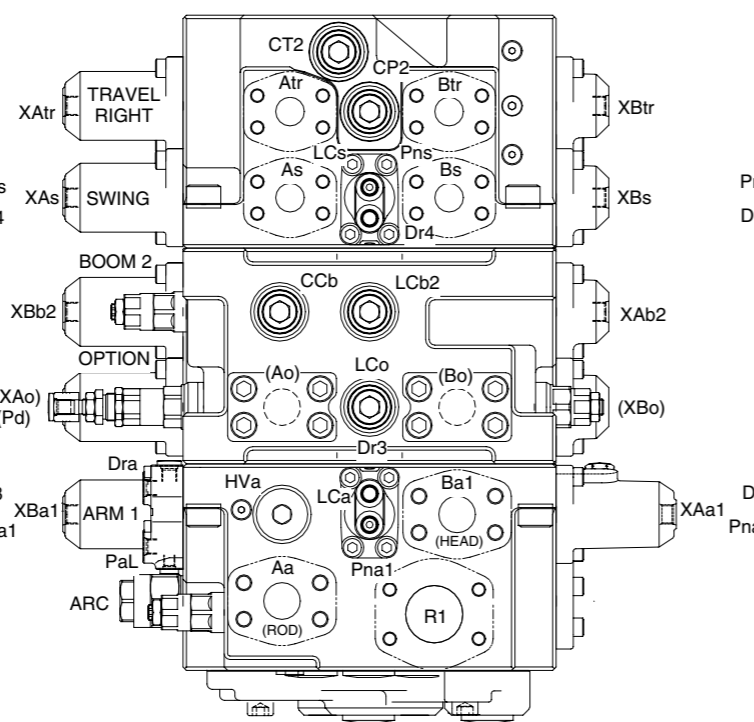
VIEW A



VIEW B

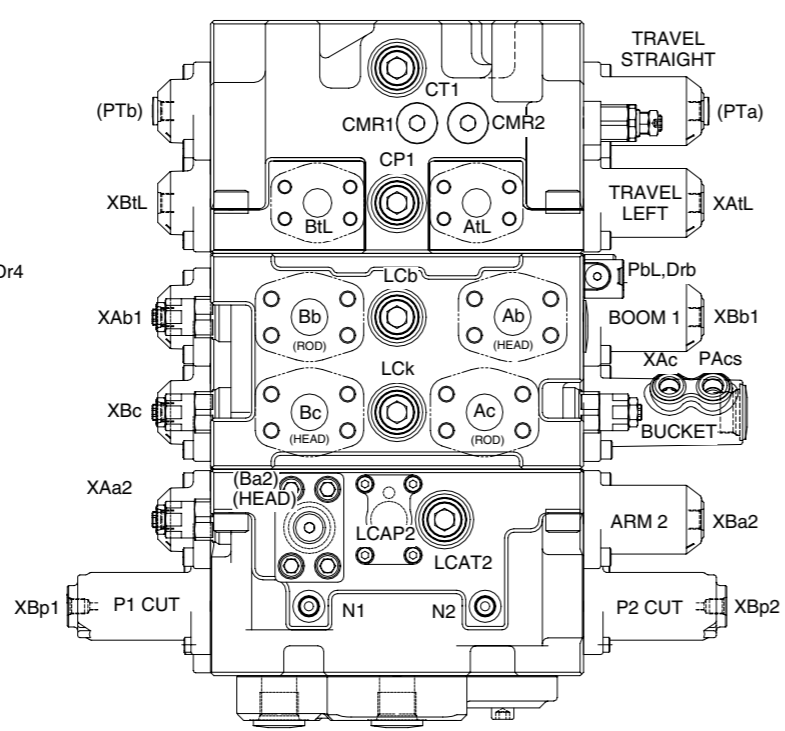
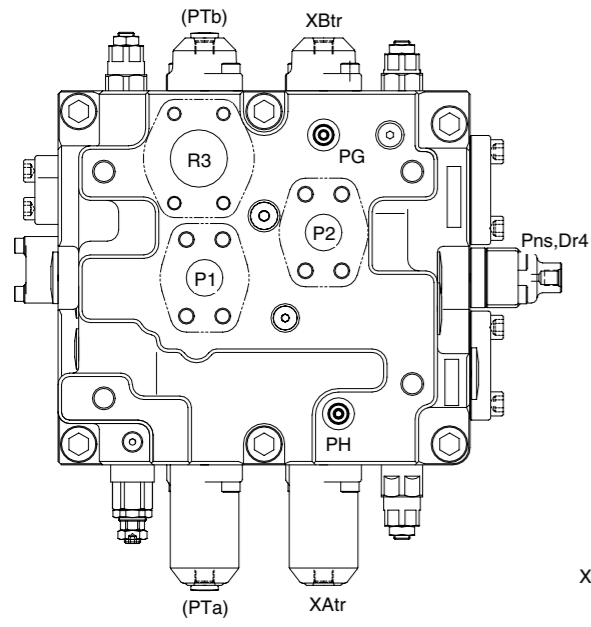


A  
B

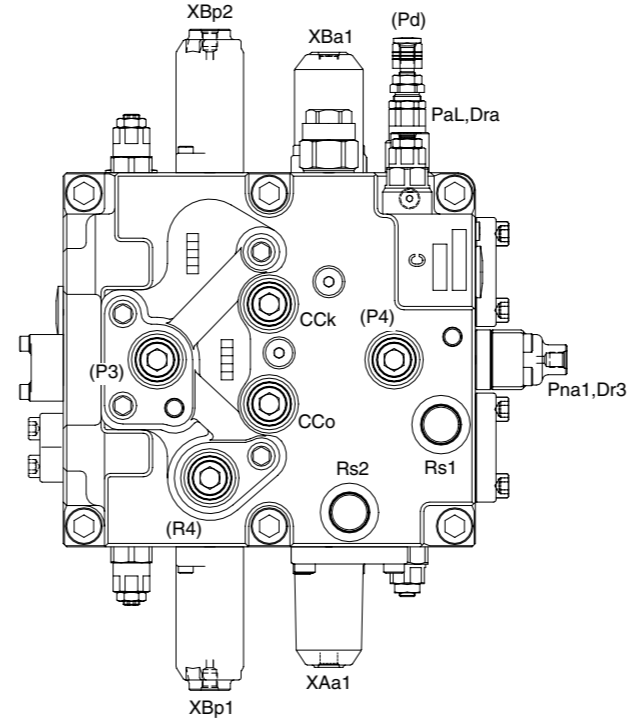


Mark	Port name	Port size	Tightening torque
(P3)	-	PF1	20.4~25.5 kgf · m (148~184 lbf · ft)
(P4)	-		
(R4)	-		
Rs1	Make up port		
Rs2	Make up port		
XAtr	Travel left (forward) pilot port	PF3/8	7.0~8.0 kgf · m (50.6~57.9 lbf · ft)
XBtr	Travel left (reverse) pilot port		
(XAO)	Optional pilot port		
(XBO)	Optional pilot port		
XAc	Bucket out pilot port		
XBc	Bucket in pilot port		
XAb1	Boom up pilot port		
XBb1	Boom down pilot port		
XAb2	Boom up pilot port		
XBb2	Boom down pilot port		
XAa2	Arm out confluence pilot port		
XBa2	Arm in confluence pilot port		
XAtL	Travel right (forward) pilot port		
XBtL	Travel right (reverse) pilot port		
XAs	Swing right pilot port		
XBs	Swing left pilot port		
XAa1	Arm out pilot port		
XBa1	Arm in pilot port		
Dr1	Drain port		
Dr2	Drain port		
(PTa)	-		
(PTb)	-		
PAcS	Bucket in stroke limit pilot port		
N1	Nega-con pressure pilot port (P1 side)		
N2	Nega-con pressure pilot port (P2 side)		
PG	Pilot port		
PH	Pilot port		
Px	Pressure port for attachment		
Py	Pressure port for travel		

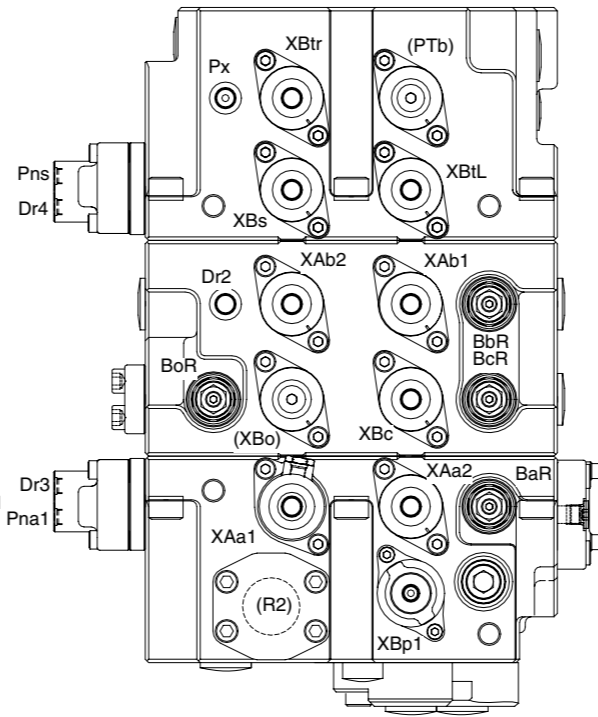
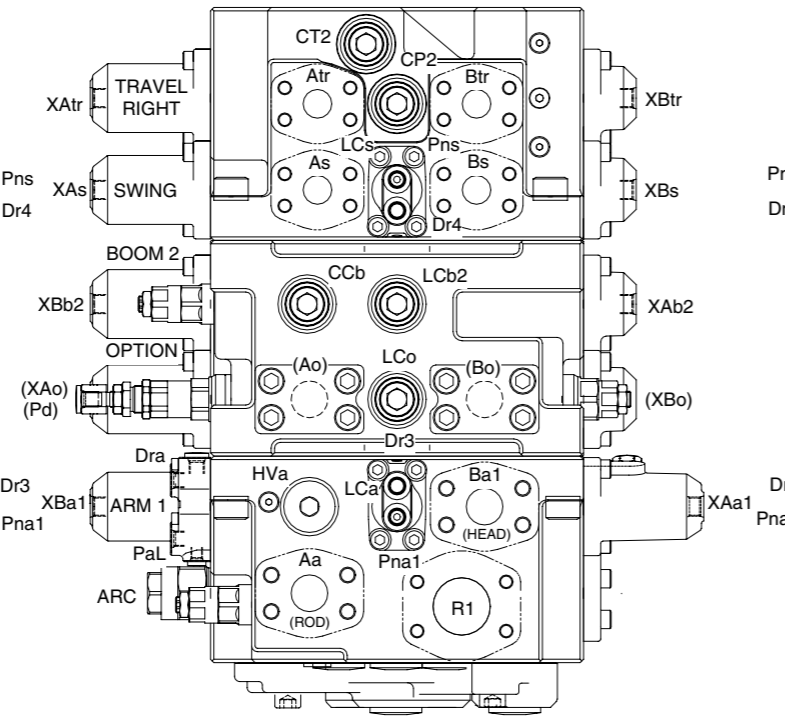
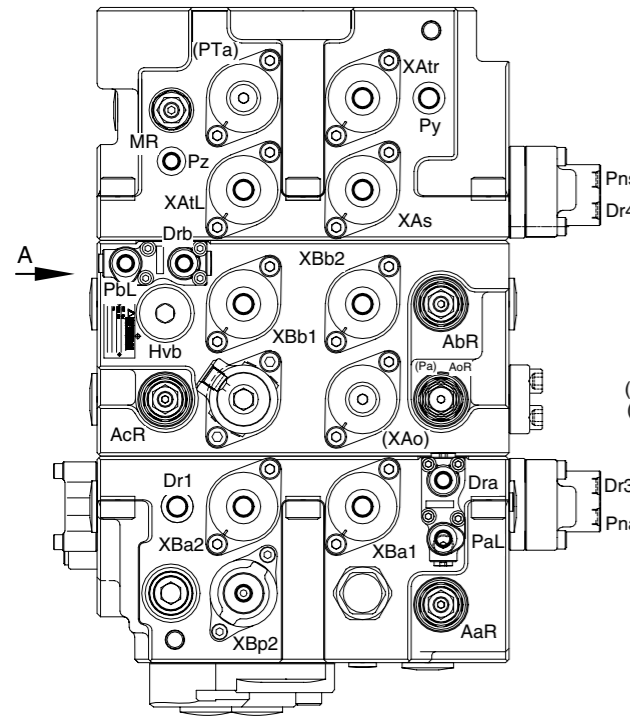
STRUCTURE (2/2)



VIEW A



VIEW B

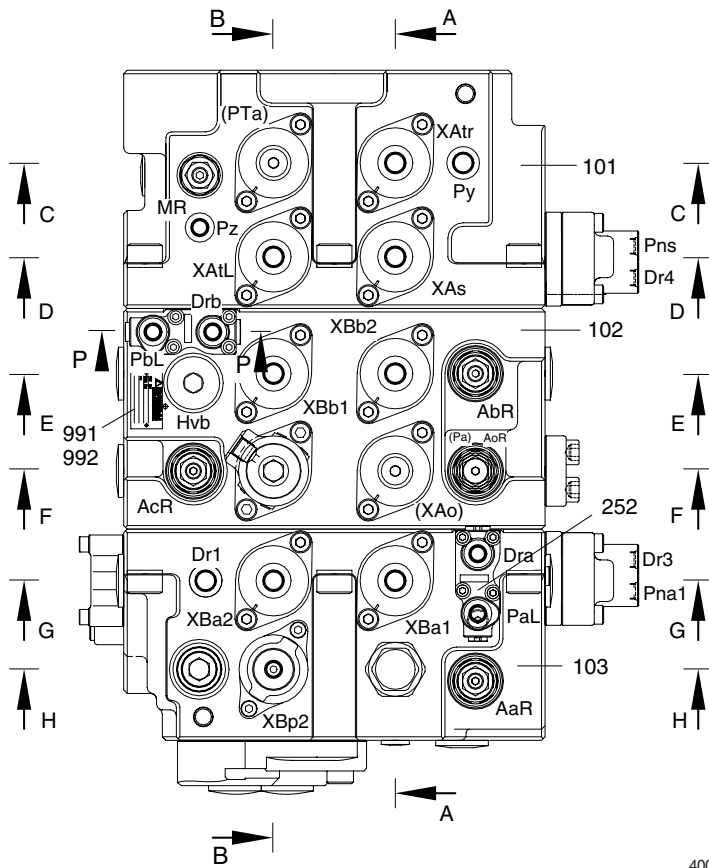


Mark	Port name	Port size	Tightening torque		
XBp1	Bypass cut spool pilot port (P1 side)	PF1/4	3.5~3.9 kgf · m (25.3~28.2 lbf · ft)		
XBp2	Bypass cut spool pilot port (P2 side)				
PaL	Lock valve pilot port (arm rod side)				
PbL	Lock valve pilot port (boom head side)				
Dra	Drain port				
Drb	Drain port				
Pna1	Arm regeneration cut pilot port				
Pns	Swing priority pilot port				
Dr3	Drain port				
Dr4	Drain port				
Pz	Main relief pilot pressure port				
(Pd)	Option relief pilot pressure port				
Atr	Travel motor left side (reverse) port			M12	8.5~11.2 kgf · m (61.5~81.0 lbf · ft)
Btr	Travel motor left side (forward) port				
As	Swing motor right port				
Bs	Swing motor left port				
AtL	Travel motor right side (reverse) port				
BtL	Travel motor right side (forward) port				
R1	Return port				
(R2)	-	M14	14.3~18.4 kgf · m (103~133 lbf · ft)		
R3	Return port				
P1	Pump port (A2 side)				
P2	Pump port (A1 side)				
(Ao)	Optional port				
(Bo)	Optional port				
Aa	Arm out port				
Ba1	Arm in port				
Ab	Boom up port				
Bb	Boom down port				
Ac	Bucket out port				
Bc	Bucket in port				
(Ba2)	-				

A  
B



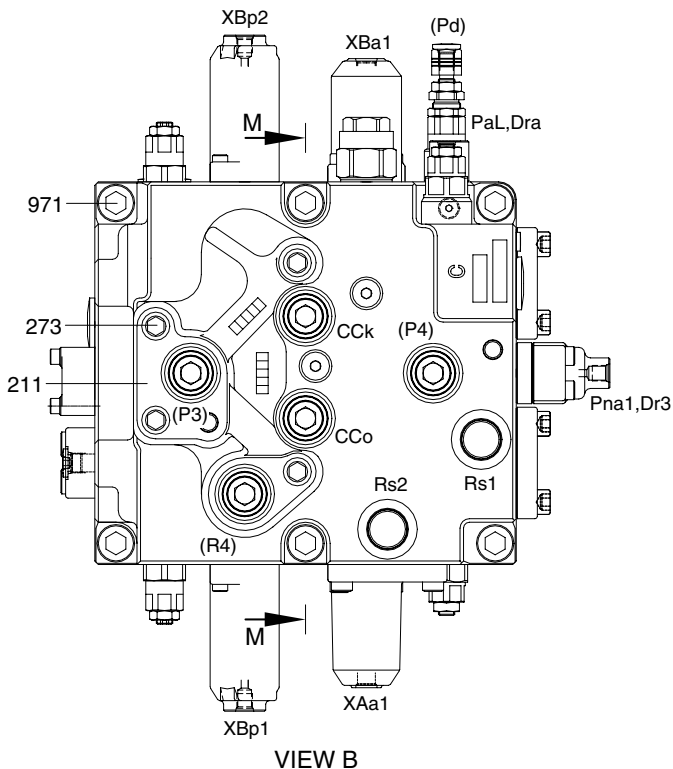
### 1) RELIEF VALVE SIDE VIEW



- 101 Casing A
- 102 Casing B
- 103 Casing C
- 252 Lock valve selector sub assy
- 991 Name plate
- 992 Pin

400SA2MC03

### 2) BACK SIDE VIEW

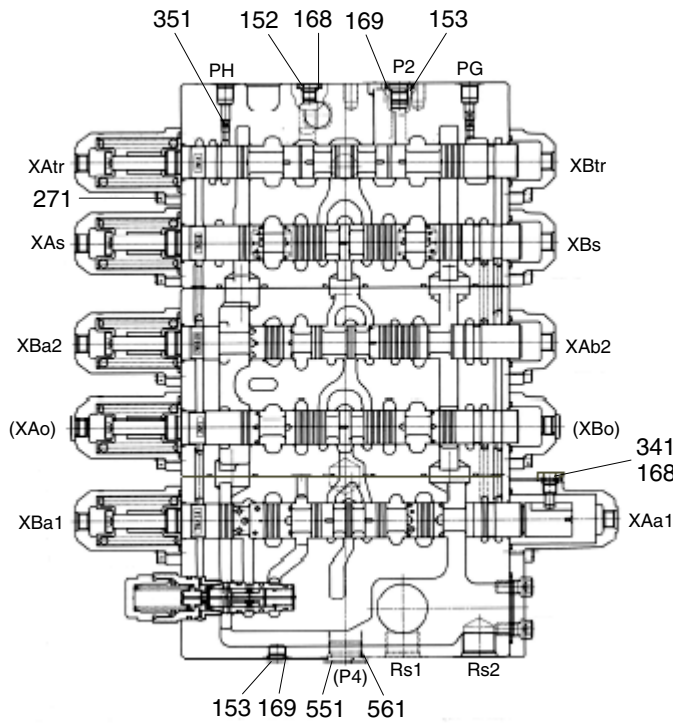


- 211 Plate
- 273 Hexagon socket screw
- 971 Hexagon socket screw

VIEW B

400SA2MC04

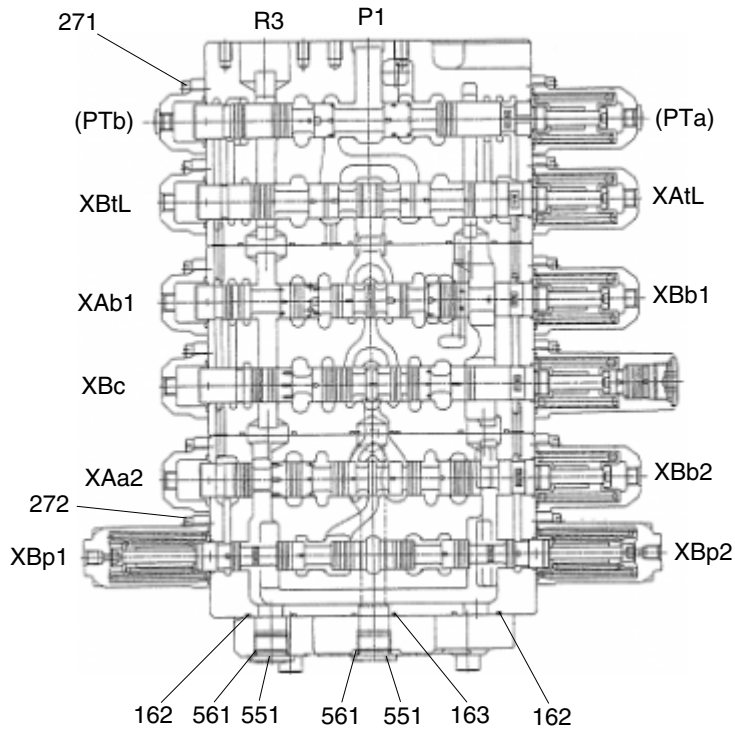
### 3) P2 SPOOL SECTION



- 152 ROH plug
- 153 ROH plug
- 168 O-ring
- 169 O-ring
- 271 Hexagon socket screw
- 341 Plug
- 351 Orifice
- 551 Plug
- 561 O-ring

400SA2MC05

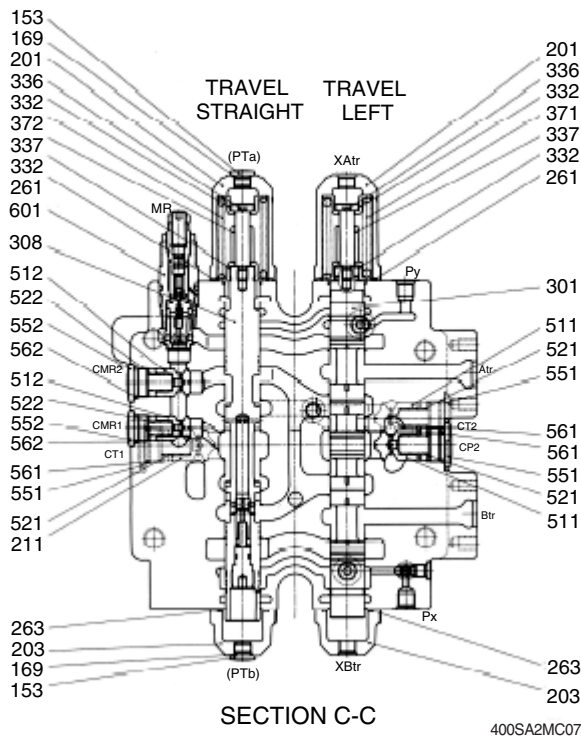
### 4) P1 SPOOL SECTION



- 162 O-ring
- 163 O-ring
- 271 Hexagon socket screw
- 272 Hexagon socket screw
- 551 Plug
- 561 O-ring

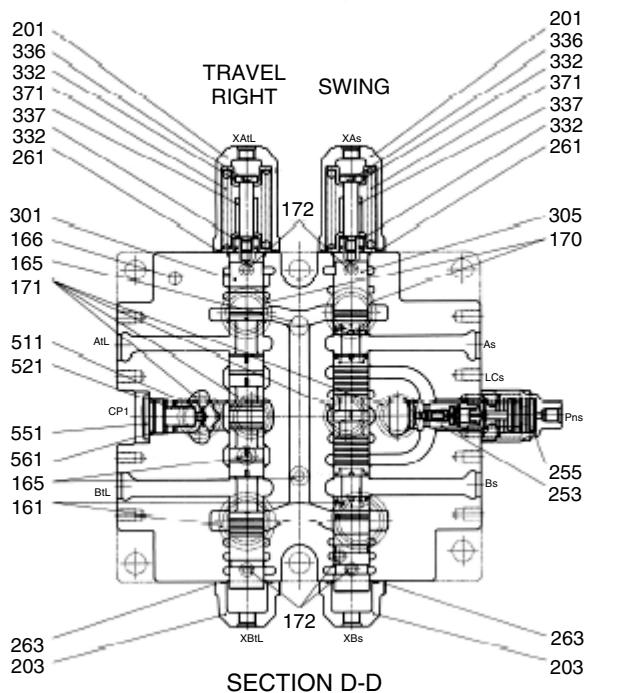
400SA2MC06

## 5) TRAVEL LEFT AND TRAVEL STRAIGHT SECTION



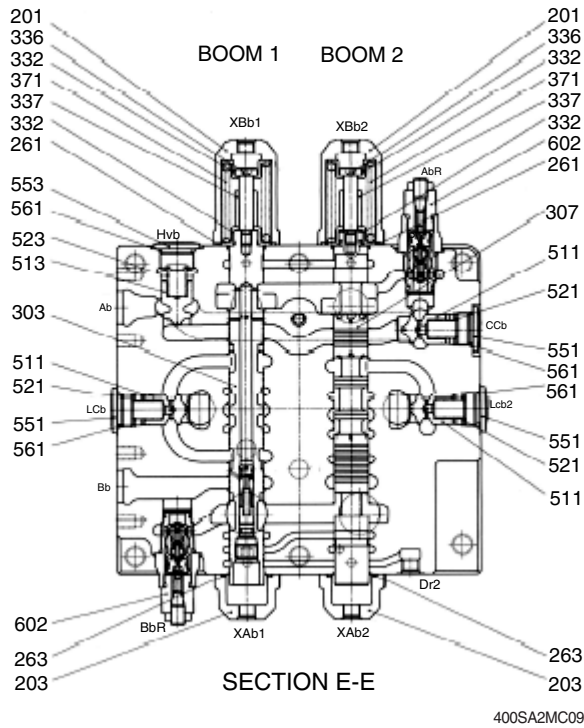
- 153 ROH plug
- 169 O-ring
- 201 Spring cover
- 203 Spool cover
- 261 O-ring
- 263 O-ring
- 301 Travel spool
- 308 Straight travel spool sub assy
- 332 Spring seat
- 336 Spacer bolt
- 337 Stopper
- 371 Spring
- 372 Spring
- 511 Poppet
- 512 Poppet
- 521 Spring
- 522 Spring
- 551 Plug
- 552 Plug
- 561 O-ring
- 562 O-ring
- 601 Main relief valve assy

## 6) TRAVEL RIGHT AND SWING SECTION



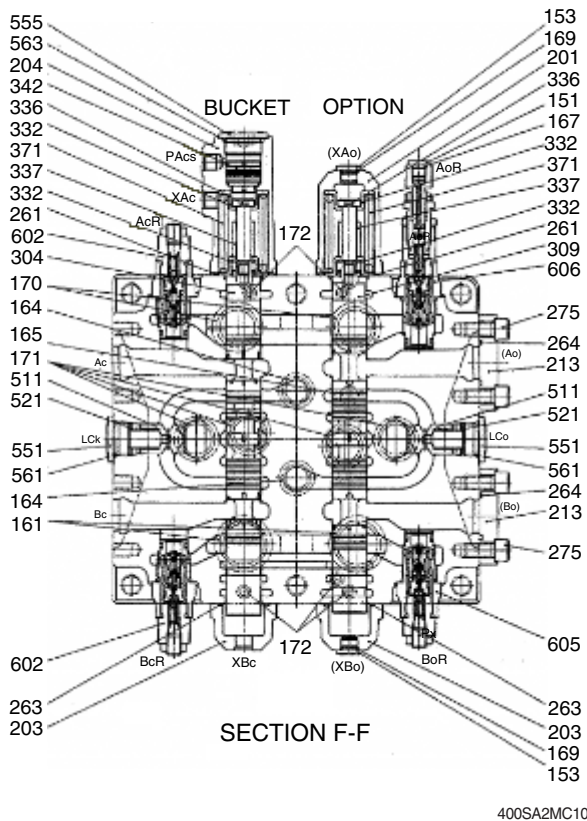
- 161 O-ring
- 165 O-ring
- 166 O-ring
- 170 O-ring
- 171 O-ring
- 172 O-ring
- 201 Spring cover
- 203 Spool cover
- 253 Logic poppet assy
- 255 Logic control valve assy
- 261 O-ring
- 263 O-ring
- 301 Travel spool
- 305 Swing spool
- 332 Spring seat
- 336 Spacer bolt
- 337 Stopper
- 371 Spring
- 511 Poppet
- 521 Spring
- 551 Plug
- 561 O-ring

## 7) BOOM 1 AND BOOM 2 SECTION



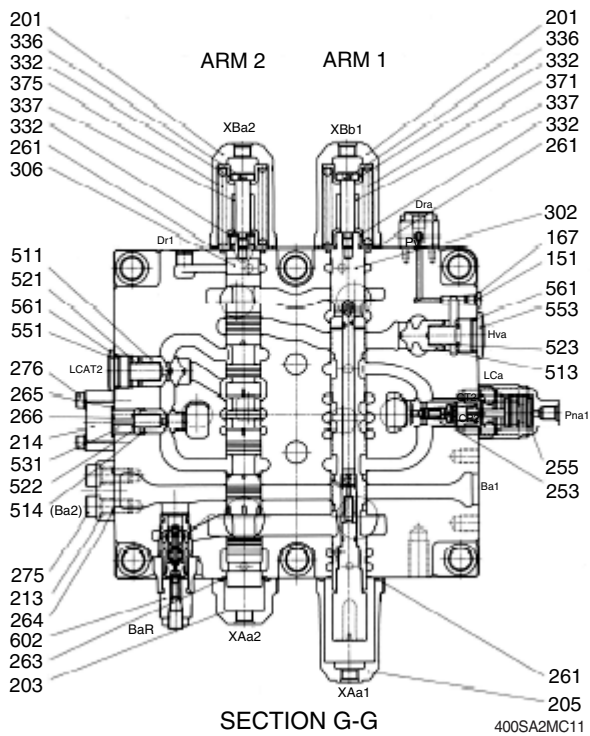
- 201 Spring cover
- 336 Spool cover
- 332 Spool cover
- 371 O-ring
- 337 O-ring
- 332 O-ring
- 602 O-ring
- 261 O-ring
- 553 Boom 1 spool sub assy
- 561 Boom 2 spool
- 523 Spring seat
- 513 Spacer bolt
- 303 Stopper
- 511 Spring
- 521 Poppet
- 551 Poppet
- 561 Spring
- 561 Spring
- 523 Spring
- 551 Plug
- 553 Plug
- 561 O-ring
- 602 Port relief valve assy

## 8) BUCKET AND OPTION SECTION



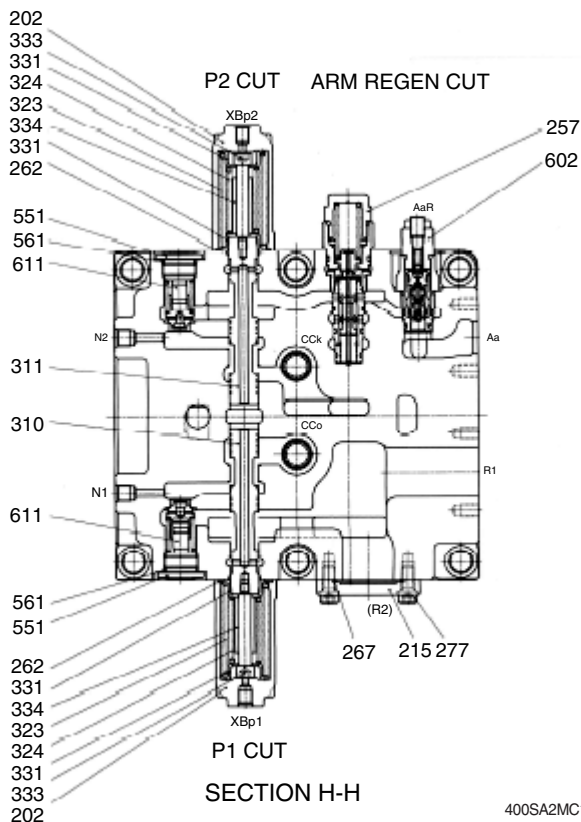
- 151 ROH plug
- 153 ROH plug
- 161 O-ring
- 169 O-ring
- 201 O-ring
- 336 O-ring
- 151 O-ring
- 167 O-ring
- 332 O-ring
- 371 O-ring
- 337 O-ring
- 332 O-ring
- 261 O-ring
- 309 O-ring
- 606 O-ring
- 275 Spring cover
- 203 Spool cover
- 204 Spool cover
- 213 Flange
- 261 O-ring
- 263 O-ring
- 264 Square ring
- 275 Hexagon socket screw
- 304 Bucket spool
- 309 Option spool
- 332 Spring seat
- 336 Spacer bolt
- 337 Stopper
- 371 Spring
- 511 Poppet
- 521 Spring
- 551 Plug
- 555 Plug
- 561 O-ring
- 562 O-ring
- 563 O-ring
- 602 Port relief valve assy
- 605 Port relief valve assy
- 606 Port relief valve assy

### 9) ARM 1 AND ARM 2 SECTION



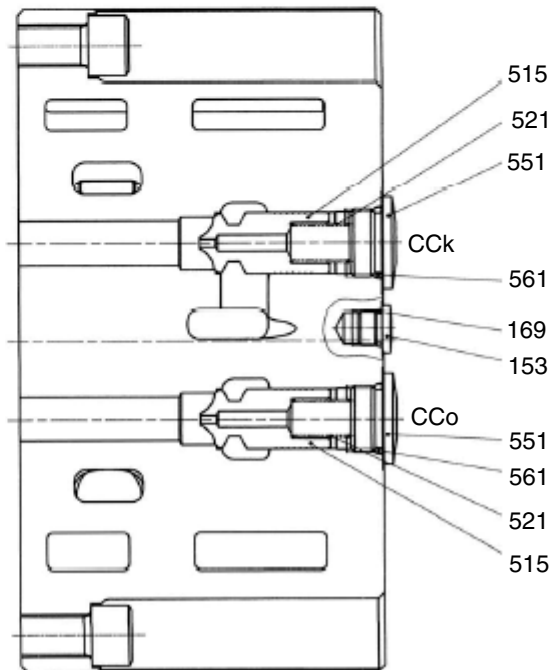
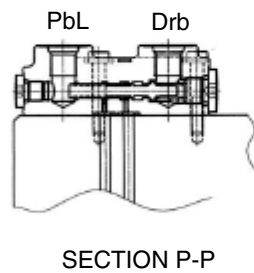
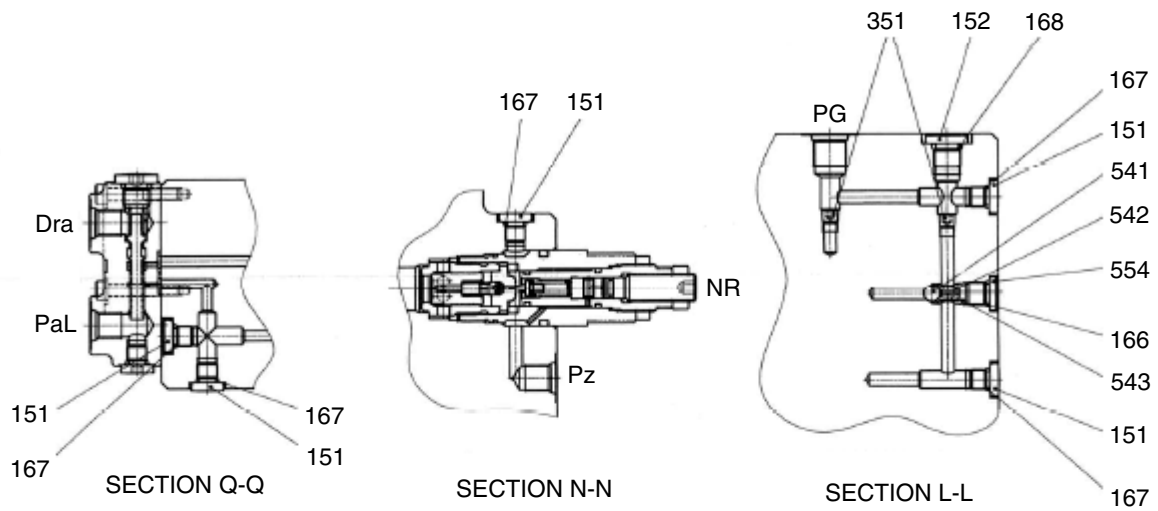
- 151 ROH plug
- 167 O-ring
- 201 Spring cover
- 203 Spool cover
- 263 O-ring
- 205 Spool cover
- 213 Flange
- 214 Load check cover
- 253 Logic poppet assy
- 255 Logic control valve assy
- 261 O-ring
- 264 Square ring
- 265 O-ring
- 266 Square ring
- 275 Hexagon socket screw
- 276 Hexagon socket screw
- 302 Arm 1 spool sub assy
- 306 Arm 2 spool
- 332 Spring seat
- 336 Spacer bolt
- 337 Stopper
- 371 Spring
- 375 Spring
- 511 Poppet
- 513 Poppet
- 514 Poppet
- 521 Spring
- 522 Spring
- 523 Spring
- 531 Spring seat
- 551 Plug
- 553 Plug
- 561 O-ring
- 602 Port relief valve assy

### 10) BYPASS CUT (P1 & P2)



- 202 Spring cover
- 215 Blank flange
- 257 Arm regen cut sub assy
- 262 O-ring
- 267 O-ring
- 277 Hexagon socket screw
- 310 Bypass-cut assy
- 311 Bypass-cut assy
- 323 Spring
- 324 Spring
- 331 Spring seat
- 333 Spacer bolt
- 334 Stopper
- 551 Plug
- 561 O-ring
- 602 Hexagon socket screw
- 611 Nega-con relief valve assy

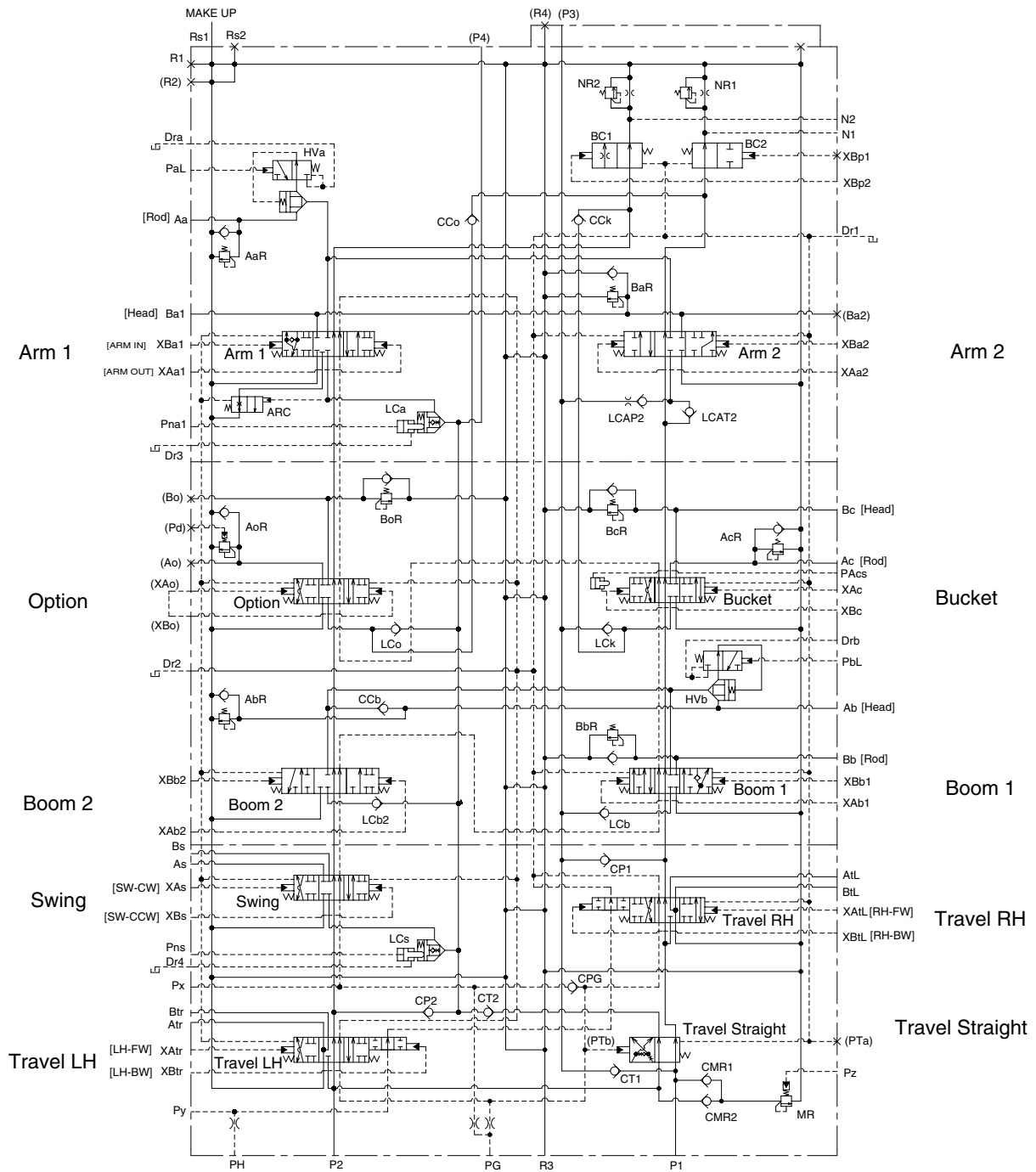
## 11) OTHER SECTION



380A2MC13

151 ROH plug	169 O-ring	543 Spring
152 ROH plug	351 Orifice	551 Plug
153 ROH plug	515 Poppet	554 Plug
166 O-ring	521 Spring	561 O-ring
167 O-ring	541 Steel ball	
168 O-ring	542 Spring seat	

## 2. HYDRAULIC CIRCUIT



400SA2MC14

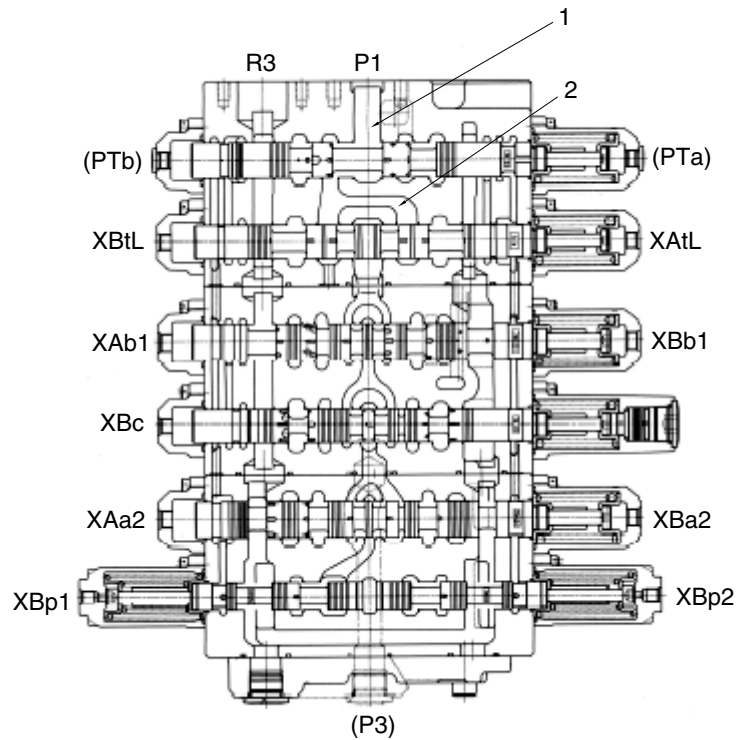
### 3. OPERATION

#### 1) NEUTRAL POSITIONS OF SPOOLS

##### (1) P1 HOUSING SIDE

When all spools are in the neutral positions, the pressurized oil discharged from the hydraulic pump (A1) passes through port P1, the main path (1), the bypass circuit (2) passing the spools for travel straight (308), travel left (301), boom 1 (303), bucket (304), arm 2 (306) and boom 1 side negative control orifice, and returns to the hydraulic oil tank through the return port (R1), (R3).

The negative control signal pressure of the boom 1 side negative control relief valve (611) is led from port N1 to the regulator on the hydraulic pump (A1) side, and controls the pump discharge flow rate to its minimum value.



380A2MC15

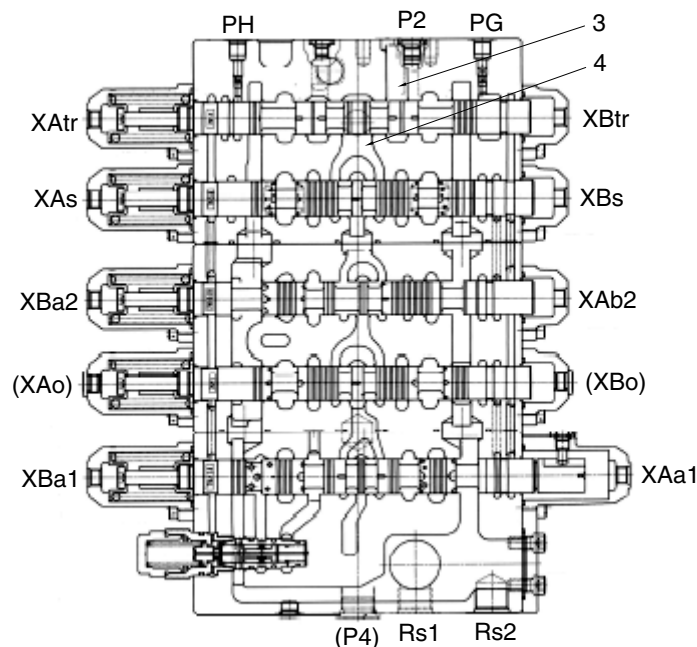


## (2) P2 housing side

The oil discharged from the hydraulic pump (A2) passes through port P2, the main path (3), the bypass circuit (4) passing the spools for travel right (301), swing (305), boom 2 (307), option (309), arm 1 (302) and arm 1 side negative control orifice, and returns to the hydraulic oil tank through the return port (R1), (R3).

The negative control signal pressure of the arm 1 side negative control relief valve (611) is led from port N2 to the regulator on the hydraulic pump (A2) side, and controls the pump discharge flow rate to its minimum value.

When any of nine main spools is changed over, the bypass circuit (2) or (4) is cut off and the control signal pressure at port N1 or N2 in the negative control circuit is changed tank pressure, and controls the pump discharge flow rate to its maximum value.



380A2MC16

## 2) TRAVEL OPERATION

### (1) Pilot circuit

Since any of the travel spools (301) on the left or right transfers and shuts off the side-bypass path, the pressure at port Py (pressure port for travel) increases.

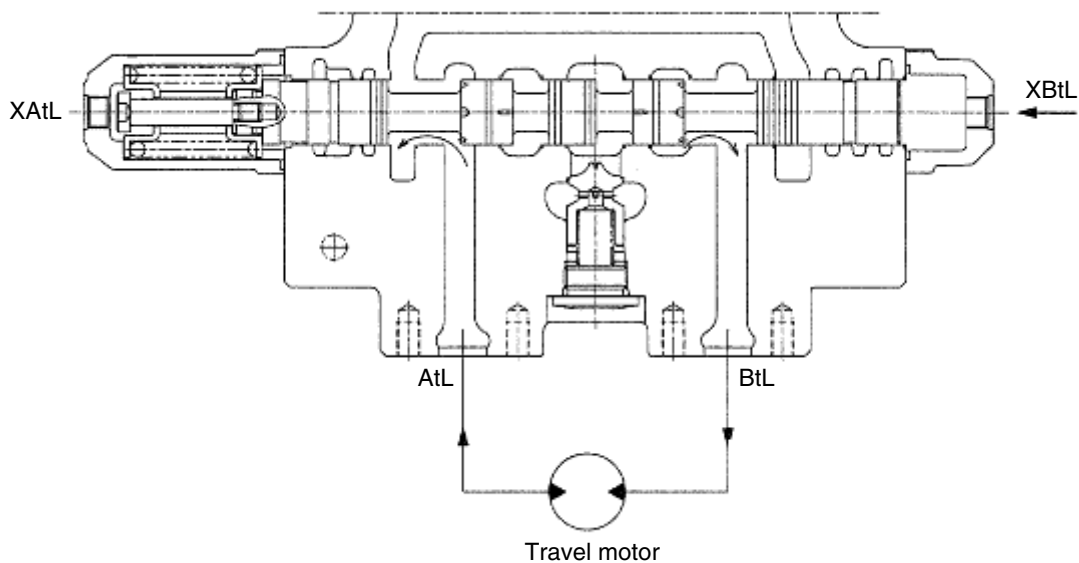
### (2) Main circuit

When pilot port XBtL of the travel left spool (301) is pressurized, the bypass circuit (2) in the boom 1 side is shut off and pressurized oil from port P1 passes through port BtL and flows to the travel left motor.

When pilot port XBtr of the travel right spool (301) is pressurized, the bypass circuit (4) in the arm 1 side is shut off and pressurized oil from port P2 passes through port Btr and flows to the travel right motor.

On the other hand, the return oil from the travel left(right) motor passes through port AtL(AtR) and travel left (right) spool , and returns to the hydraulic oil tank through the tank port (R1), (R3).

In the case of the opposite operation (when the pilot pressure is applied to ports XAtL and XAtr of the control valve), the operation is similar.



380A2MC17

### 3) ARM OPERATION

#### (1) Arm stretching operation

##### ① Pilot circuit

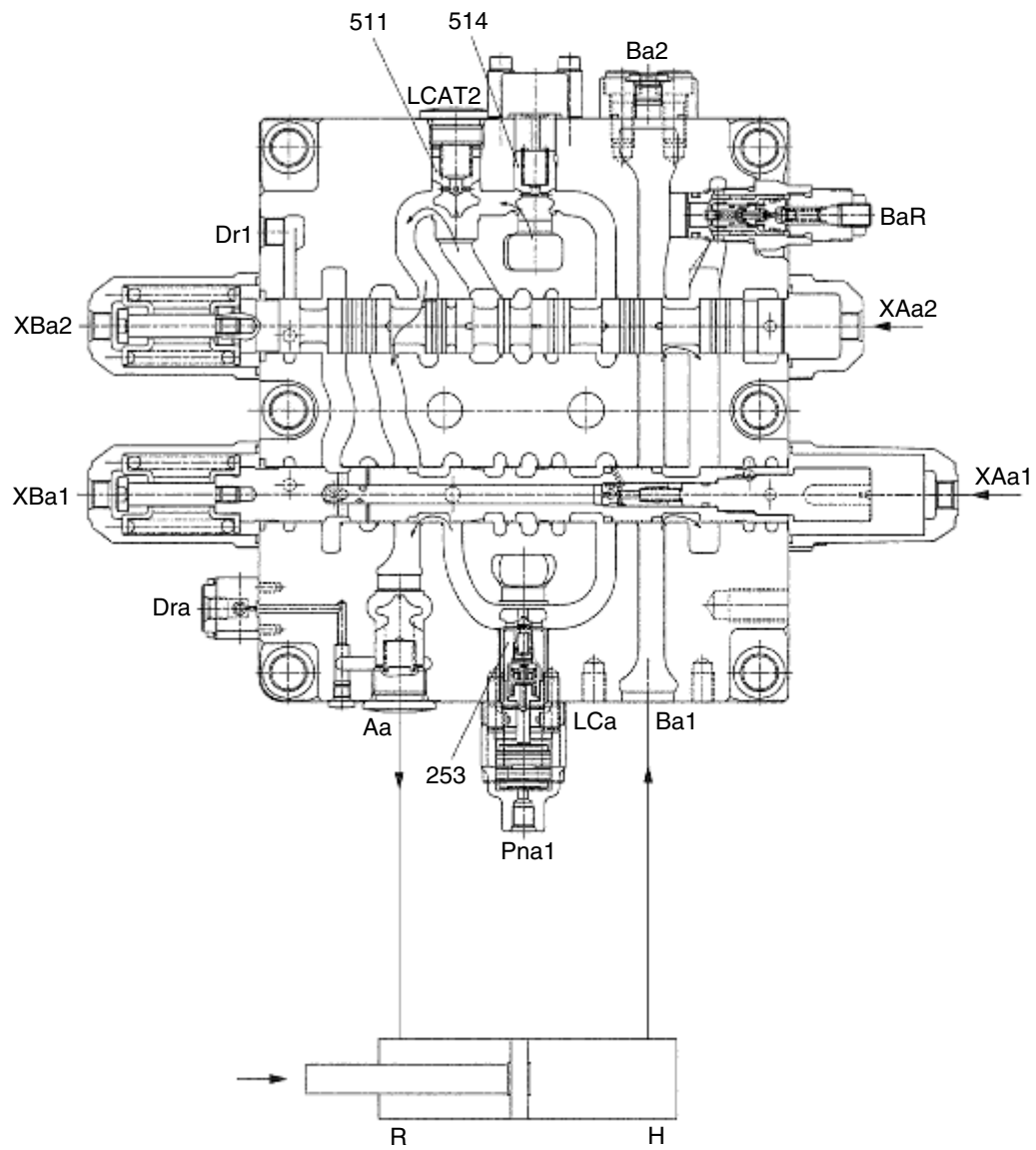
Since the arm 1 spool (302) transfers and shuts off the side-bypass path, the pressure at port Px increases.

##### ② Main circuit

During the arm stretching operation, the pilot pressure enters through ports XAa1 and XAa2. When the pressure enters through ports XAa1 and XAa2, the arm 1 and arm 2 spools transfer in the left direction in figure. The hydraulic oil entering through port P2 passes through the main path (3) and flows to the bypass circuit (4), but the bypass circuit is shut off due to transfer of the arm 1 spool (302). Therefore, the hydraulic oil from the parallel circuit pushes open the logic poppet (253) and flows through the U-shaped path to the arm 1 spool (302). Then, it flows around the periphery of the arm 1 spool (302) to port Aa, and is supplied to the arm cylinder rod side (R).

On the other hand, the oil entering through port P1 passes in the main path (1), and flows into the bypass circuit (2), and the bypass circuit is shut off due to transfer of the arm 2 spool (306). The hydraulic oil from the parallel circuit pushes open the check valve (514) and oil from the bypass circuit pushes open the check valve (511) and flows through the U-shaped path to the arm 2 spool (306). Then, it flows around the periphery of arm 2 spool (306) and joins into port Aa through the inside path.

Besides, the return oil from the arm cylinder head side (H) passes through port Ba1, flows into tank line in arm 1 side and in arm 2 side and returns to the hydraulic oil tank through the tank ports (R1), (R3).



380A2MC18

## (2) Arm excavating operation

### ① Pilot circuit

Since the arm 1 spool (302) transfers and shuts off the side-bypass path, the pressure at port Px (pressure port for attachment) increases. Then, the pressure enters also through port PaL and the release signal is sent to the lock valve selector (252).

### ② Main circuit

During the arm excavating operation, the pilot pressure enters through ports XBa1 and XBa2. When the pressure enters through ports XBa1 and XBa2, the arm 1 and arm 2 spools transfer in the right direction in figure. The hydraulic oil entering through port P2 passes through the main path (3) and flows to the bypass circuit (4), but the bypass circuit is shut off due to transfer of the arm 1 (302) spool. Therefore, the hydraulic oil from the parallel circuit pushes open the logic poppet (253) and flows through the U-shaped path to the arm 1 spool (302). Then, it flows around the periphery of the arm 1 spool (302) to port Ba1, and is supplied to the arm cylinder head side (H).

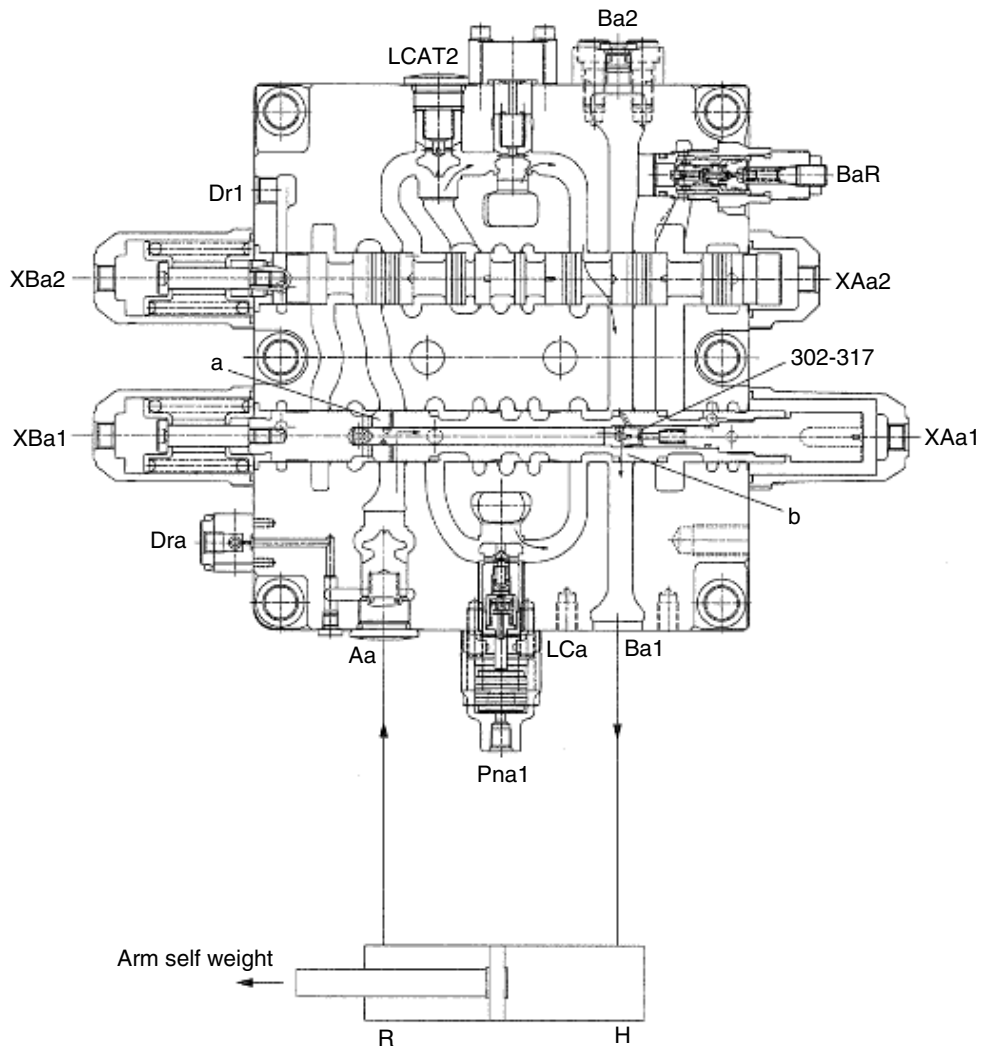
On the other hand, the hydraulic oil entering through port P1 passes in the main path (1), and flows into the bypass circuit (2), and the bypass circuit is shut off due to transfer of the arm 2 spool (306). The hydraulic oil from the parallel circuit pushes open the check valve (514) and oil from the bypass circuit pushes open the check valve (511) and flows through the U-shaped path to the arm 2 spool (306). Then, it flows around the periphery of arm 2 spool (306) and joins into port Ba1 through the inside path.

On the other hand, the return oil from the arm cylinder rod side (R) is pressurized by self-weight of the arms and so on, and returns to port Aa. The pressurized oil returning to port Aa enters into the spool through the outside hole (a) of the arm 1 spool (302). During a light load only, it pushes open the sleeve check valve (302-317) and joins into port Ba from the spool hole (b). This is called the arm regeneration function.

When the pressure in the arm cylinder head side (H) and the U-shaped path increases, the arm regeneration cut spool (257-103) is transferred in the left direction in Fig. \*\*\*, and at the same time the check valve (302-317) is closed by its backpressure.

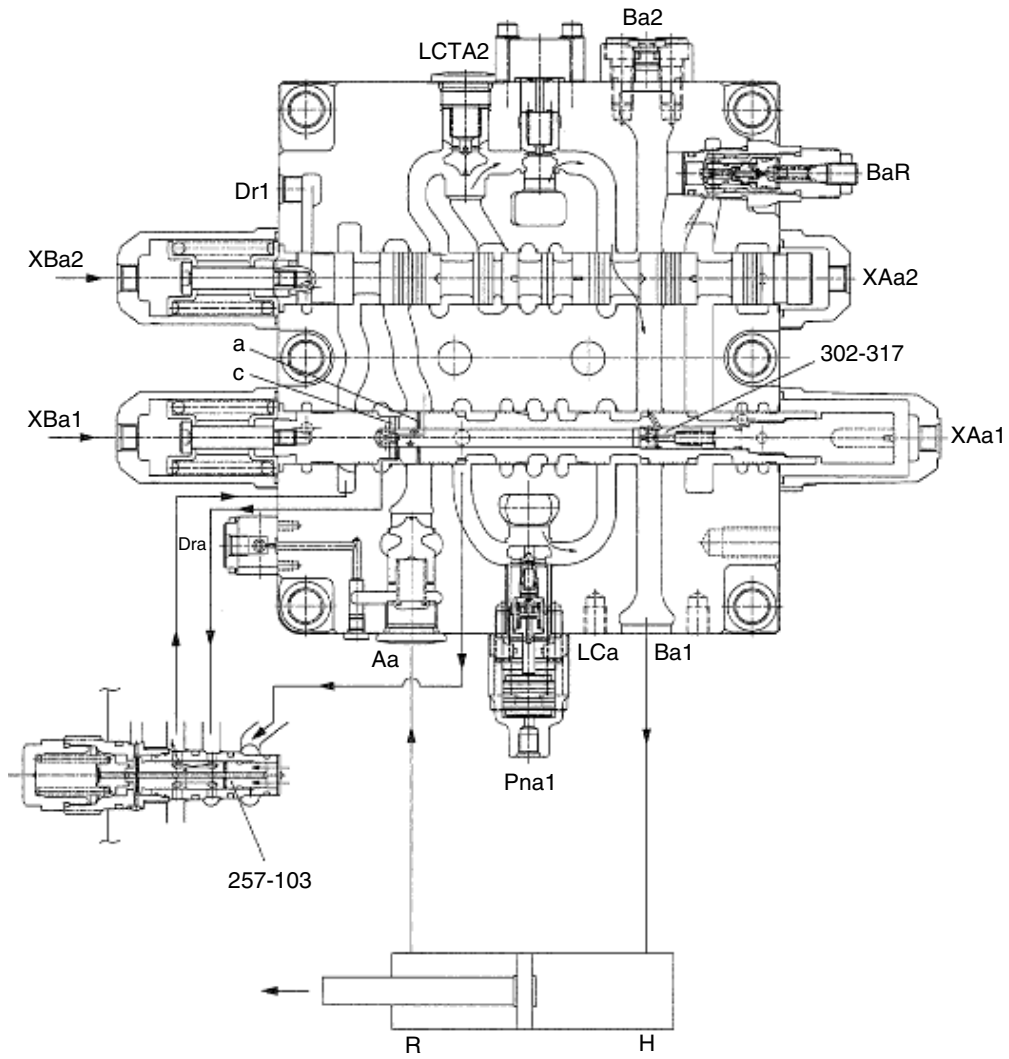
This shuts off the arm regeneration function, and the return oil from the arm cylinder rod side (R) enters from port Aa through the periphery hole (a) of the arm 1 spool (302) into the spool, flows to the arm regeneration cut valve (257) through the periphery hole (c) of the arm 1 spool (302), and returns through the tank port (R1), (R3) to the hydraulic oil tank.

· During light load only



380A2MC19

- In case the pressure in the arm cylinder head side (H) increases.



380A2MC20

## 4) BOOM OPERATION

### (1) Boom hoisting operation

#### ① Pilot circuit

Since the boom 2 spool (307) transfers and shuts off the side-bypass path, the pressure at port Px (Pressure port for attachment) increases.

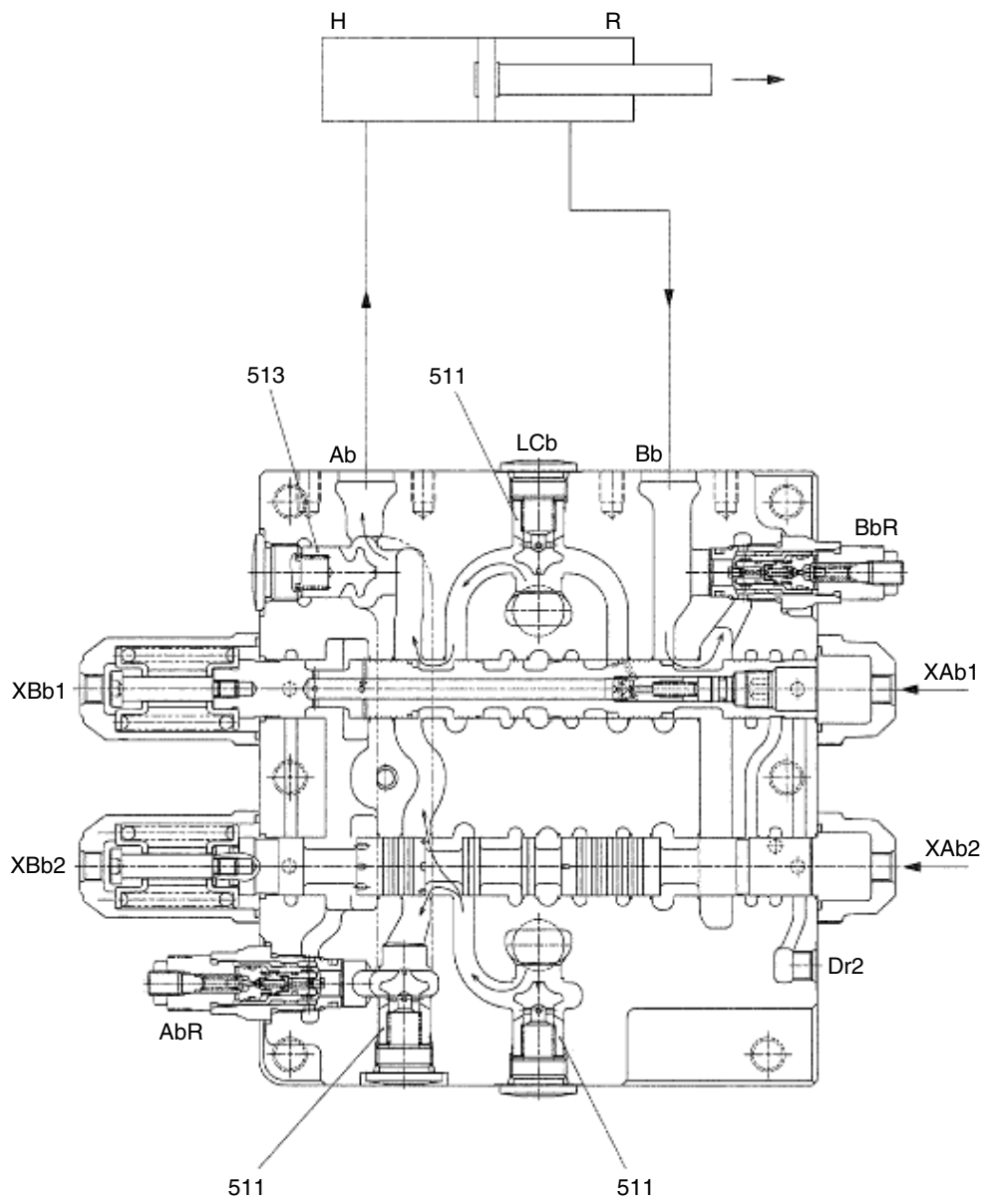
#### ② Main circuit

During the boom hoisting operation, the pilot pressure enters through port XAb1 and transfers the boom 1 spool (303) in the left direction in figure. The pressurized oil entering through port P1 passes through the main path (1) and flows to the bypass circuit (2), but the bypass circuit is shut off due to transfer of the boom 1 spool (303). Therefore, the pressurized oil flows into the parallel circuit, pushes open the check valve (511), and flows through U-shaped path to the boom 1 spool (303). Then, it flows around the periphery of the boom 1 spool (303) to port Ab, and is supplied to the boom cylinder head side (H).

At the same time, the pilot pressure enters also through port XAb2 to transfer the boom 2 spool (307) in the left direction in figure. Though the pressurized oil enters into port P2, the bypass circuit is shut off due to transfer of the boom 2 spool (307). Therefore, the oil flows in the parallel circuit and flows through the U-shaped path to the boom 2 spool (307). Then, the oil passes through the periphery of the boom 2 spool, pushes open the check valve (511), joins into port Ab through the inside path, and is supplied to the boom cylinder head side (H). (boom confluent flow)

On the other hand, the return oil from the boom cylinder rod side (R) enters through port Bb, passes around the periphery of the boom 1 spool (303), and returns to the hydraulic oil tank through the tank ports (R1), (R3).





380A2MC21

## (2) Boom lowering operation

### ① Pilot circuit

Since the boom 2 spool (307) transfers and shuts off the side-bypass path, the pressure at port Px increases. Then, the pressure enters also through port PbL and the release signal is sent to the lock valve selector (252).

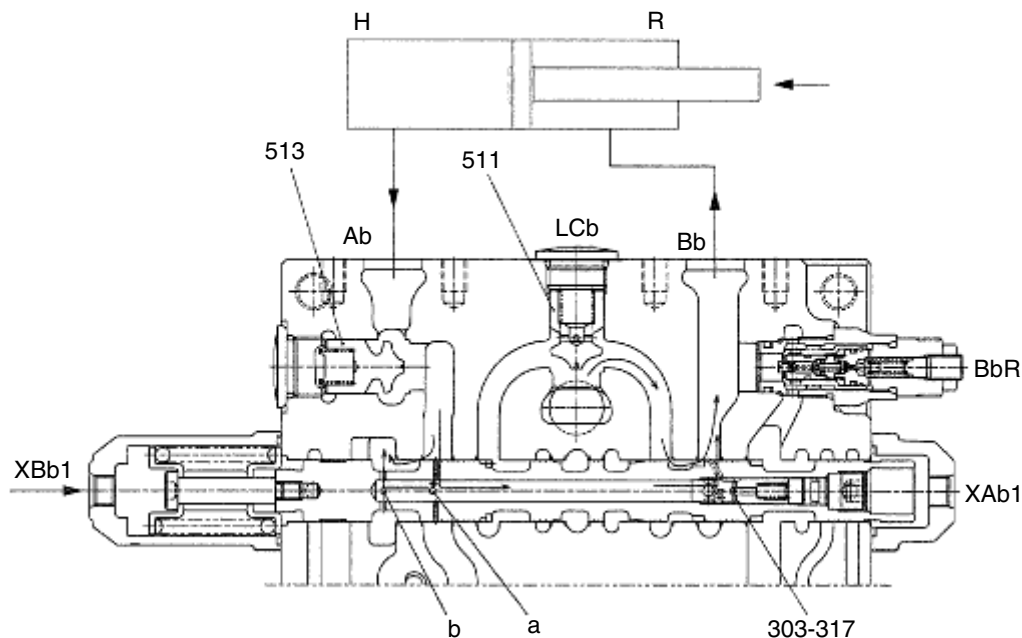
### ② Main circuit

During the boom lowering operation, the pilot pressure enters through port XBb1 and transfers the boom 1 spool (303) in the right direction in figure. The pressurized oil entering through port P1 passes through the main path (1) and flows to the bypass circuit (2), but the bypass circuit is shut off due to transfer of the boom 1 spool (303). Therefore, the pressurized oil flows into the parallel circuit, pushes open the check valve (511), and flows through the U-shaped path to the boom 1 spool (303). Then, it flows around the periphery of the boom 1 spool (303) to port Bb and is supplied to the boom cylinder rod side (R).

On the other hand, the return oil from the boom cylinder head side (H) passes through the periphery hole (a) and the periphery of the boom 1 spool (303).

Since this return oil has a sufficient pressure caused by the weight of the boom, it passes through the path inside the spool, pushes the poppet (303-317) in the spool in the right direction shown in the figure. flows around the outside of the spool. Then, it is supplied again to the boom cylinder rod side (R) as hydraulic oil to lower the boom. (boom regeneration function)

Besides, a part of the return oil from the boom cylinder flows from the hole (b) into the tank.



380A2MC22

## 5) BUCKET OPERATION

### (1) Bucket excavating operation

#### ① Pilot circuit

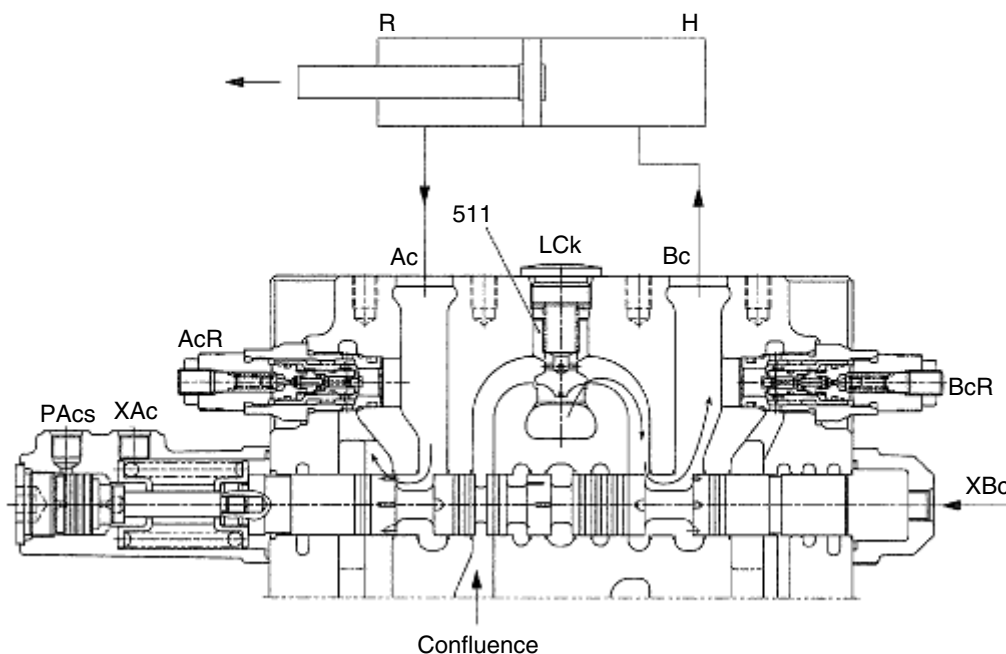
Since the bucket spool (304) transfers and shuts off the side-bypass path, the pressure at port Px increases. Then, the pressure enters also through port XBp2.

#### ② Main circuit

During the bucket excavating operation, the pilot pressure enters through port XBc and transfers the bucket spool (304) in the left direction in figure. The pressurized oil entering through port P1 passes through the main path (1) and flows through the bypass circuit (2), but the bypass circuit is shut off due to transfer of the bucket spool (304). Therefore, the pressurized oil flows into the parallel circuit, pushes open the check valve (511), and flows through the U-shaped path to the bucket spool (304). Then, it flows through the periphery of the bucket spool (304) to port Bc and is supplied to the bucket cylinder head side (H).

On the other hand, the return oil from the bucket cylinder rod side (R) enters through port Ac, passes around the periphery of the spool, and returns to the hydraulic oil tank through the tank ports (R1) and (R3).

During both the boom hoisting operation and bucket excavating operation, the pilot pressure enters through port PAcs and the bucket spool transfers in the half stroke not full stroke. Therefore, the pressurized oil entering through port P1 flows to the boom 1 spool (303) preferentially to the bucket spool (304) to make the boom hoisting operation most preferential.



380A2MC23

## (2) Bucket releasing operation

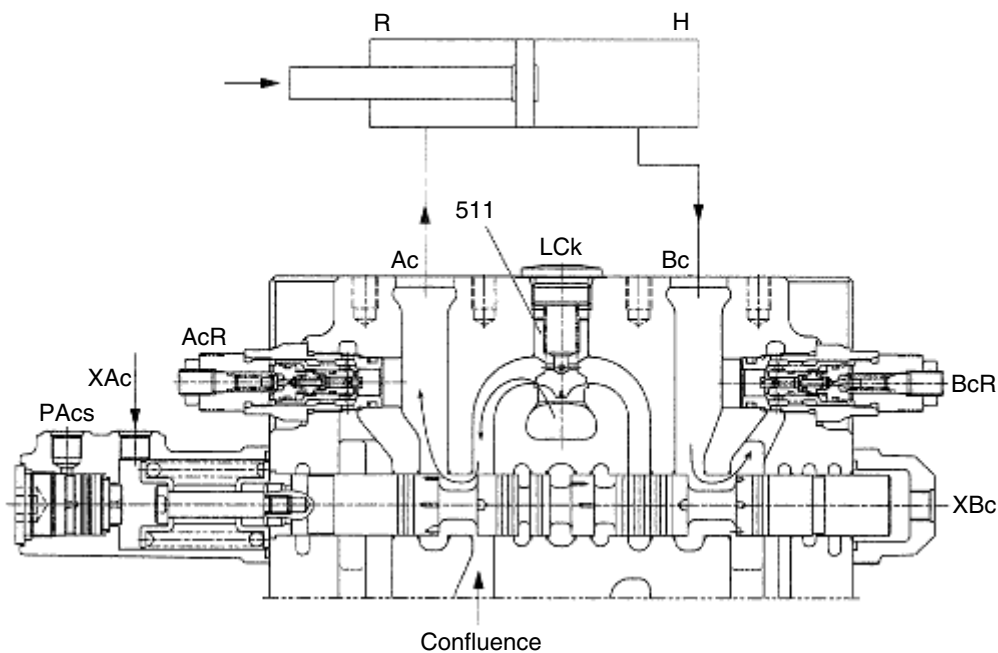
### ① Pilot circuit

Since the bucket spool (304) transfers and shuts off the side-bypass path, the pressure at port Px increases. Then, the pressure enters also through port XBp2.

### ② Main circuit

During the bucket releasing operation, the pilot pressure enters through port XAc and transfers the bucket spool (304) in the right direction in figure. The pressurized oil entering through port P1 passes through the main path (1) and flows through the bypass circuit (2), but the bypass circuit is shut off due to transfer of the bucket spool (304). Therefore, the pressurized oil flows into the parallel circuit, pushes open the check valve (511), and flows through the U-shaped path to the bucket spool (304). Then, it flows through the periphery of the bucket spool (304) to port Ac and is supplied to the bucket cylinder rod side (R).

On the other hand, the return oil from the bucket cylinder head side (H) enters through port Bc, passes around the periphery of the spool, and returns to the hydraulic oil tank through the tank ports (R1), (R3).



380A2MC24

### ③ Bucket confluence

During the bucket excavating or releasing operation, the pilot pressure enters also through port XBp2 and transfers the bypass-cut spool (310). The pressurized oil entering through port P2 passes through the main path (3) and flows through the bypass circuit (4), but the bypass circuit is shut off due to transfer of the bypass-cut spool (310). Therefore, the pressurized oil pushes open the check valve (515), and flows through inside path and the U-shaped path to the bucket spool (304).

## 6) SWING OPERATION

### (1) Independent swing operation

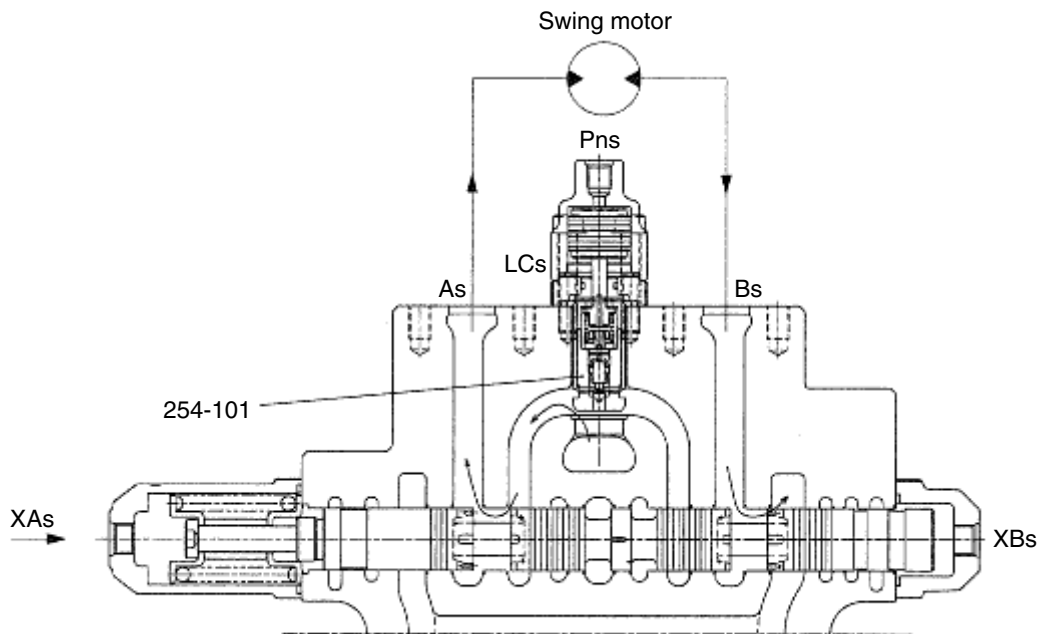
#### ① Pilot circuit

Since the swing spool (305) transfers and shuts off the side-bypass path, the pressure at port Px increases.

#### ② Main circuit

During the swing operation, the pilot pressure enters through port XAs (or XBs) and transfers the swing spool (305). The pressurized oil entering through port P2 passes through the main path (3) and flows through the bypass circuit (4), but the bypass circuit (4) is shut off due to transfer of the swing spool (305). Therefore, the pressurized oil flows into the parallel circuit, pushes open the logic poppet (254-101), and flows through the U-shaped path to the swing spool (305). Then, it flows through the periphery of the spool to port As (or Bs) and is supplied to the swing motor.

On the other hand, the return oil from the swing motor enters port Bs (or As) and returns to the hydraulic oil tank through the tank ports (R1), (R3).



380A2MC25

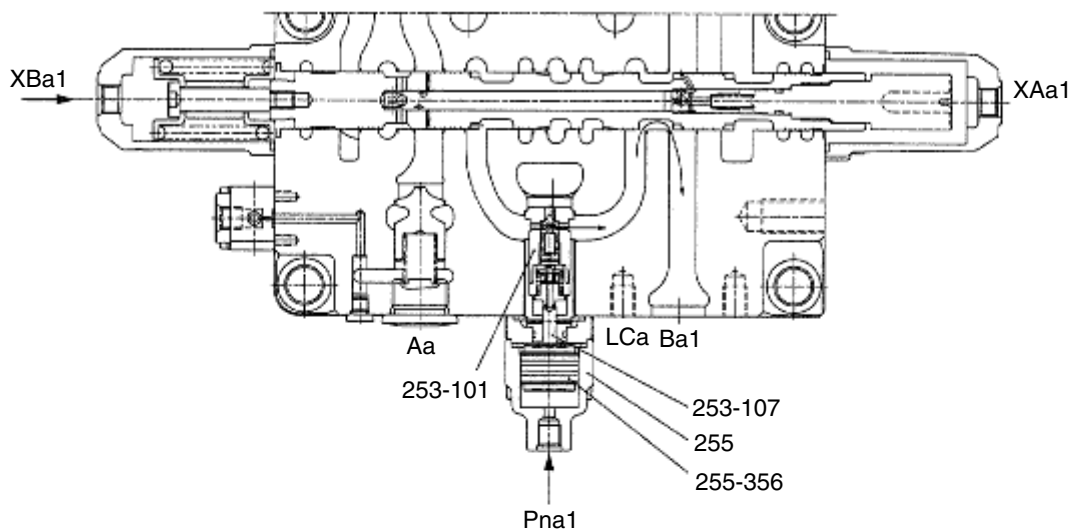
## (2) Swing priority function

The following is the case of making the swing operation prior to the arm excavating operation.

### ① Main circuit

During both the arm excavating operation and the swing operation, the swing pilot pressure enters through ports Pna1 of the logic poppet (255), and transfers the piston (255-356) and the spool (253-107) upward in figure. Therefore, the lift of the poppet (253-101) is limited, and the passage from the parallel circuit to the U-shaped path is restricted. As a result, the pressurized oil flows to the swing spool preferentially to the arm 1 spool to make the swing operation prior.

Similarly, in case the pilot pressure is applied to port Pns of the logic poppet (255), the lift of the poppet (254-101) is limited, and the boom hoisting operation is made prior to the swing operation.



380A2MC26

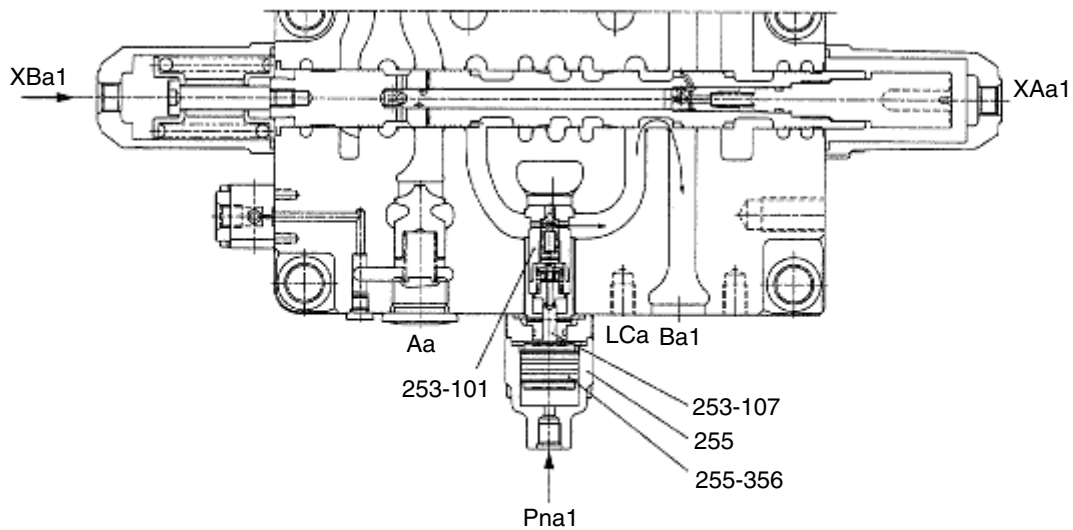
## (2) Swing priority function

The following is the case of making the swing operation prior to the arm excavating operation.

### ① Main circuit

During both the arm excavating operation and the swing operation, the swing pilot pressure enters through ports Pna1 of the logic poppet (255), and transfers the piston (255-356) and the spool (253-107) upward in figure. Therefore, the lift of the poppet (253-101) is limited, and the passage from the parallel circuit to the U-shaped path is restricted. As a result, the pressurized oil flows to the swing spool preferentially to the arm 1 spool to make the swing operation prior.

Similarly, in case the pilot pressure is applied to port Pns of the logic poppet (255), the lift of the poppet (254-101) is limited, and the boom hoisting operation is made prior to the swing operation.



380A2MC26

## 7) OPTION OPERATION

This spool is used for controlling the optional attachments like a nibbler.

### (1) Option operation

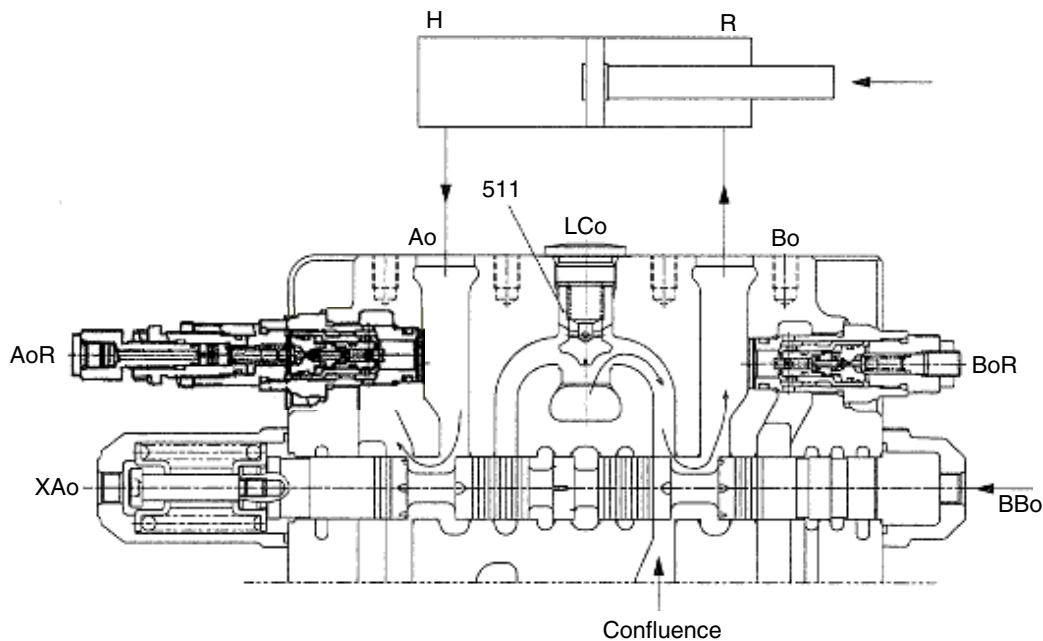
#### ① Pilot circuit

Since the side bypass sections of both travel spools (301) shut off and the side bypass section of the downstream-side of swing spool shuts off, the pilot pressure from the port PG enters through the port PTb to transfer the travel straight spool (308).

#### ② Main circuit

During the swing operation, the pilot pressure enters through port XAs (or XBs) and transfers the swing spool (305). The pressurized oil entering through port P2 passes through the main path (3) and flows through the bypass circuit (4), but the bypass circuit (4) is shut off due to transfer of the swing spool (305). Therefore, the pressurized oil flows into the parallel circuit, pushes open the logic poppet (254-101), and flows through the U-shaped path to the swing spool (305). Then, it flows through the periphery of the spool to port As (or Bs) and is supplied to the swing motor.

On the other hand, the return oil from the swing motor enters port Bs (or As) and returns to the hydraulic oil tank through the tank ports (R1), (R3).



400SA2MC27

### (2) Option confluence

In order to use the option confluence, the pilot pressure enters through port XBp1 and transfers the bypass-cut spool (310). The pressurized oil entering through port P1 passes through the main path (1) and flows through the bypass circuit (2), but the bypass circuit (2) is shut off due to transfer of the bypass-cut spool (310). Therefore the pressurized oil pushes open the check valve (515), and flows through the inside path and the U-shaped path to the option spool (309).



## 8) TRAVEL STRAIGHT OPERATION

Simultaneous operating of both travel spools (301) and other spool makes the operation useful. The following is the case where both travel spools (301) and swing spool (305) are changed over. (the pilot ports XAtL, XAtR and XAs are pressurized.)

### ① Pilot circuit

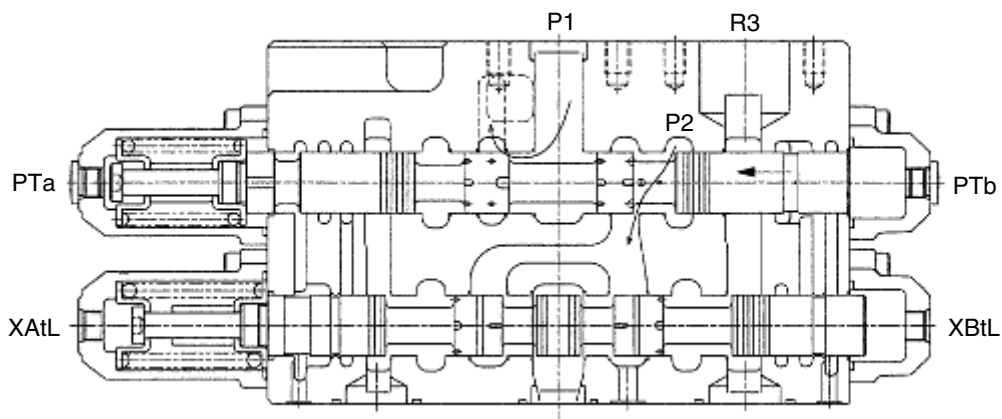
Since the side bypass sections of both travel spools (301) shut off and the side bypass section of the downstream-side of swing spool shuts off, the pilot pressure from the port PG enters through the port PTb to transfer the travel straight spool (308).

### ② Main circuit

After changeover of the travel straight spool (308), the port P2 and both travel spools (301) are connected preferentially and the port P1 and the parallel paths of swing, boom 2, option and arm 1 / boom 1, bucket and arm 2 are connected preferentially. Therefore, the pressurized oil entering through port P2 passes through mainly ports AtL and Atr, and flows to both travel motors separately.

On the other hand, the pressurized oil entering through port P1 flows to port As and is supplied to the swing motor.

When the pressure of port P2 is lower than the pressure of port P1, the part of oil entering through port P1 flows into Port P2 side. Therefore, it prevents the rapid slowdown of travel.



380A2MC28

## 9) FUNCTION OF LOCK VALVE

The lock valve (252) is installed between the arm cylinder rod side (R) and the arm 1 spool (302). It decreases the leakage by the pressure of the cylinder.

Similarly, another lock valve (252) is installed between the boom cylinder head side (H) and the boom 1 spool (303) and decreases the leakage by the pressure of the cylinder.

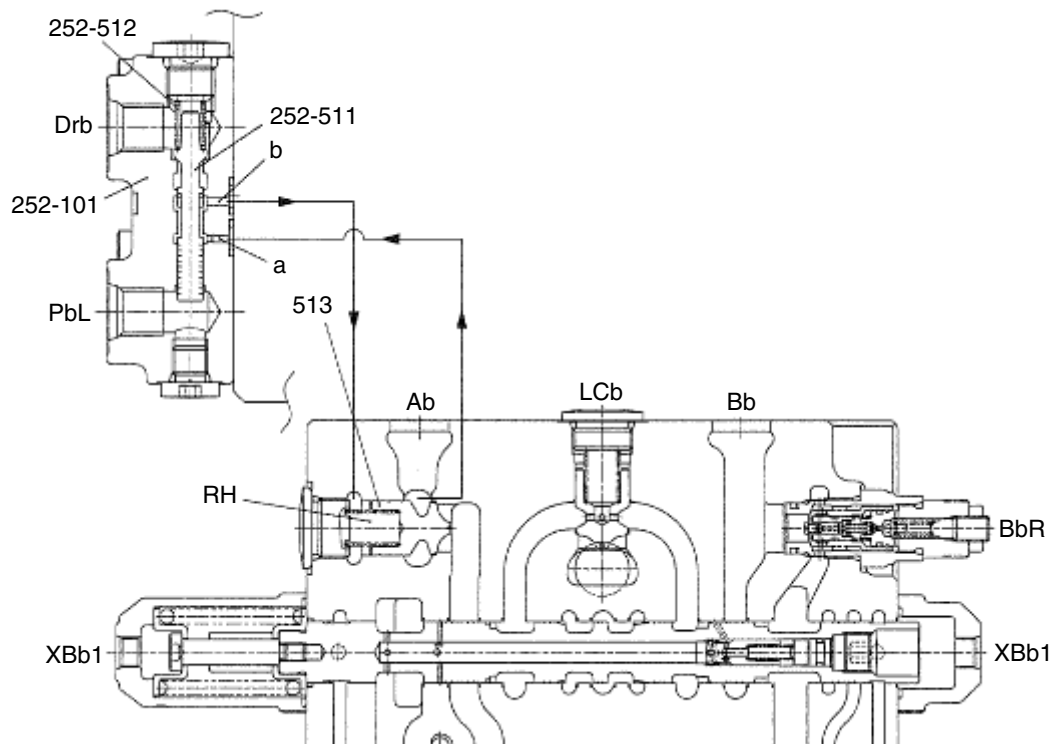
The following is the case of the boom cylinder head side (H).

(the case of the arm cylinder rod side (R) is in the same way.)

### (1) Neutral positions of spools

During the boom 1 spool (303), boom 2 spool (307) are in the neutral position, the spool (252-511) in the lock valve is kept in the position shown in figure by the force of the spring (252-512). The spool (252-511) is pushed to the seat of the lock valve (252-101).

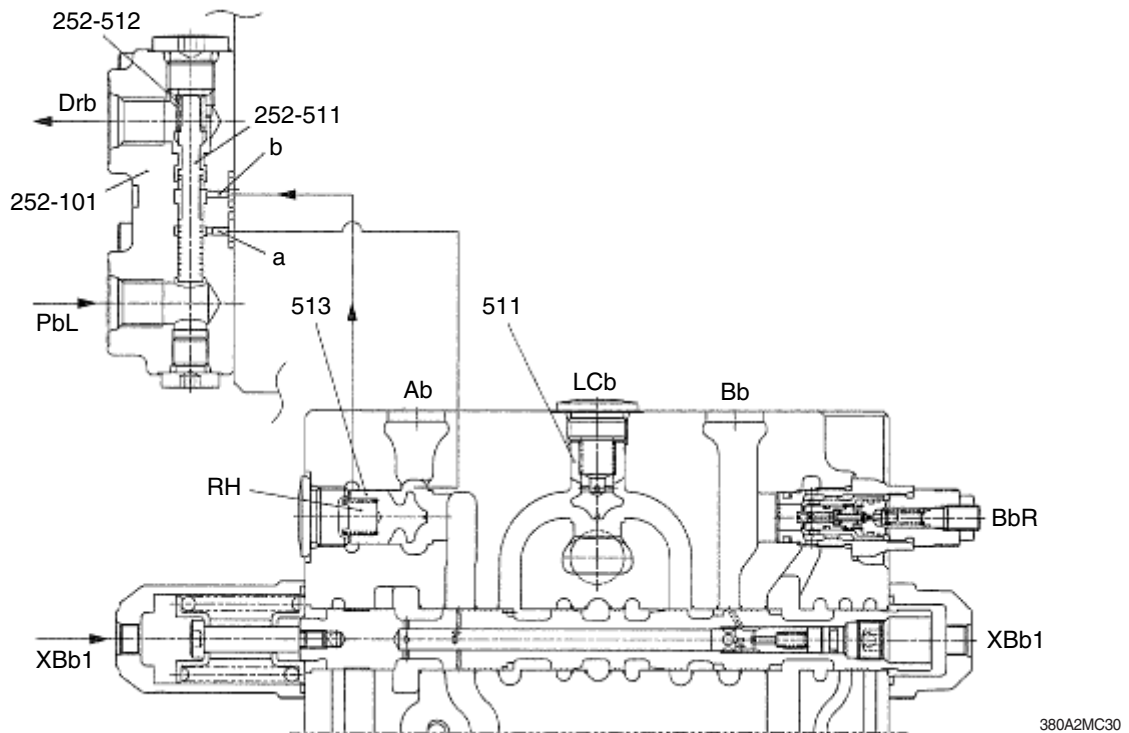
In this position, pressurized oil from the boom cylinder head side (H) enters through hole (a), the periphery of the spool (252-511) in the lock valve and hole (b), and it pushes the poppet (513) to the casing seat, and the leakage is decreased.



380A2MC29

## (2) Boom lowering operation

During the boom lowering operation, pilot pressure enters through port PbL, XBb1 and XBb2. Pilot pressure transfers the spool (252-511) in the lock valve in the top direction in figure. By the transfer of the spool (252-511), firstly the hole (a) is blocked and pressurized oil from the boom cylinder head side (H) does not enter to spring chamber (RH). Secondly, the oil in spring chamber (RH) enters through hole (b) and flows to drain circuit. Therefore, the poppet (513) is lifted by the pressure of the boom cylinder head side (H) and the function of the lock valve (252) is released.



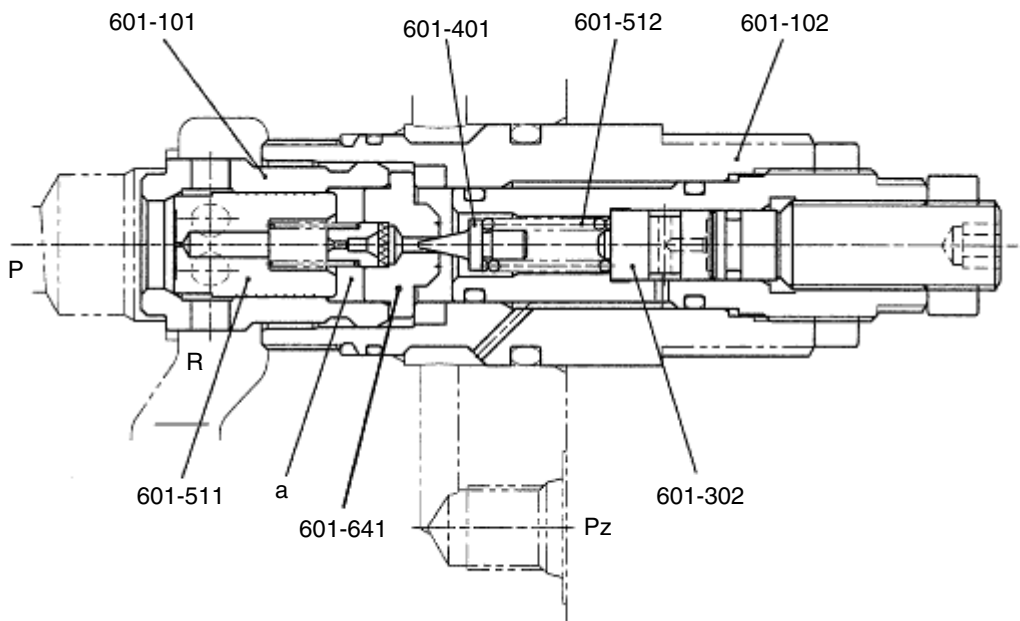
## (3) Boom hoisting operation

During the boom hoisting operation, the pilot pressure enters through ports XAb1, XAb2. The oil flowing from the boom 1 spool (303) and the boom 2 spool (307) pushes open the poppet (513) and flows to port Ab.

## 10) FUNCTION OF MAIN RELIEF VALVEN

The main relief valve (601) is fitted in the casing A (101) and functions as follows.

- (1) The hydraulic oil is filled up in the inside space chamber (a) from the path (P) through a hole of the body (601-101) and a restriction of the plunger (601-511), and seats the plunger (601-511) against body (601-101) securely.
- (2) When the pressure in the path (P) becomes equal to the set load of the spring (601-512), the poppet (601-401) opens to make the hydraulic oil flow through a hole of the seat (601-641), around the poppet (601-401) and into the low pressure path (R).
- (3) Opening of the poppet (601-401) causes the pressure in the chamber (a) to fall and the plunger (601-511) to open. As the result the pressurized oil in the path (P) runs into the low pressure path (R) directly.
- (4) When the pressurized oil higher than pressure 3MPa enters through the port Pz, it pushes the piston (601-302) to change the relief set pressure of the spring (601-512) to the high pressure.



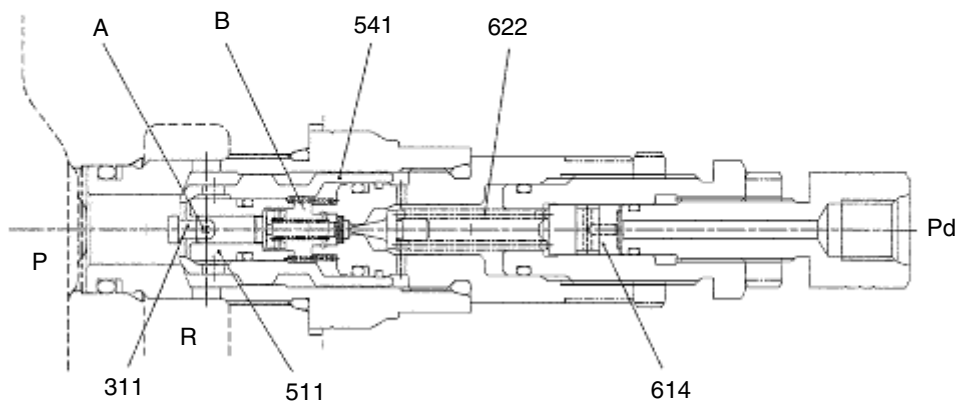
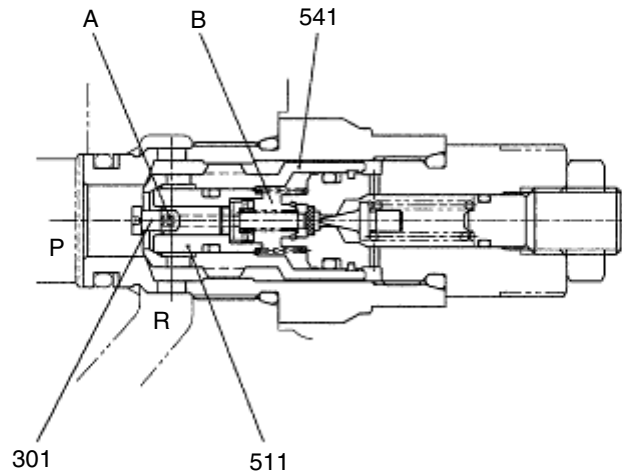
380A2MC31

## 11) FUNCTION OF PORT RELIEF VALVE

The port relief valve is fitted between the cylinder port and low-pressure path. In addition to the relief valve, this serves also as an anti-cavitation check valve, and functions as follows:

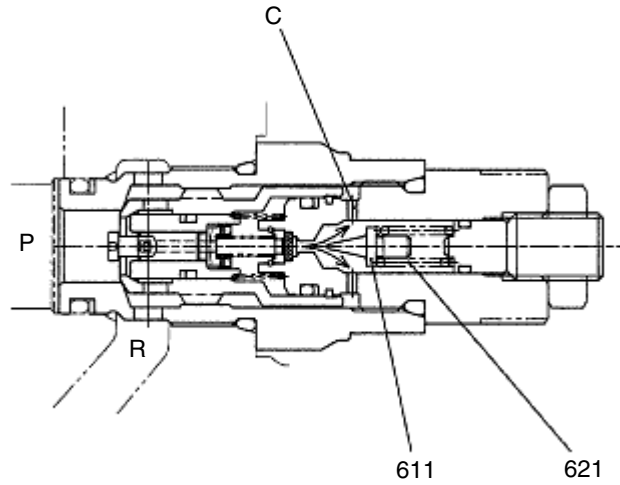
### (1) Function as relief valve

- ① The pressurized oil passes through Hole A of the piston (301), is filled up in chamber B of the inside space, and seat the plunger (511) against the seat (541) securely.



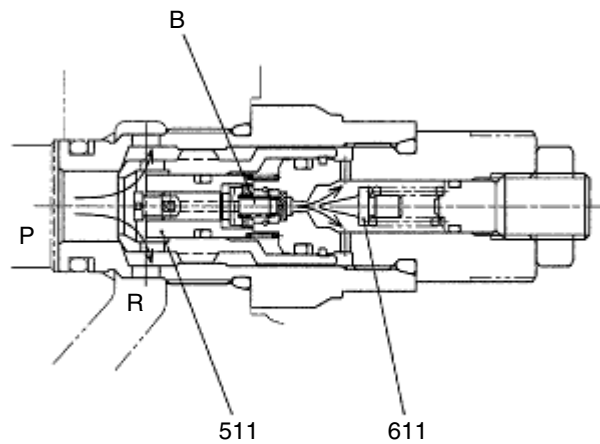
380A2MC32

- ② When the pressure in the path (P) becomes equal to the set pressure of the spring (621), the pressurized oil pushes open the poppet (611), flows around it, and flows to the low pressure path (R) through hole C.



380A2MC33

- ③ Opening of the poppet (611) causes the pressure in chamber B to fall and the plunger (511) to open. As the result the pressurized oil in the path (P) runs into the low pressure path (R) directly.

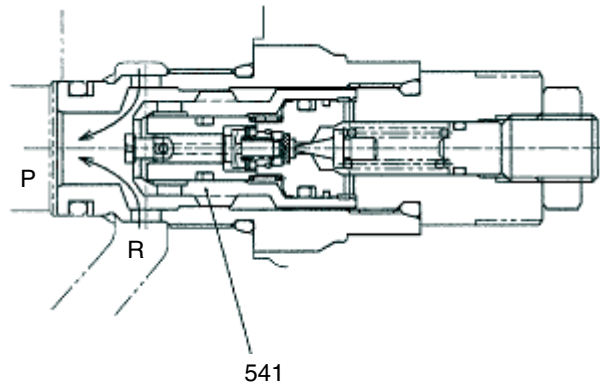


380A2MC34

## (2) Function as anti-cavitation check valve

When any negative pressure exists in the path (P), the oil is supplied through the path (R). When the pressure at (R) becomes higher than that in the path (P), the seat (541) moves in the right direction.

Then, sufficient oil passes around the seat (541) from the path (R) to the path (P) and prevents cavitation.



380A2MC35

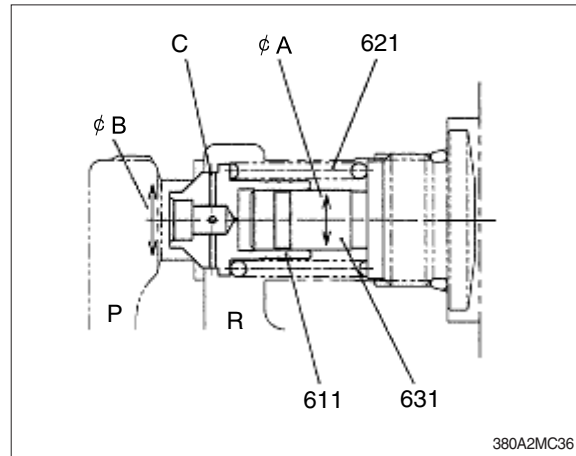
## (12) FUNCTION OF NEGATIVE CONTROL RELIEF VALVE

The negative control relief valve is fitted between the downstream of the center bypass path and low-pressure path, and functions as follows:

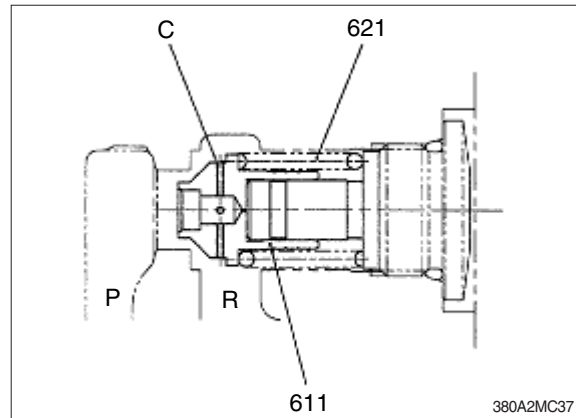
- ① When the pressure in the path (P) falls below the set level of the spring (621), the poppet (611) is in the condition shown in the figure.

The pressure acting area of the poppet (611) is reduced to  $(\phi B - \phi A)$ , as the area  $\phi B$  is cancelled by the area  $\phi A$  of the damping rod (631).

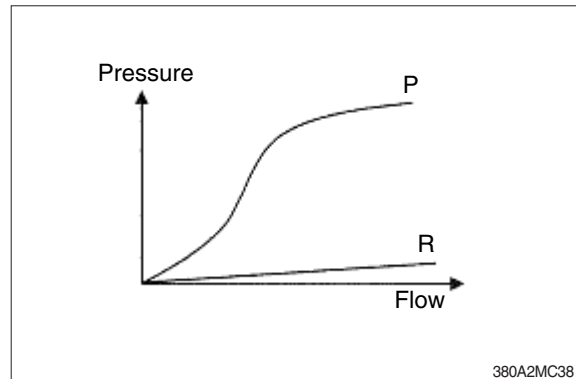
In this condition, the pressurized oil in the path (P) runs out to the path (R) through the orifice (C).



- ② When the pressure in the path (P) goes over the set pressure of the spring (621), the poppet (611) opens as shown in the figure. Then, the pressurized oil in the port P passes around the outside of the poppet (611) and flows to the low-pressure path (R).



The relation between the flow rate Q and pressure P of the hydraulic oil that flows from the path (P) to the low-pressure path (R) is as shown in figure.



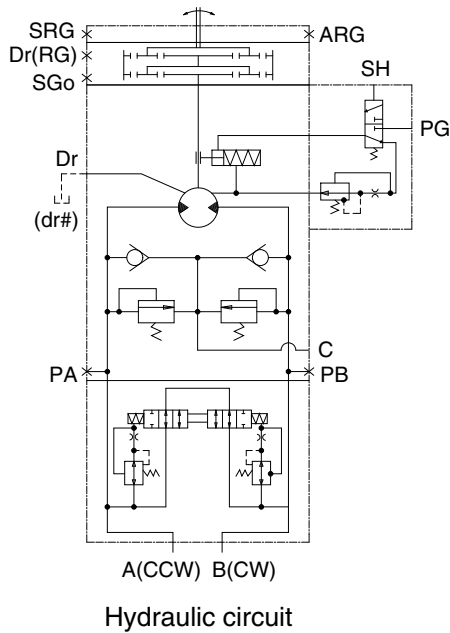
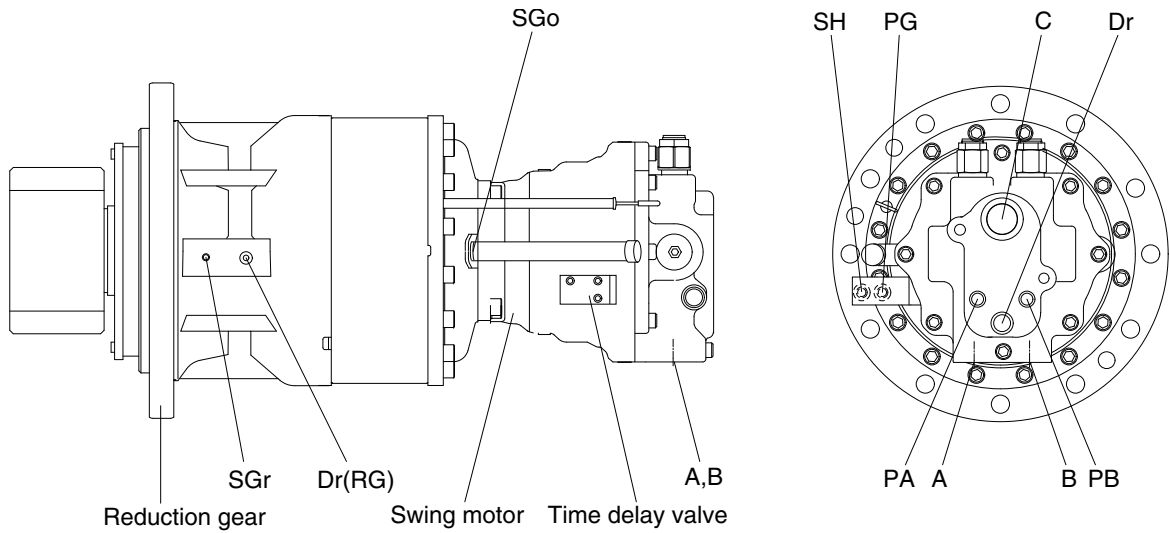


## GROUP 3 SWING DEVICE

### 1. STRUCTURE (TYPE 1)

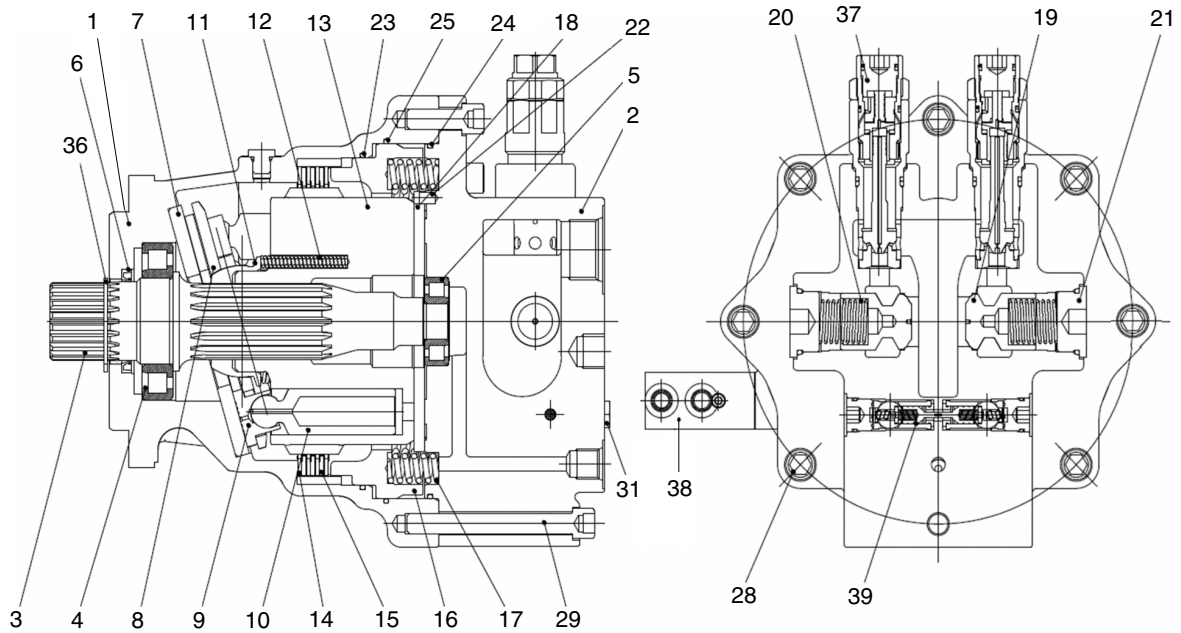
Swing device consists swing motor, swing reduction gear.

Swing motor include mechanical parking valve, relief valve, make up valve and time delay valve.



Port	Port name	Port size
A	Main port	SAE 1"
B	Main port	SAE 1"
DB	Drain port	PF 1/2
C	Make up port	PF 1 1/4
SH	Brake release pilot port	PF 1/4
PG	Brake release stand by port	PF 1/4
PA, PB	Gauge port	PF 1/4
SGr	Grease filling port	PT 1/8
Dr (R/G)	Gear oil drain port	PT 1/2
SGo	Gear oil filling port	PT 3/4

## 1) SWING MOTOR (TYPE 1)



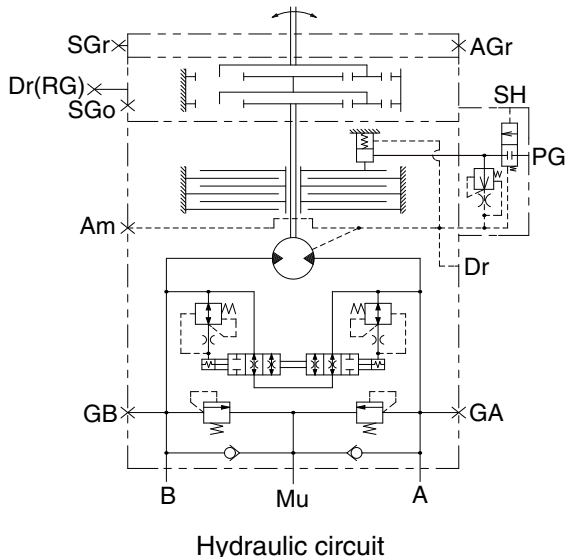
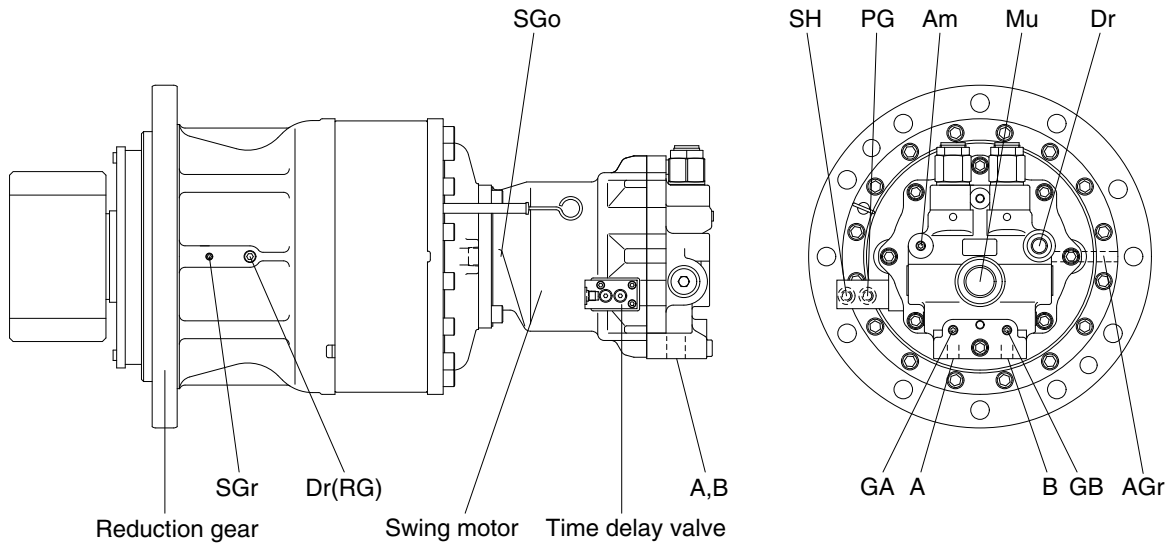
380A8SM05

1	Casing	12	Cylinder spring	23	O-ring
2	Valve casing	13	Cylinder block	24	O-ring
3	Drive shaft	14	Friction plate	25	O-ring
4	Roller bearing	15	Separation plate	28	Socket bolt
5	Roller bearing	16	Brake piston	29	Socket bolt
6	Oil seal	17	Brake spring	30	Socket bolt
7	Shoe plate	18	Valve plate	31	VP plug assy
8	Retainer plate	19	Plunger	36	Snap ring
9	Shoe	20	Check spring	37	Relief valve
10	Piston	21	RO plug assy	38	Brake valve
11	Thrust ball	22	Pin	39	Reactionless valve

## STRUCTURE (TYPE 2)

Swing device consists swing motor, swing reduction gear.

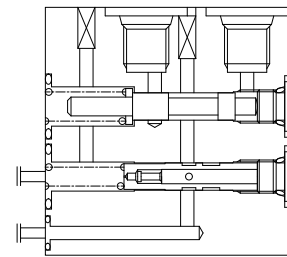
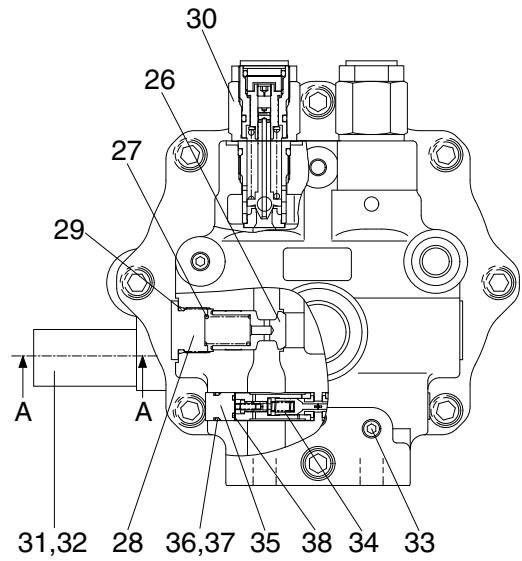
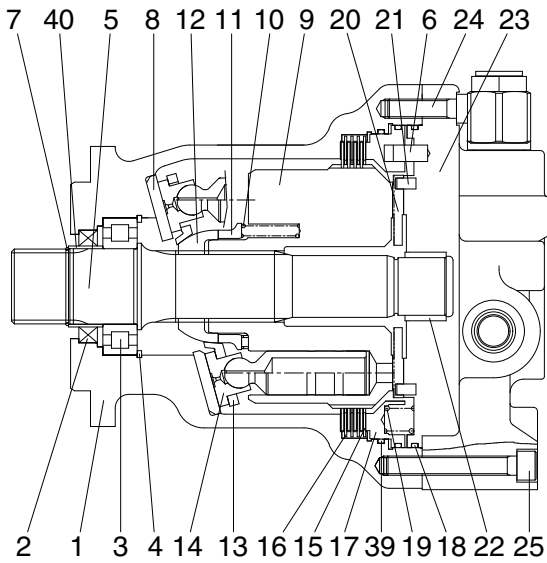
Swing motor include mechanical parking valve, relief valve, make up valve and time delay valve.



Port	Port name	Port size
A	Main port	SAE 1"
B	Main port	SAE 1"
Dr	Drain port	PF 1/2
Mu	Make up port	PF 1 1/4
SH	Brake release pilot port	PF 1/4
PG	Brake release stand by port	PF 1/4
GA, GB	Gauge port	PF 1/4
Am	Motor air bleed port	PF 1/4
AGr	R/G air bleed port	PT 1/8
SGr	Grease filling port	PT 1/8
Dr(R/G)	Gear oil drain port	PT 1/2
SGo	Gear oil filling port	PT 3/4

38092SM01A

## 1) SWING MOTOR (TYPE 2)

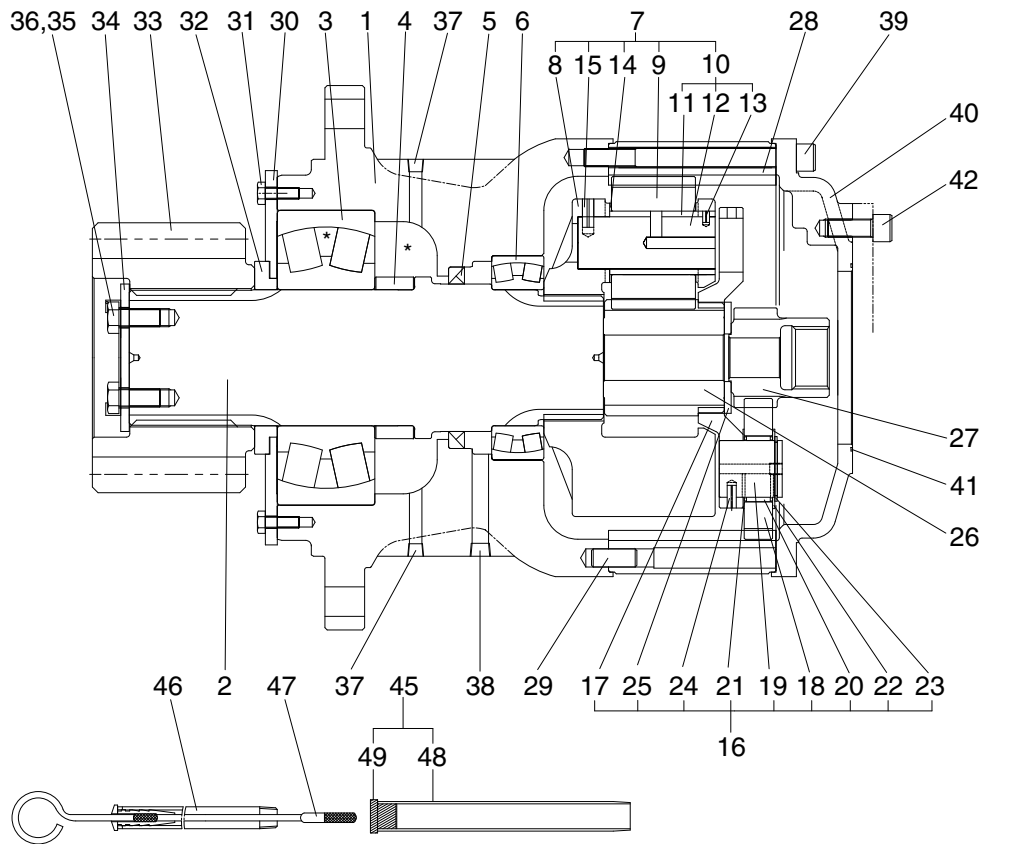


SECTION A-A

38092SM02

1	Body	15	Friction plate	29	O-ring
2	Oil seal	16	Plate	30	Relief valve assy
3	Roller bearing	17	Brake piston	31	Time delay valve
4	Snap ring	18	O-ring	32	Wrench bolt
5	Shaft	19	Spring	33	Plug
6	Pin	20	Valve plate	34	Swing reactionless valve assy
7	Stop ring	21	Pin	35	Plug
8	Shoe plate	22	Needle bearing	36	O-ring
9	Cylinder block	23	Rear cover	37	Back up ring
10	Spring	24	Wrench bolt	38	O-ring
11	Ball guide seat	25	Wrench bolt	39	O-ring
12	Ball guide	26	Poppet	40	Bushing
13	Set plate	27	Spring		
14	Piston assy	28	Plug		

## 2) REDUCTION GEAR



380A2SM03

1	Casing	17	Carrier 1	33	Pinion gear
2	Drive shaft	18	Planetary gear 1	34	Lock plate
3	Taper roller bearing	19	Pin 1	35	Hexagon bolt
4	Spacer ring	20	Needle cage	36	Lock washer
5	Oil seal	21	Side plate 1	37	Plug
6	Taper roller bearing	22	Side plate 2	38	Plug
7	Carrier assy 2	23	Stop ring	39	Socket bolt
8	Carrier 2 assy	24	Spring pin	40	Cover
9	Planetary gear 2	25	Thrust ring	41	O-ring
10	Pin assy 2	26	Sun gear 2	42	Hexagon socket bolt
11	Pin 2 assy	27	Sun gear 1	45	Air breather assy
12	Bushing 2	28	Ring gear	46	Gauge pipe
13	Spring pin	29	Knock pin	47	Gauge bar
14	Thrust washer	30	Cover plate	48	Air breather post
15	Spring pin	31	Hexagon bolt	49	Air breather cap
16	Carrier assy 1	32	Spacer		

## 2. FUNCTION

### 1) ROTARY PART

When high pressurized oil enters a cylinder through port (a), which is the inlet of valve plate (1), hydraulic pressure acting on the piston causes axial force  $F$ . The pressure force  $F$  works via the piston (2) upon the retainer plate (3) which acts upon the shoe plate (4) via an hydrostatic bearing. Force  $F_1$  perpendicular to shoe plate (4) and force  $F_2$  perpendicular to cylinder center.

Being transferred to the cylinder block (5) through piston, force  $F_2$  causes rotational moment at surroundings of cylinder.

Since cylinder block has 9 equidistantly arrayed pistons, rotational torque is transmitted to cylinder shaft in order by several pistons connected to the inlet port of high pressurized oil. When the direction of oil flow is reversed, rotational direction of cylinder is also reversed. Output torque is given by the equation.

$$T = \frac{p \times q}{2\pi} , q = Z \cdot A \cdot \text{PCD} \cdot \tan \theta , F_1 = \frac{F}{\cos \theta} , F_2 = F \tan \theta , S = \text{PCD} \times \tan \theta$$

Where  $p$  : Effective difference of pressure (kgf/cm<sup>2</sup>)

$q$  : Displacement (cc/rev)

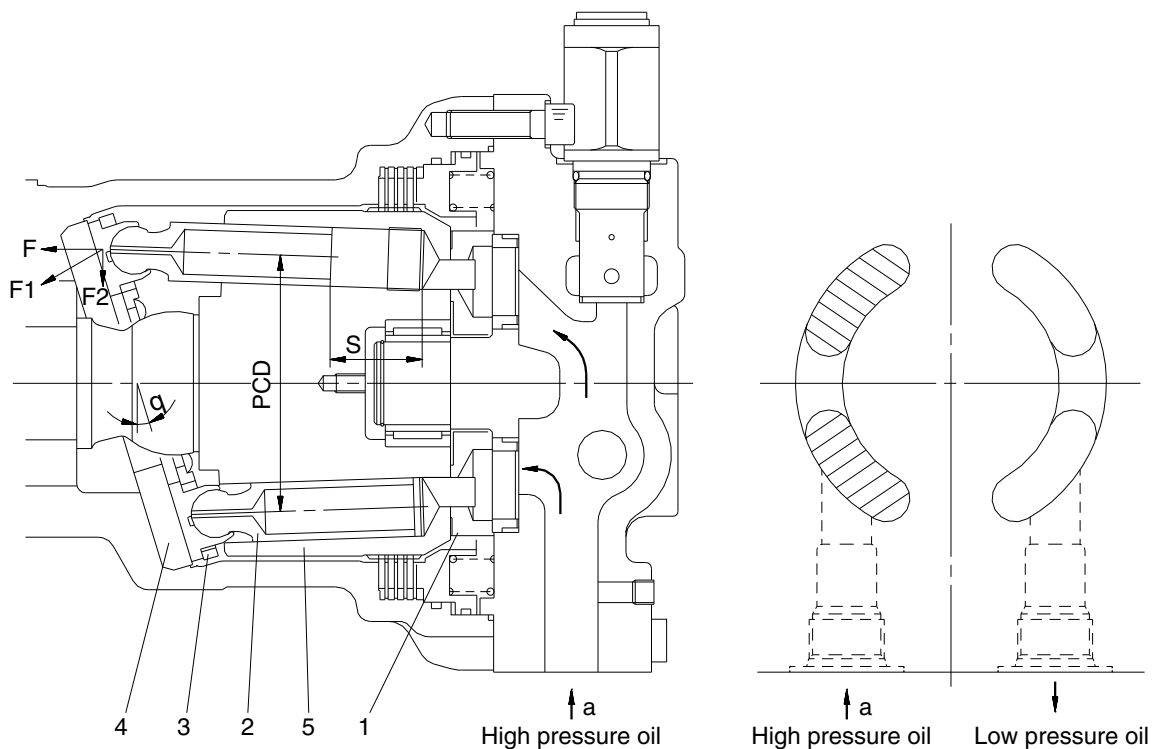
$T$  : Output torque (kgf · cm)

$Z$  : Piston number

$A$  : Piston area (cm<sup>2</sup>)

$\theta$  : Tilting angle of shoe plate (degree)

$S$  : Piston stroke (cm)



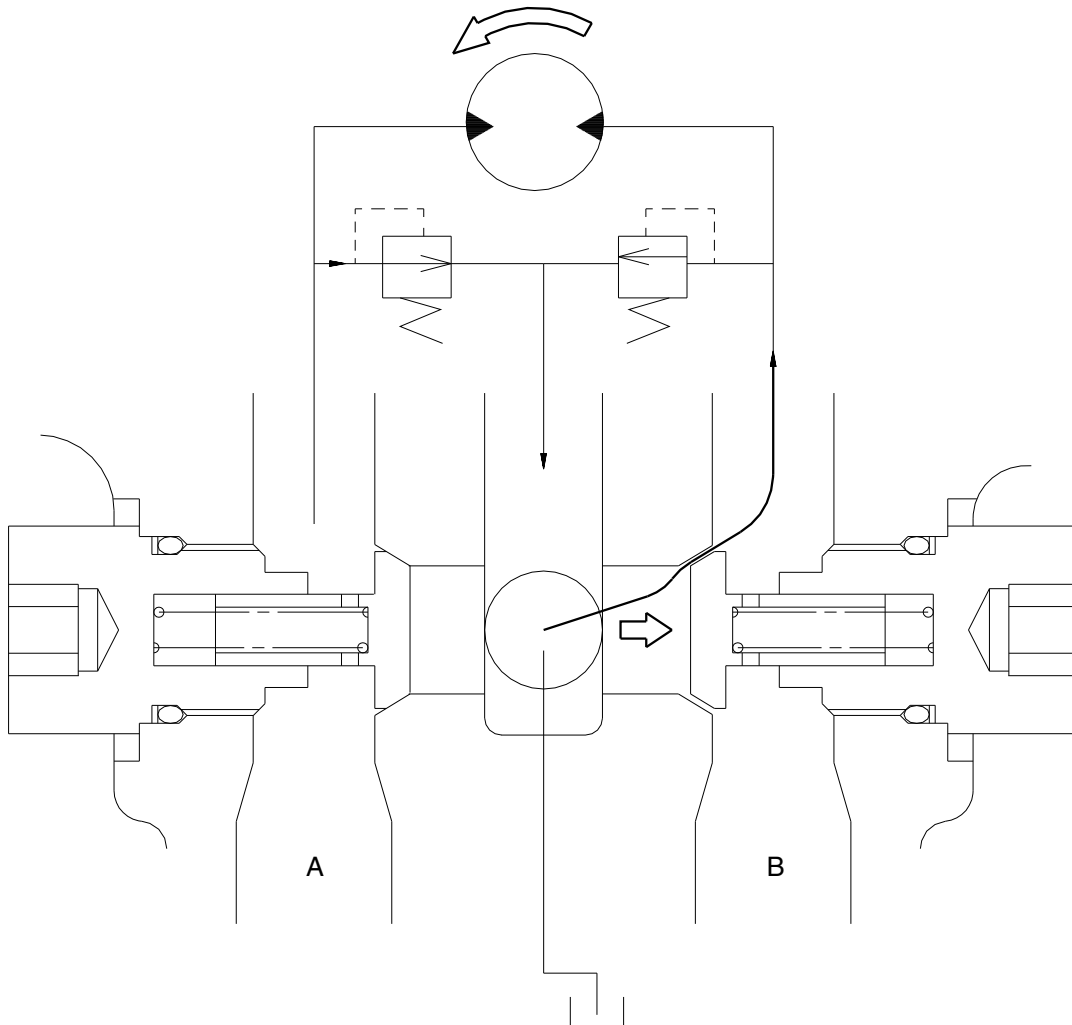
## 2) MAKE UP VALVE

In the system using this type of motor, there is no counter balance functioning valve and there happens the case of revolution exceeding hydraulic supply of motor. To prevent the cavitation caused by insufficient oil flow there is a make up valve to fill up the oil insufficiency.

A make up valve is provided immediately before the port leading to the hydraulic oil tank to secure feed pressure required when the hydraulic motor makes a pumping action. The boost pressure acts on the hydraulic motor's feed port via the make up valve.

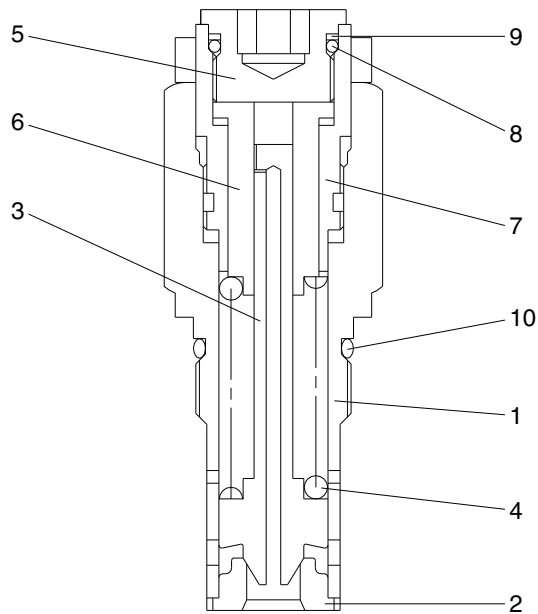
Pressurized oil into the port B, the motor rotate counterclockwise.

If the plunger of MCV moves neutral position, the drain oil from Mu port run into motor via right make up valve, which prevent the cavitation of motor.



36072SM05

### 3) RELIEF VALVE



- 1 Body
- 2 Seat
- 3 Plunger
- 4 Spring
- 5 Adjusting screw
- 6 Piston
- 7 Sleeve
- 8 O-ring
- 9 Back up ring
- 10 O-ring

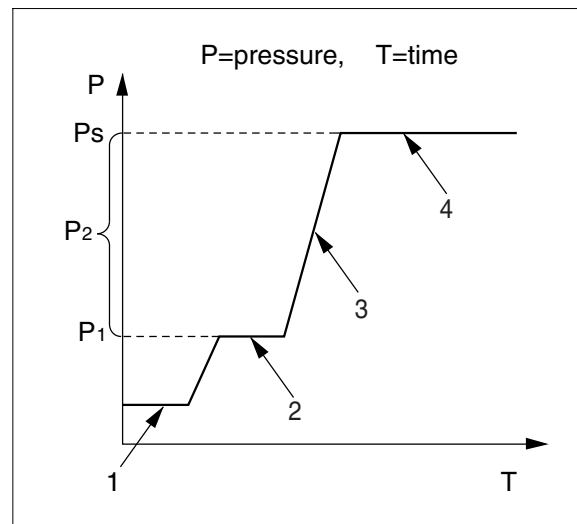
36072SM06

#### (1) Construction of relief valve

The valve casing contains two cartridge type relief valves that stop the regular and reverse rotations of the hydraulic motor. The relief valves relieve high pressure at start or at stop of swing motion and can control the relief pressure in two steps, high and low, in order to insure smooth operation.

#### (2) Function of relief valve

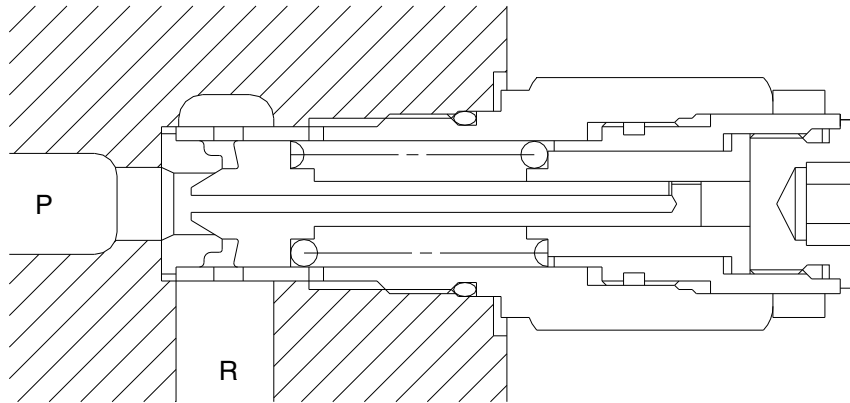
Figure illustrates how the pressure acting on the relief valve is related to its rising process. Here is given the function, referring to the figure following page.



2-51(2) [360-7]



① Ports (P, R) at tank pressure.

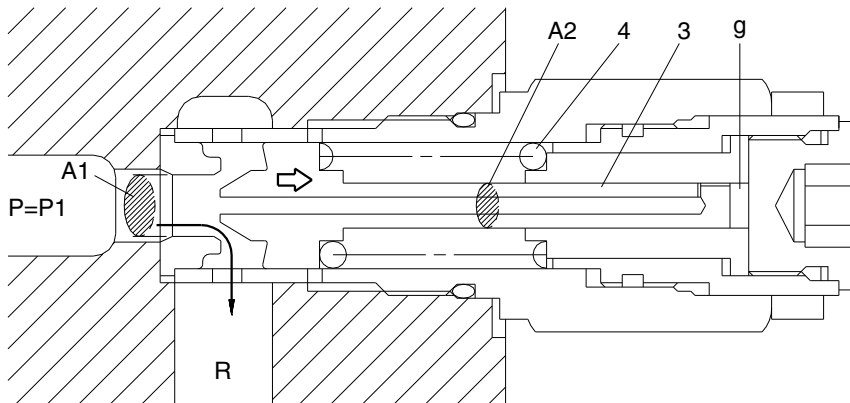


36072SM07

② When hydraulic oil pressure ( $P \times A_1$ ) reaches the preset force ( $F_{SP}$ ) of spring (4), the plunger (3) moves to the right as shown.

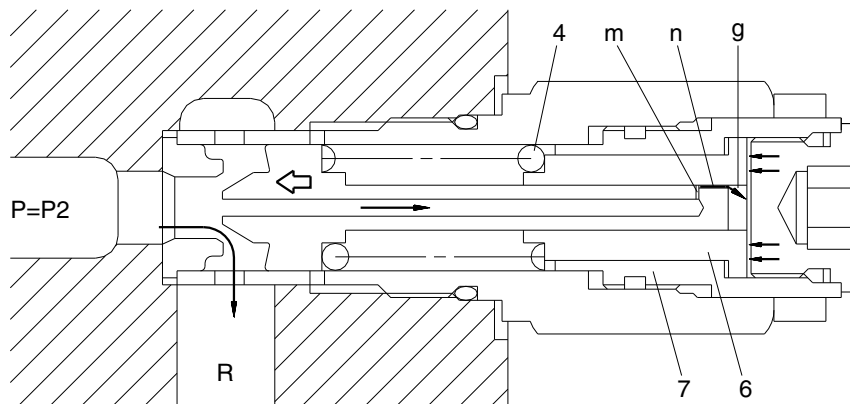
$$P_1 \times A_1 = F_{SP} + P_g \times A_2$$

$$P_1 = \frac{F_{SP} + P_g \times A_2}{A_1}$$



36072SM08

- ③ The oil flow chamber g via orifice m and n. When the pressure chamber g reaches the preset force ( $F_{sp}$ ) of spring (4), the piston (6) moves left and stop the piston (6) hits the bottom of sleeve (7).

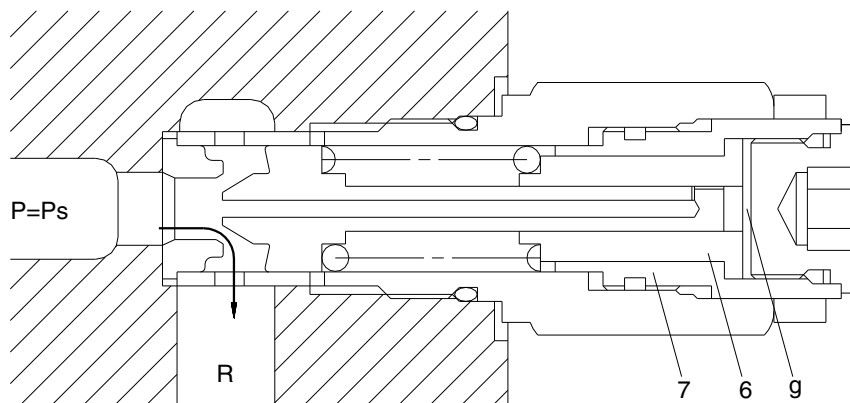


36072SM09

- ④ When piston (6) hits the end of sleeve (7), it stops moving to the left any further. As the result, the pressure in chamber (g) equals ( $P_s$ ).

$$P_s \times A_1 = F_{SP} + P_s \times A_2$$

$$P_s = \frac{F_{sp}}{A_1 - A_2}$$

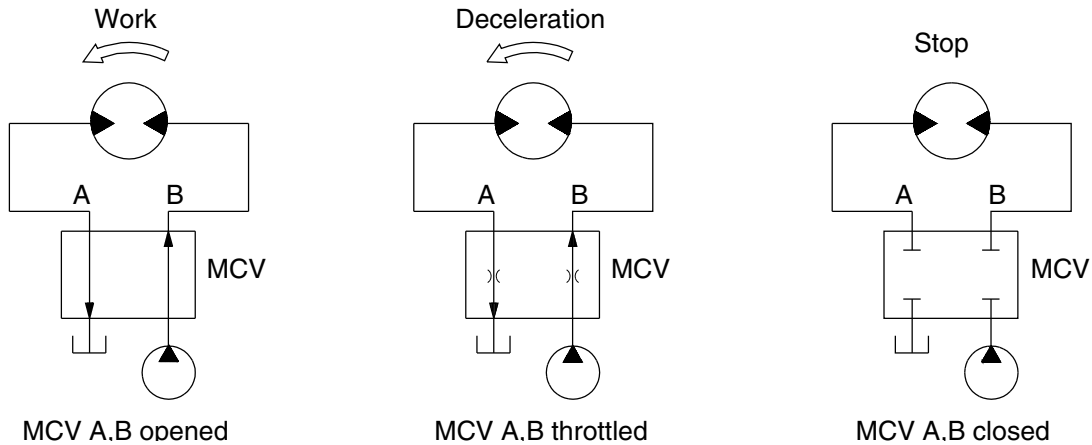


36072SM10

## 4) BRAKE SYSTEM

### (1) Control valve swing brake system

This is the brake system to stop the swing motion of the excavator for during operation. In this system, the hydraulic circuit is throttled by the swing control valve, and the resistance created by this throttling works as a brake force to slow down the swing motion.



R130SM05

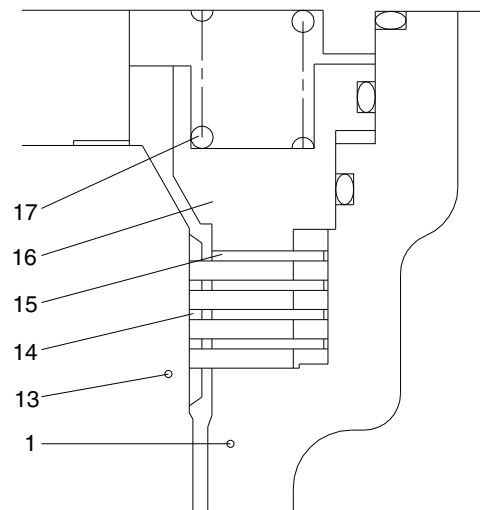
### (2) Mechanical swing parking brake system

The mechanical swing parking brake system is installed to prevent the upper structure from swinging downhill because of its own weight when the excavator is parked on a slope since it completely eliminates the hydraulic drift of swing motion while the excavator is on a slope, work can be done more easily and safely.

#### ① Brake assembly

Circumferential rotation of separate plate (15) is constrained by the groove located at casing (1). When housing is pressed down by brake spring (17) through friction plate (14), separate plate (15) and brake piston (16), friction force occurs there.

Cylinder block (13) is constrained by this friction force and brake acts, while brake releases when hydraulic force exceeds spring force.

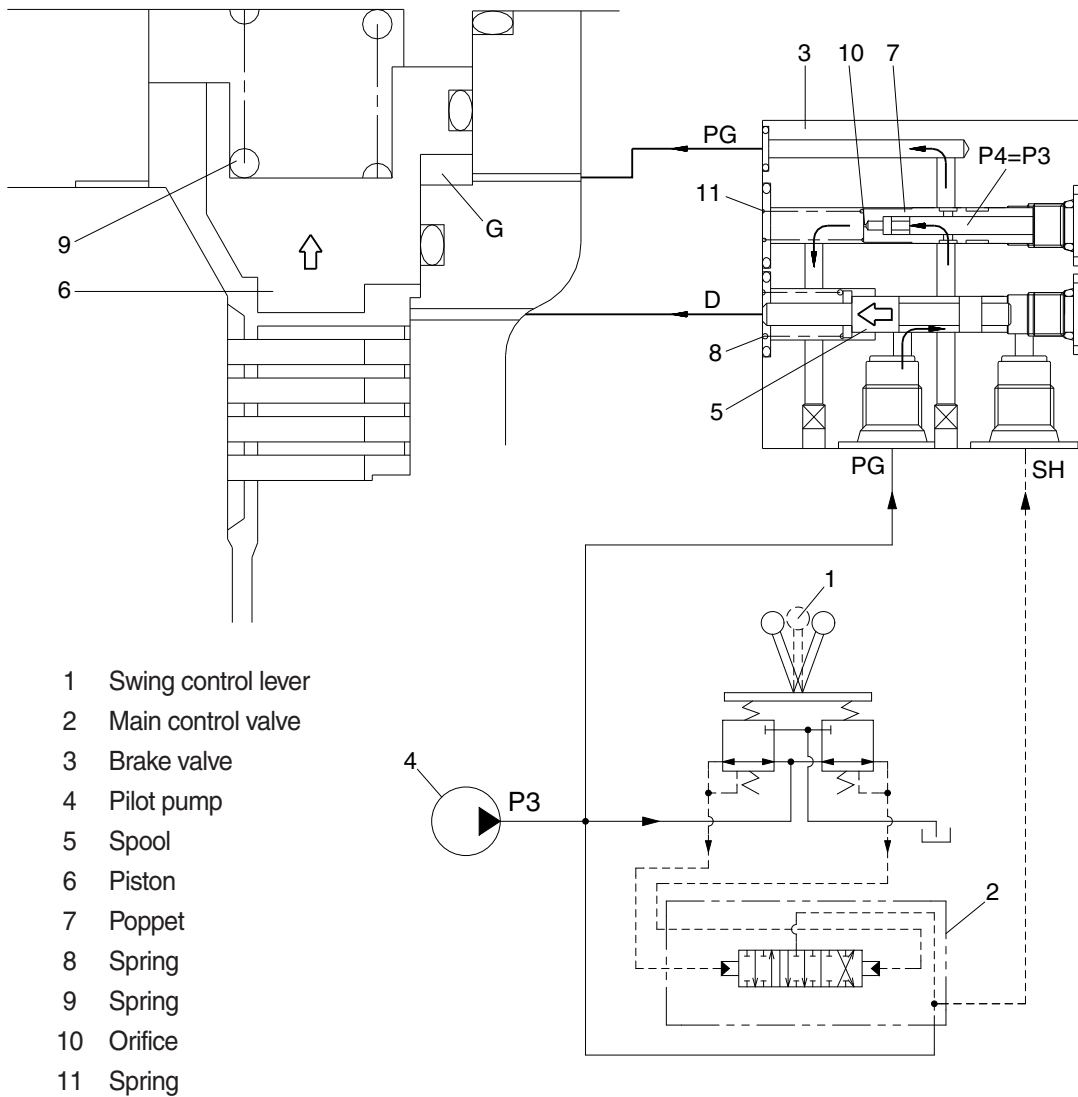


36072SM11

1	Casing	15	Separate plate
13	Cylinder block	16	Brake piston
14	Friction plate	17	Brake spring

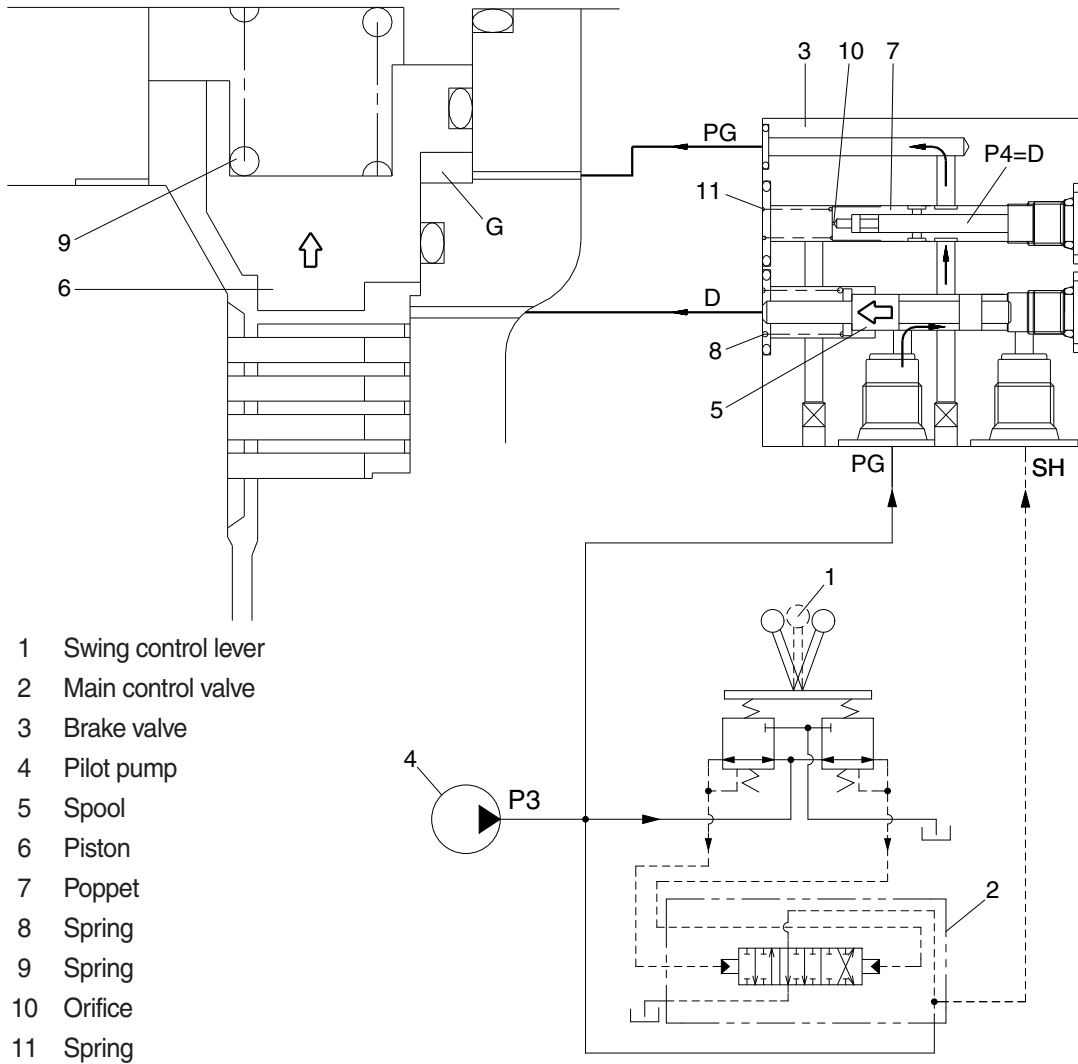
## ② Operating principle

- a. When one of the RCV lever (1) is set to the operation position, the each spool is shifted to left or right and the pilot oil flow is blocked. Then the pilot oil go to SH of the brake valve (3). This pressure moves spool (5) to the leftward against the force of the spring(8), so pilot pump charged oil (P3) goes to the chamber G through port PG. This pressure is applied to move the piston (6) to the upward against the force of the spring (9). Thus, it releases the brake force.



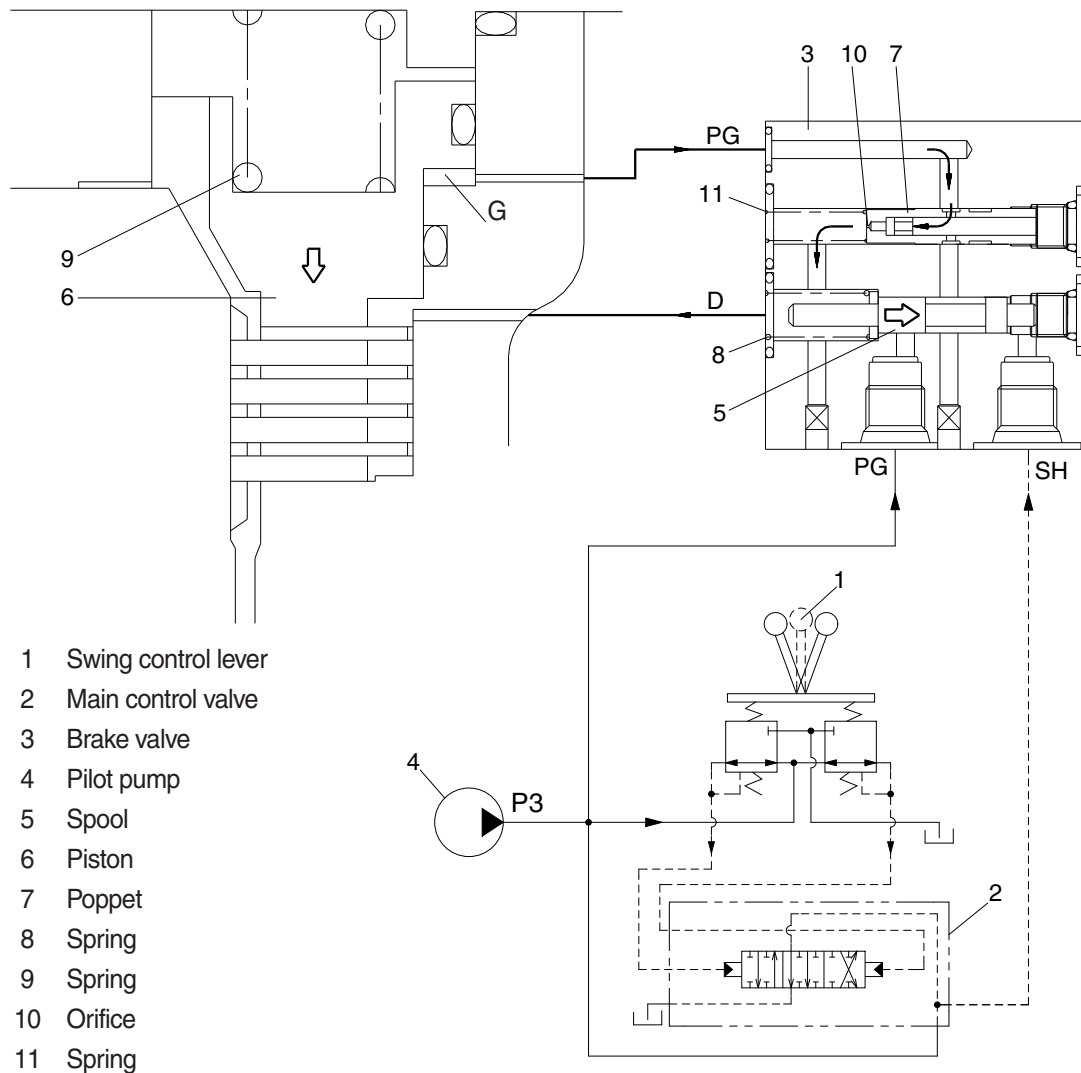
36072SM12

- b. When all of the RCV lever (1) are set the neutral position, the spool (5) returns to right. Then, the piston (6) is moved lower by spring force and the return oil from the chamber G flows back to tank port. At this time, the brake works.



36072SM13A

- c. When the swing control (1) lever is set the neutral position the spool (5) returns right in the brake valve (3).
- Then, the piston (6) is moved lower by spring force and the return and the return oil from the chamber G flows back to D-port through orifice (10) of the poppet (7).
- At this time, the poppet (7) works to make a time lag for 5 seconds.



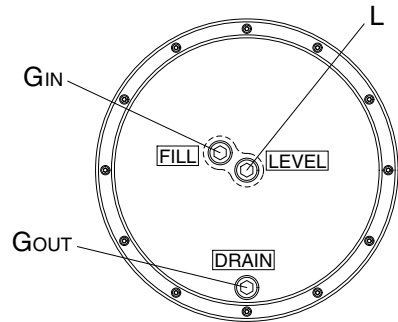
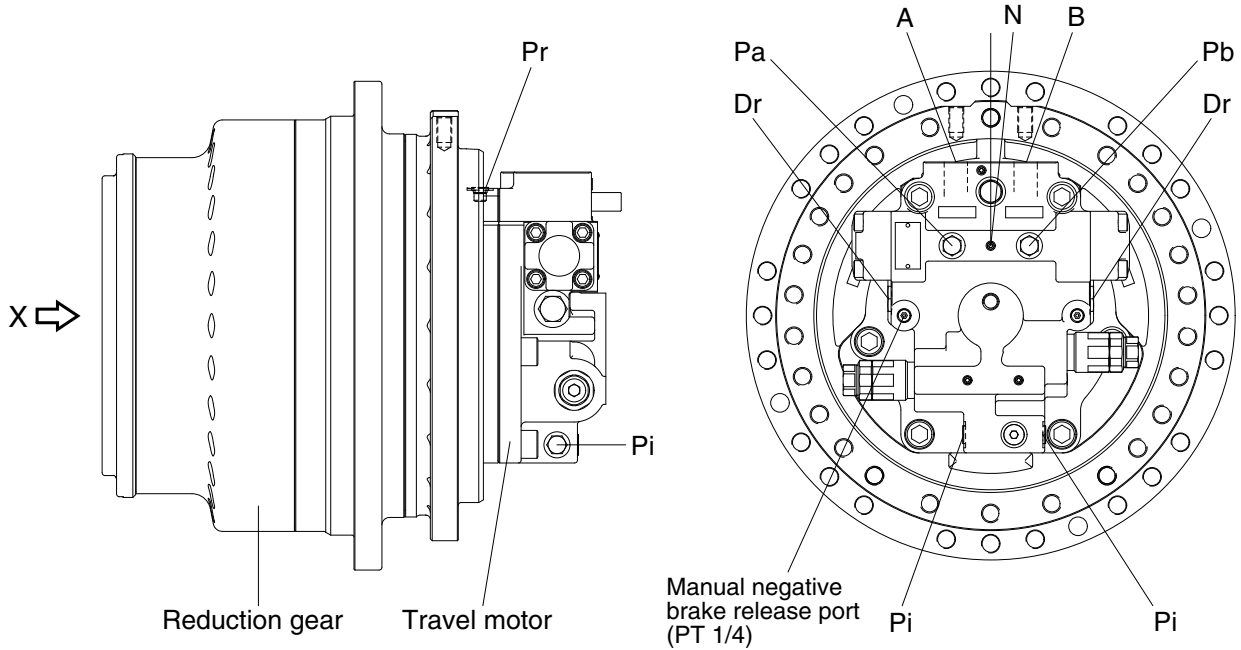
38092SM04

# GROUP 4 TRAVEL DEVICE

## 1. CONSTRUCTION

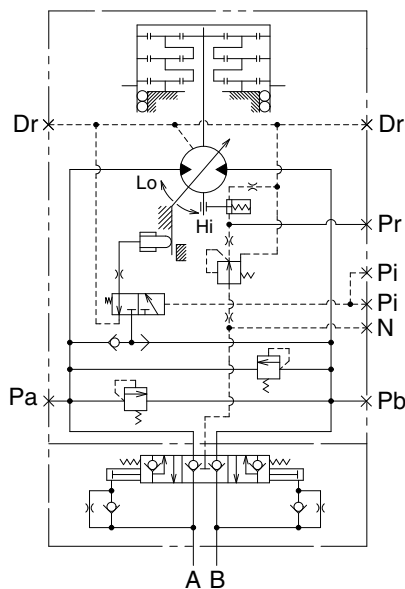
Travel device consists travel motor and reduction gear.

Travel motor include counterbalance valve, cross over relief valve.



VIEW X

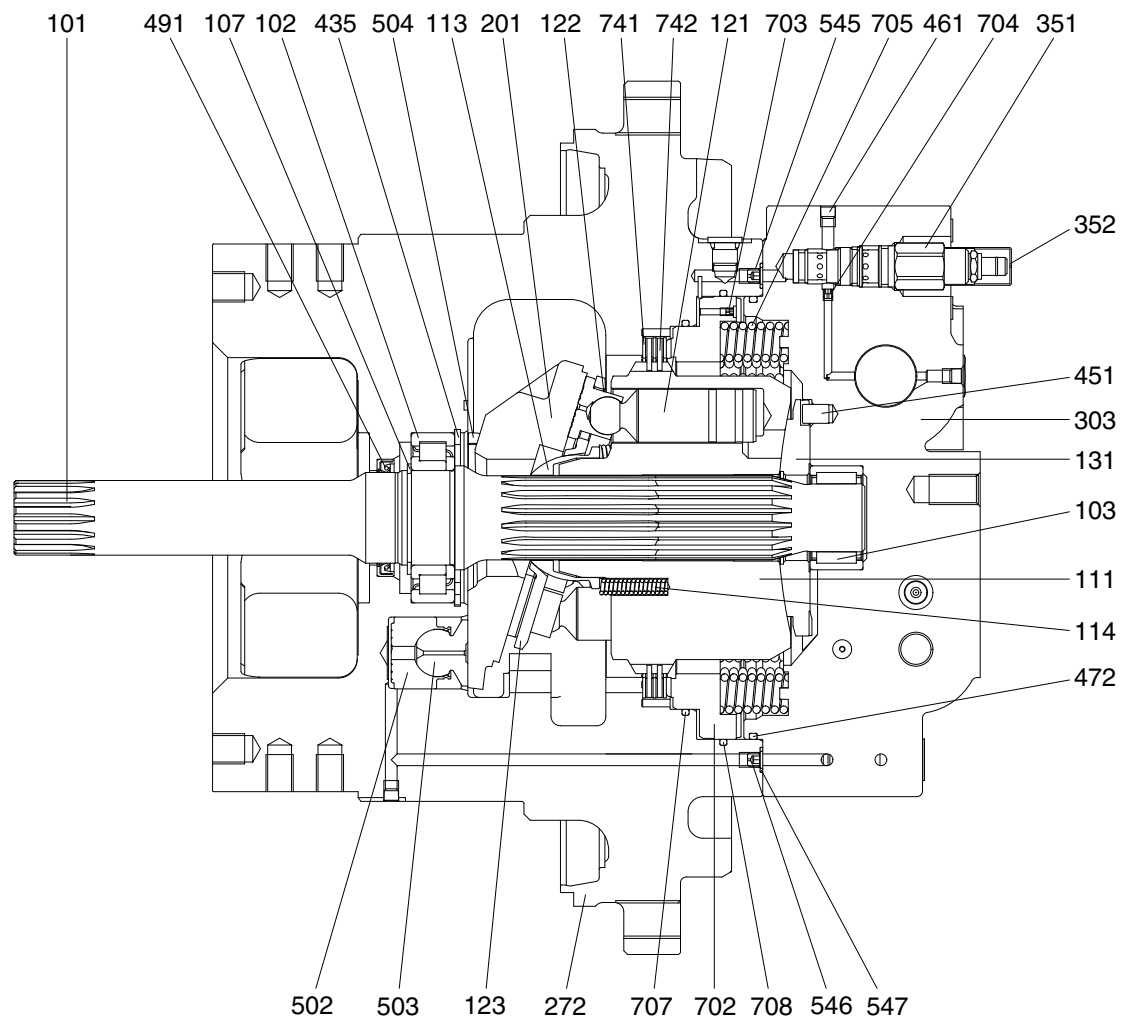
3809A2TM01



Hydraulic circuit

Port	Port name	Port size
A	Main port	SAE 6000 psi 1"
B	Main port	SAE 6000 psi 1"
Pi	Pilot port	PF 1/4
Dr	Drain port	PF 1/2
N	Negative brake release port	NPTF 1/16
Pa, Pb	Pressure gauge port	PF 1/4
Pr	Brake release pressure gauge port	PF 1/4
L	Level gauge	PF 1/2
GIN	Gear oil inlet port	PF 1/2
GOUT	Gear oil outlet port	PF 1/2

## 1) TRAVEL MOTOR (1/2)

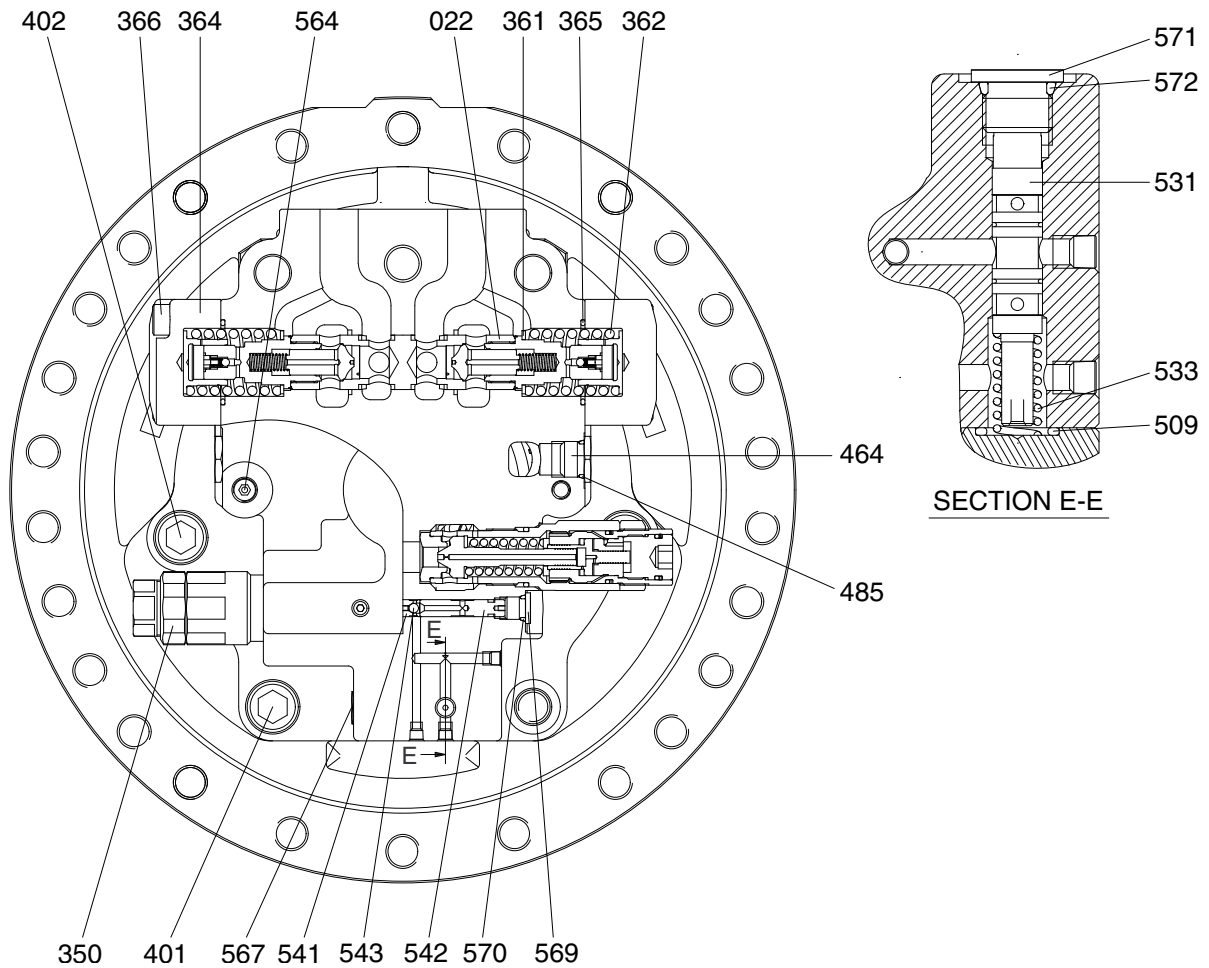


3809A2TM02

101	Drive shaft	272	Shaft casing	545	Orifice
102	Roller bearing	303	Valve casing	546	Orifice
103	Needle bearing	351	Reducing valve	547	O-ring
107	Snap ring	352	Cover	702	Brake piston
111	Cylinder block	435	Snap ring	703	Orifice
113	Spherical bushing	451	Pin	704	Orifice
114	Cylinder spring	461	Plug	705	Brake spring
121	Piston	472	O-ring	707	O-ring
122	Shoe	491	Oil seal	708	O-ring
123	Set plate	502	Piston	741	Separation plate
131	Valve plate	503	Shoe	742	Friction plate
201	Swash plate	504	Pivot ball		



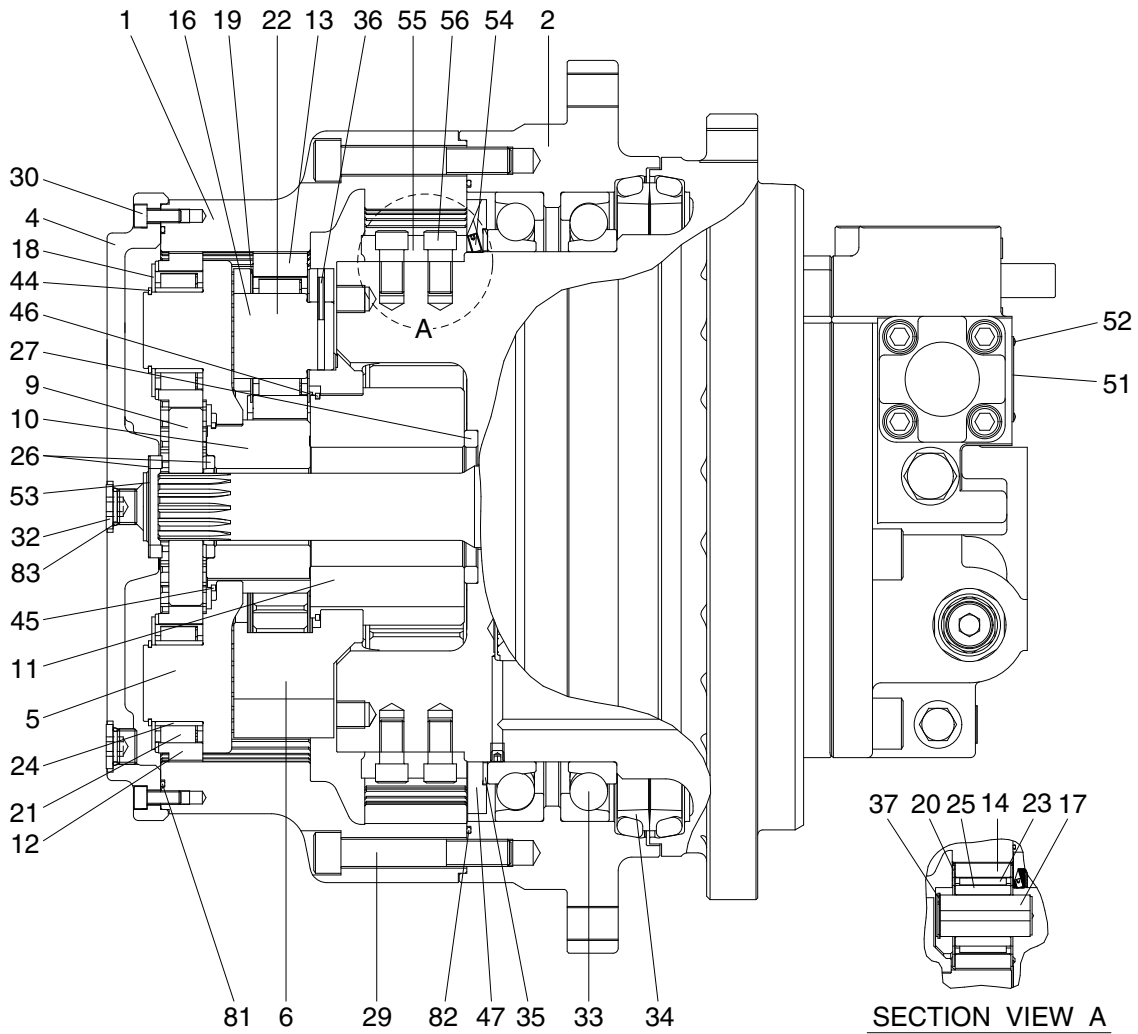
## TRAVEL MOTOR (2/2)



022 Counterbalance spool	402 Hex socket bolt	543 Steel ball
350 Relief valve	464 VP plug	564 Plug
361 Washer	485 O-ring	567 VP plug
362 Counterbalance spring	509 O-ring	569 RO plug
364 Counterbalance cover	531 Tilting spool	570 O-ring
365 O-ring	533 Tilting spring	571 RO plug
366 Hex socket bolt	541 Seat	572 O-ring
401 Hex socket bolt	542 Stopper	

3607A2TM03

## 2) REDUCTION GEAR

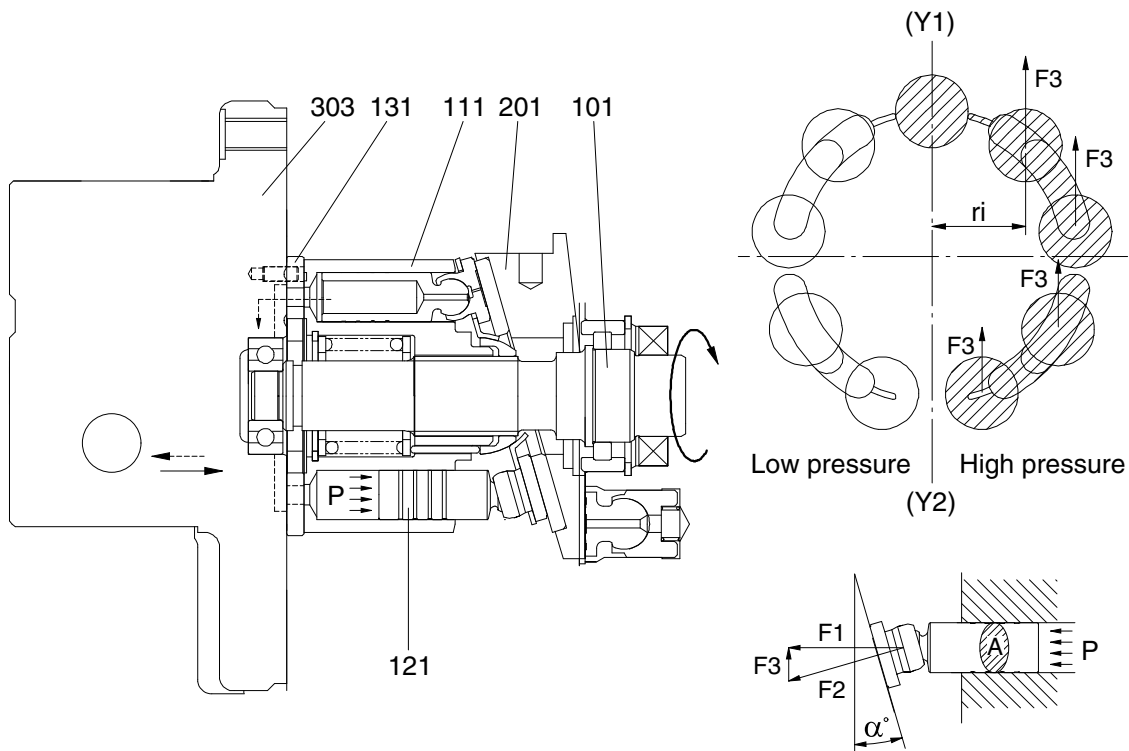


3809A2TRG01

1	Ring gear	20	Side plate	37	Snap ring
2	Housing	21	Needle cage	44	Snap ring
4	Side cover	22	Needle cage	45	Clip
5	Carrier 1	23	Needle cage	46	W clip
6	Carrier 2	24	Inner ring	47	Nutring
9	Sun gear 1	25	Floating bushing	51	Name plate
10	Sun gear 2	26	Thrust ring	52	Rivet
11	Sun gear 3	27	Thrust ring	53	Washer
12	Planetary gear 1	29	Socket bolt	54	Set screw
13	Planetary gear 2	30	Socket bolt	55	Nutring stopper
14	Planetary gear 3	32	RO plug	56	Hex socket bolt
16	Pin 2	33	Angular bearing	81	O-ring
17	Pin 3	34	Floating seal	82	O-ring
18	Side plate	35	Shim	83	O-ring
19	Side plate	36	Spring pin		

## 2. FUNCTION

### 1) GENERATION OF TORQUE



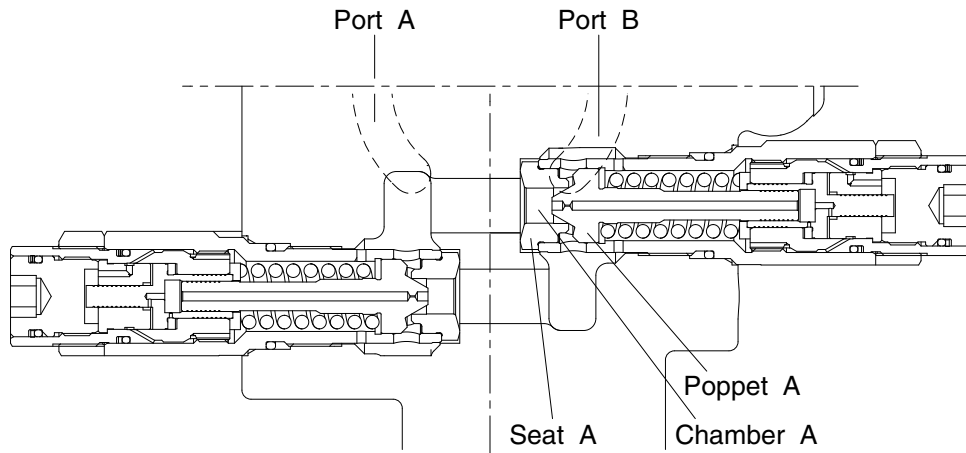
3607A2TRG02

The pressurized oil delivered from the hydraulic pump flows to valve casing (303) of the motor, passes through the brake valve mechanism, and is introduced into cylinder block (111) via valve plate (131). This oil constructively introduced only to one side of (Y1)- (Y2) connecting the upper and lower dead points of stroke of piston (121). The pressurized oil led to one side in cylinder block (111) pushes each piston (121) four or five and generates a forec [ $F \text{ (kgf)} = P \text{ (kgf/cm}^2) \times A \text{ (cm}^2)$ ]. This force acts on swash plate (201), and is resolves into components (F2 and F3) because swash plate (201) is fixed at an angle ( $\alpha$ ) with the axis of drive shaft (101). Radial component (F3) generates respective torques ( $T=F3 \times r_i$ ) for (Y1)- (Y2). This residual of torque [ $T=S (F3 \times r_i)$ ] rotates cylinder block (111) via piston (121). Since the cylinder block (111) is spline coupled with drive shaft (101). So the drive shaft (101) rotates and the torque is transmitted.

## 2) RELIEF VALVE

The relief valve mainly has the following two functions :

- (1) To keep the starting pressure of the hydraulic motor at a constant value and bypass to the return line excessive oil generated at the motor inlet depending upon the acceleration speed of the driven inertia.
- (2) To generate a brake pressure at the outlet during stopping of the driven inertia, and stop it forcedly.



3607A2TM06

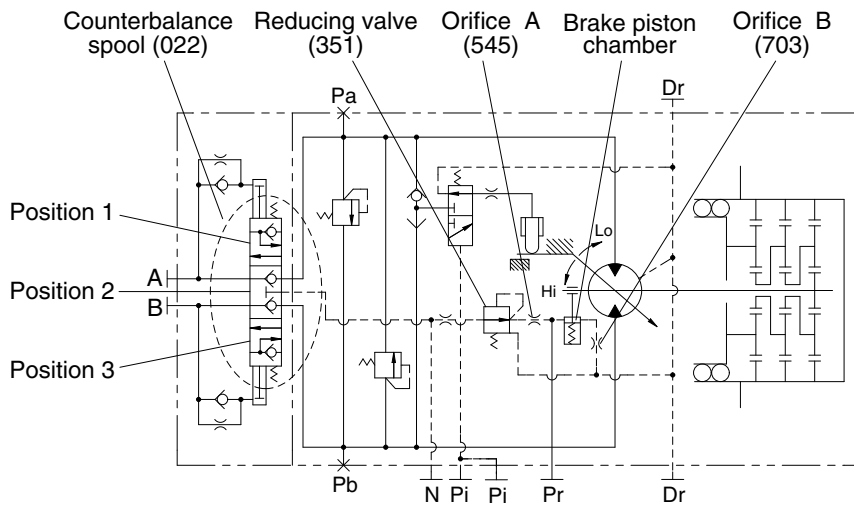
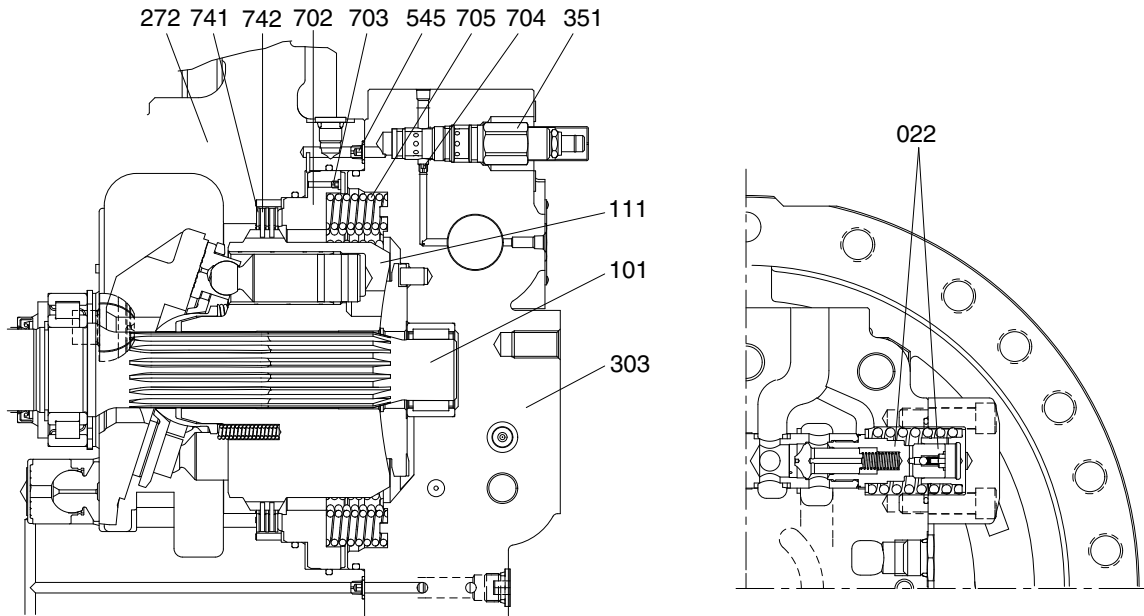
The chamber A is always connected to the port A of the motor.

When the pressure at port A increases and the force pushing poppet A is higher than the set pressure of the spring, then poppet A is pushed up from the contact surface of seat A, and oil flows from chamber A to port B.

### 3) NEGATIVE BRAKE

The negative brake is released applying to the brake piston (702) the pressure led through the built-in counterbalance spool sub-assembly (022).

With no pressure working, the brake force is always ensured.

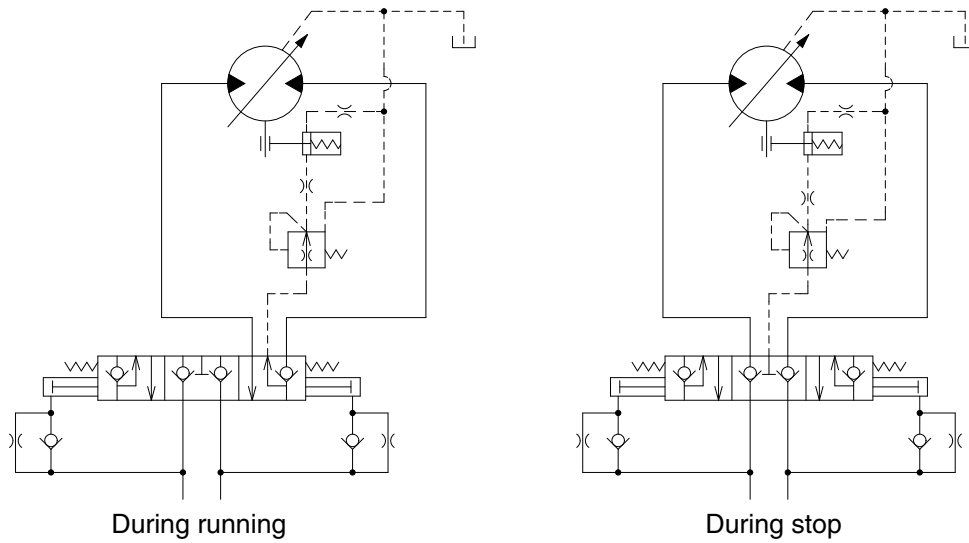


3607A2TM07

The brake force is the friction force generated on the surfaces of the friction plates (742) spline-coupled with the cylinder block (111), when their rotation is restricted by the shaft casing (272), separation plate (741), and brake piston (702).

Without pressure being applied to the brake piston, the brake piston is pushed by fourteen brake springs (705), and the friction plate and separation plate are held between the brake and shaft casing. This holding force functions as the friction force. This friction force restrains the shaft (101) spline-coupled with the cylinder block, and this function is the brake.

#### 4) PRESSURE RELEASE VALVE (Flow control valve)



3607A2TM08A

This brake is of a backpressure-insensitive type. In other words, since the counterbalance spool used be overlapped at the neutral position, the pressure release valve prevents the circuit backpressure from working into the brake chamber when the machine stops traveling and works, and so the specified brake torque is available even on a slope.

During normal traveling, the pressure coming through the counterbalance valve is applied to the brake chamber to release the break, and is also applied to the pressure release valve section.

This pressure release valve is of a constant differential pressure type, and irrespective of the working pressure, the passing flow is constant and approximately 1 to 2  $\ell / \text{min}$ .

When the condition changes from traveling to stop, the counterbalance spool returns to its neutral position. The brake piston is pushed by the brake spring, and the oil in the brake chamber flow to the motor drain line via the pressure release valve. Then the brake torque is generated.

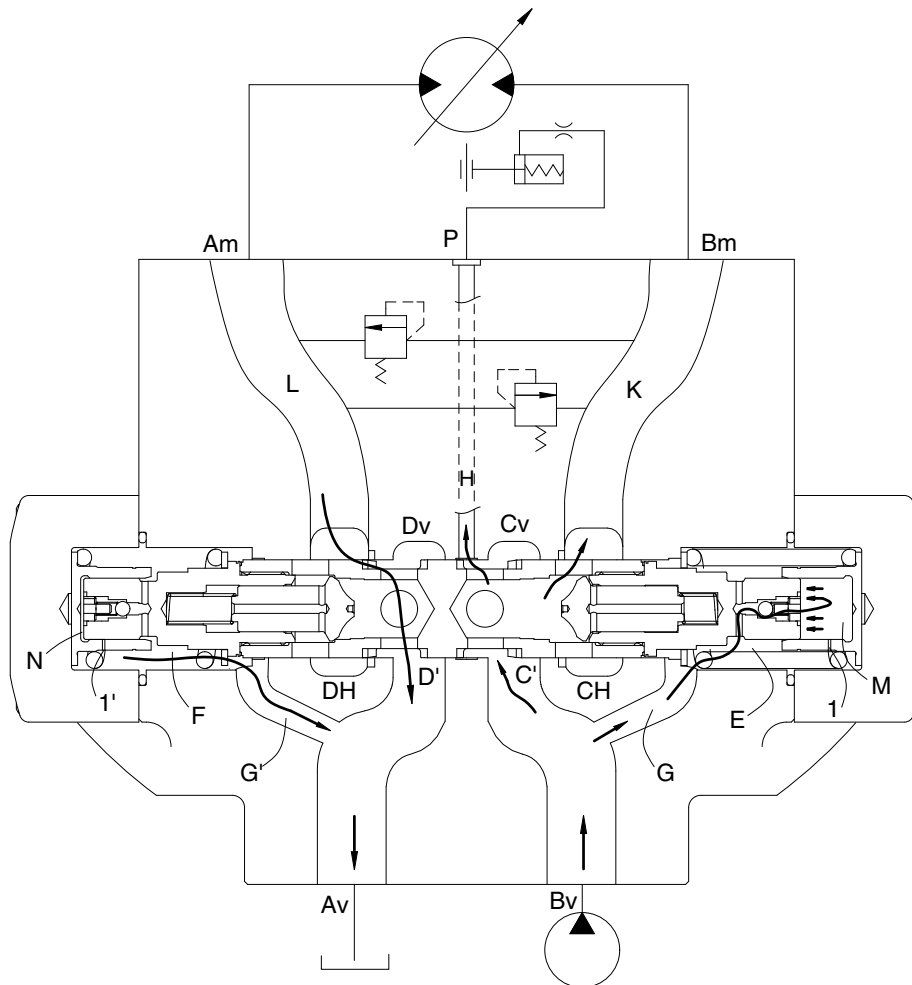
## 5) RELEASING METHOD OF NEGATIVE BRAKE

In releasing the negative brake without applying the brake releasing pressure, follow the procedures shown below.

Details of work	Tools
Remove two plugs (564) from the valve casing (303). (For their position, see the attached installation dimension) Tighten an M10 screw of 135 mm in length into a tapped hole of the brake piston (702). Then the condition having the brake release pressure is attained and the brake is released.	Socket wrench 6 mm 8 mm

Note : Even with the negative brake released, the hydraulic motor will not turn. When it is difficult to generate the working pressure due to failure of the pump or so, and the whole machine is to be pulled for transportation without removing the hydraulic motor, connect pressure measurement ports  $P_a$  and  $P_b$  with a short hose or something. Then the machine can be pulled slowly.

## 6) COUNTERBALANCE VALVE



3607A2TRG03

Suppose port Bv is connected to the hydraulic pump and Port Av, to the tank. The oil supplied from the hydraulic pump passes through Bv, Cv and C' in sequence, pushes up the poppet of the check valve, passes through K to Port Bm, and is supplied to the hydraulic motor to turn it.

Therefore, the pump discharge oil pressure increases, and the pressure is led via passage G to spring room E and via the ball check valve to dumping room M. When the pressure in rooms E and M exceeds the value equivalent to the force of the spring which holds the spool at its neutral position, the spool begins to move left. Since the working oil in room N flows into room F via throttle 1' and that in room F is discharged via passage G' through port Av to the tank, the spool moves left to have passage L-DH-D'-Dv composed. In addition, passage Cv-H-P is also composed, and the pump discharge pressure in port Bv is led to port P.

Because of the throttle or clearance provided for the working oil flow from room N, this changeover motion of the spool is comparatively slow.

When the pump discharge pressure is higher, the spool movement is larger and the above opening area of the spool is larger.

When the pump discharge pressure falls, pressures in rooms E and M fall and the spool will move right due to the spring on the room F side.

Since working oil in room M flows to room E via throttle 1 and that in room E, to port Bv via passage G, the spool moves right.

When the pressure at port Bv falls down to the tank pressure, the pressure in room E also falls to the tank pressure and becomes equal to that in room F, and so the spool returns to its neutral position.



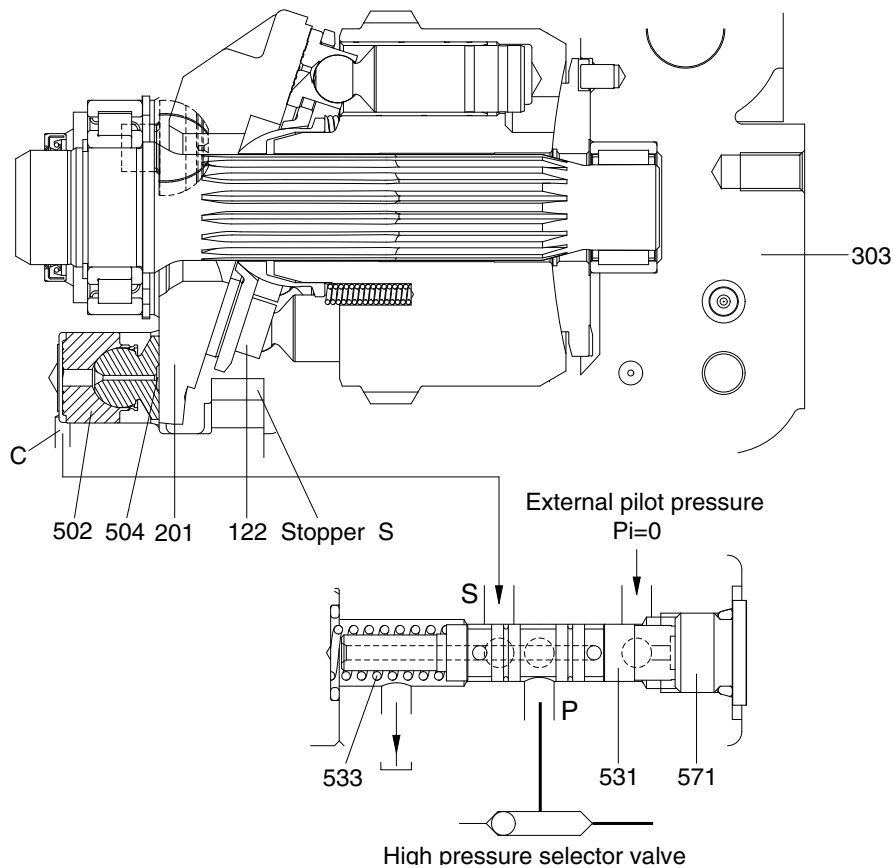
## 7) DISPLACEMENT CHANGEOVER SECTION

As a supporting mechanism for the swash plate (201) on which the shoes (122) slide, the pillar system is adopted to support the load with semi-cylindrical sliding bearings provided at both ends of the mechanism.

The capacity is changed by changing the tilting angle of this swash plate.

This is a mechanism that swash plate was pushed by tilting position, and the tilting angle of the swash plate is decided in two positions (large and small) by controlling the flows to and from these piston rooms with the displacement changeover valve section.

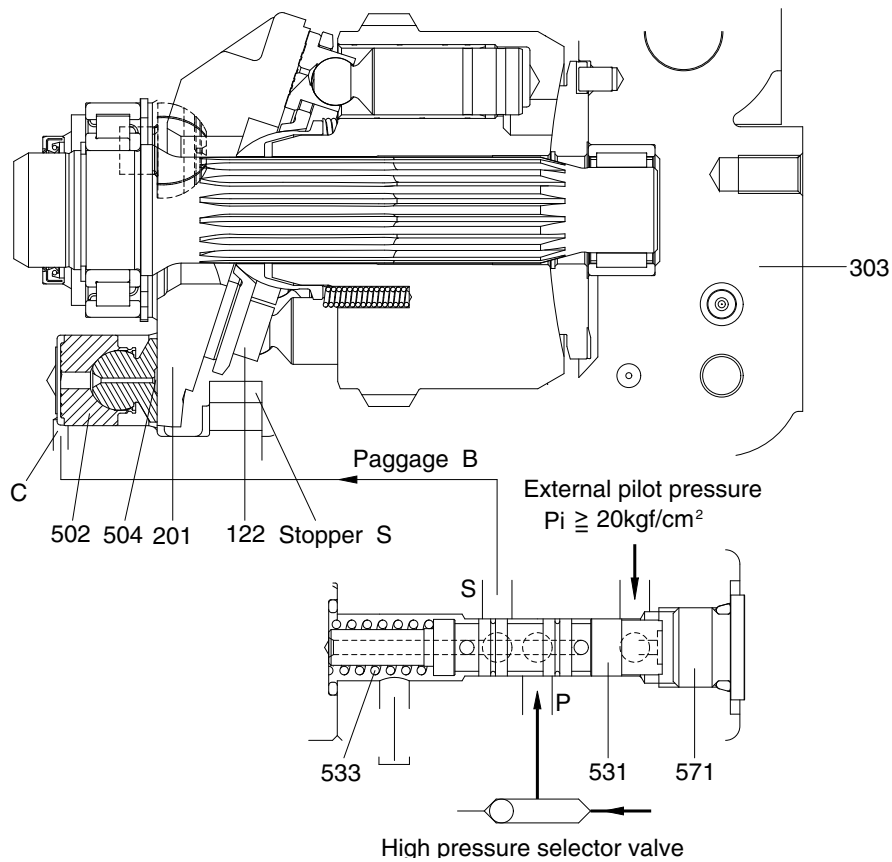
(1) External pilot pressure :  $P_i = 0$  ..... Large displacement



3607A2TM04

By means of the built-in high pressure selector mechanism in the valve casing (303), the high pressure oil working on the motor functions to port P of the displacement-changeover valve. This pressure becomes the servo pressure. Since the spool (531) assembled in the displacement changeover valve is pressed to plug (571) by thy spring (533), the high pressure oil at port P is enclosed.

(2) External pilot pressure :  $P_i \geq 20 \text{ kgf/cm}^2$  ——— small displacement

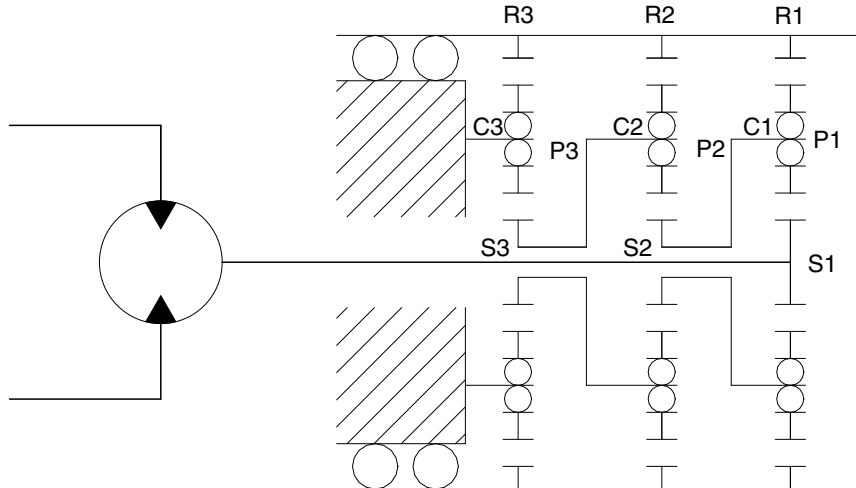


3607A2TM05

The force working on the spool (531) of the displacement-changeover valve becomes higher than that of the spring (533), and the spool moves left. The high pressure oil flows from port P of the displacement-changeover valve through port S and passage B to room C where it works. The displacement changeover piston (502) is pushed light by the high pressure oil and the swash plate moves in the arrowed direction. The swash plate moves until it touched stopper S, and then is fixed there.

## 8) REDUCTION GEAR

The reduction gear is composed of a three-stage planetary gear mechanism shown in the following figure. Since the sun gear is designed to have a floating mechanism, errors of the gears and carrier pin hole pitches will not affect the gears' lives heavily.



3607A2TRG04

The input rotation of the hydraulic motor is transmitted to No. 1 sun gear (S1) and this drives No. 1 planetary gears (P1). This No. 1 planetary gears (P1) drive No.1 ring gear (R1) with the same force as the meshing tangential force with No. 1 sun gear (S1), and also No. 1 carrier (C1) with the same force as the meshing reaction force. In other words, No. 1 planetary gears (P1) revolve rotating. This rotation of No. 1 carrier (C1) becomes the output of the 1st stage, and is transmitted directly to No. 2 sun gear (S2).

(No. 1 carrier is spline-coupled with No. 2 sun gear.) Similarly the revolution of No. 2 planetary gear (P2) are transmitted via No.2 carrier (C2) to No. 3 sun gear (S3). Since No. 3 carrier (C3) supporting No. 3 planetary gears (P3) are fixed, No. 3 planetary gears (P3) do not revolve, but rotates to drive No. 3 ring gear (R3).

Therefore, the rotating case is driven by the overall driving torque of No1, 2 and 3 ring gears.

This reduction ratio is expressed as shown below:

$$i = \frac{(Z_{S1} + Z_{R1}) (Z_{S2} + Z_{R2}) (Z_{S3} + Z_{R3})}{Z_{S1} \cdot Z_{S2} \cdot Z_{S3}} - 1$$

where Z : Number of teeth of each gear

The direction of rotation is reverse to that of the input shaft.

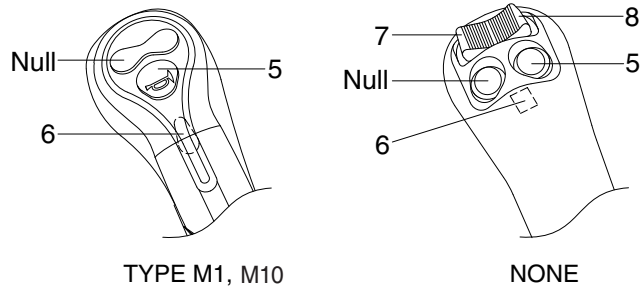
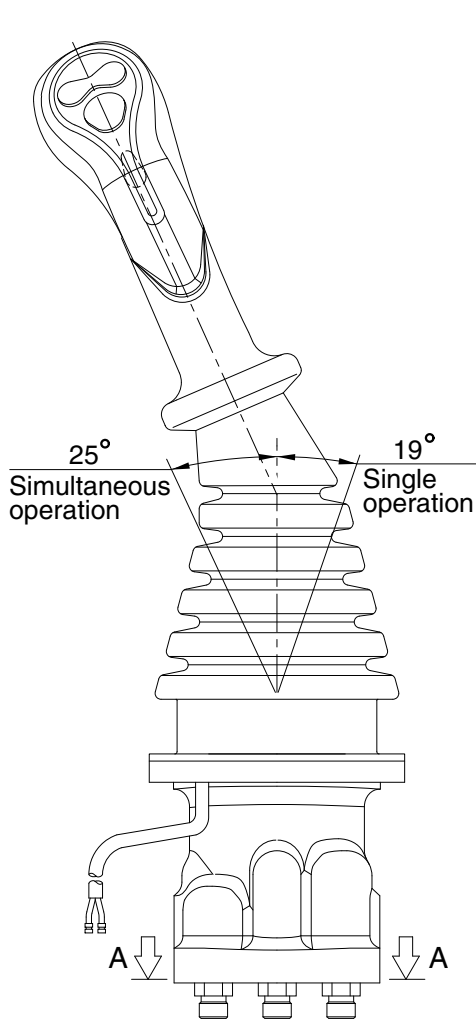
## GROUP 5 RCV LEVER

### 1. STRUCTURE

The casing has the oil inlet port P (primary pressure) and the oil outlet port T (tank). In addition the secondary pressure is taken out through ports 1, 2, 3 and 4 provided at the bottom face.

※ Refer to the parts manual for the types of the RCV lever.

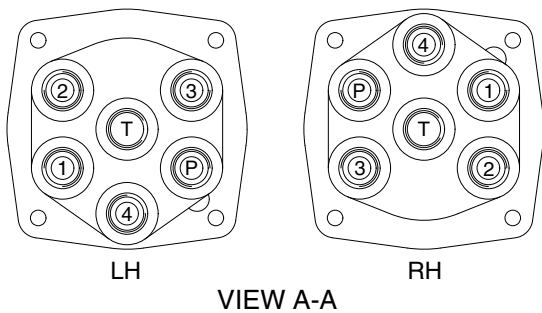
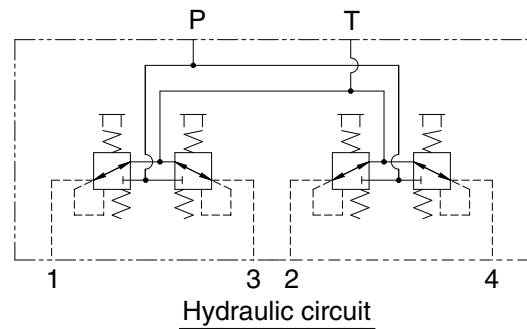
#### 1) TYPE M1, M10



#### Switches

Type	No.	LH	RH
M1, M10	5	One touch decel	Horn
	6	Power boost	Breaker
None	5	One touch decel	Horn
	6	Power boost	Null
	7	CCW rotation	Close
	8	CW rotation	Open

※ Number 7 and 8 : Option attachment

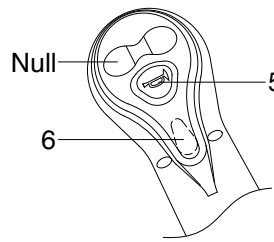
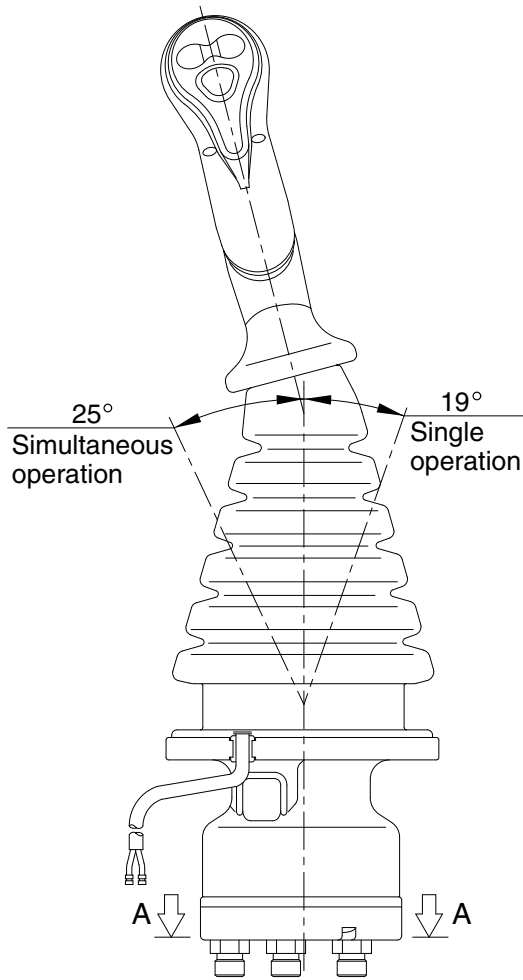


#### Pilot ports

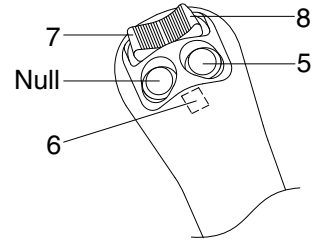
Port	LH	RH	Port size
P	Pilot oil inlet port	Pilot oil inlet port	PF 3/8
T	Pilot oil return port	Pilot oil return port	
1	Left swing port	Bucket out port	
2	Arm out port	Boom up port	
3	Right swing port	Bucket in port	
4	Arm in port	Boom down port	

480A2RL01

## 2) TYPE M11, M12



TYPE M12

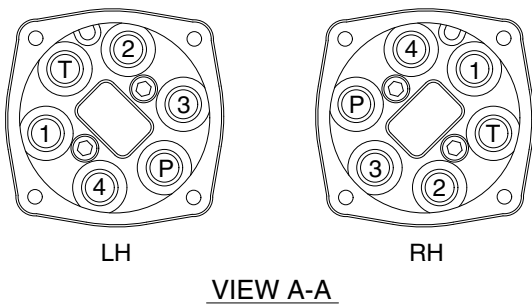
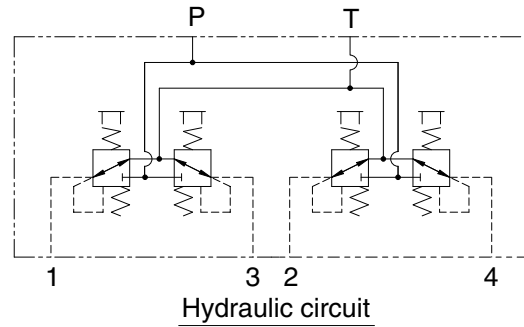


TYPE M11

### Switches

Type	No.	LH	RH
M12	5	One touch decel	Horn
	6	Power boost	Breaker
M11	5	One touch decel	Horn
	6	Power boost	Null
	7	CCW rotation	Close
	8	CW rotation	Open

※ Number 7 and 8 : Option attachment

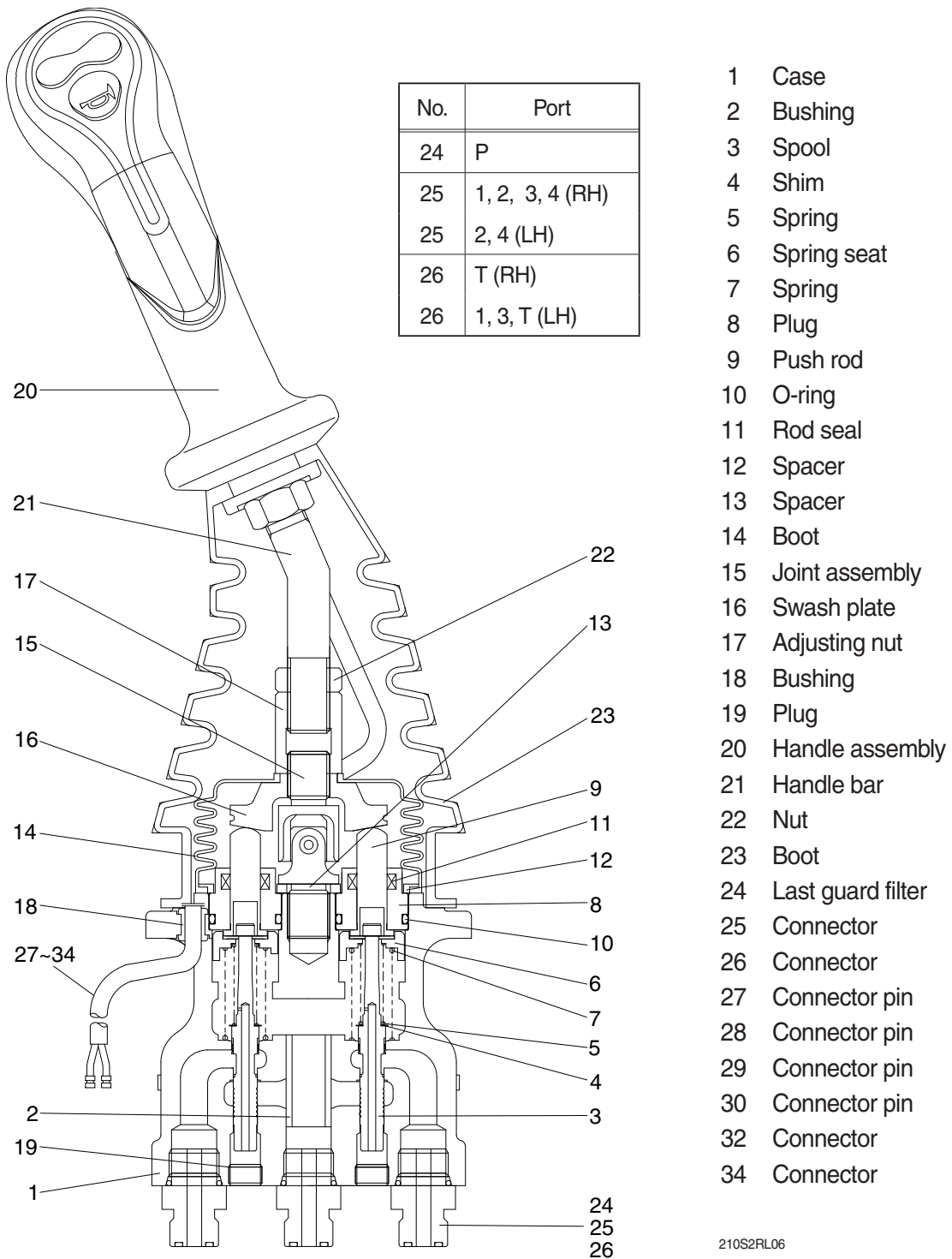


### Pilot ports

Port	LH	RH	Port size
P	Pilot oil inlet port	Pilot oil inlet port	PF 3/8
T	Pilot oil return port	Pilot oil return port	
1	Left swing port	Bucket out port	
2	Arm out port	Boom up port	
3	Right swing port	Bucket in port	
4	Arm in port	Boom down port	

480A2RL05

### 3) CROSS SECTION



210S2RL06

#### Item numbers are based on the type M1.

The construction of the pilot valve is shown in the attached cross section drawing. The casing has vertical holes in which reducing valves are assembled.

The pressure reducing section is composed of the spool (3), spring (5) for setting secondary pressure, return spring (7), spring seat (6) and shim (4). The spring for setting the secondary pressure has been generally so preset that the secondary pressure is 5 to 20.5 kgf/cm<sup>2</sup> (depending on the type). The spool is pushed against the push rod (9) by the return spring.

When the push rod is pushed down by tilting the handle, the spring seat comes down simultaneously and changes setting of the secondary pressure spring.

## 2. FUNCTIONS

### 1) FUNDAMENTAL FUNCTIONS

The pilot valve is a valve that controls the spool stroke, direction, etc of a main control valve. This function is carried out by providing the spring at one end of the main control valve spool and applying the output pressure (secondary pressure) of the pilot valve to the other end.

For this function to be carried out satisfactorily, the pilot valve is composed of the following elements.

- (1) Inlet port (P) where oil is supplied from hydraulic pump.
- (2) Output ports (1, 2, 3 & 4) to apply pressure supplied from inlet port to ends of control valve spools.
- (3) Tank port (T) necessary to control the above output pressure.
- (4) Spool to connect output port to inlet port or tank port.
- (5) Mechanical means to control output pressure, including springs that work on the above spools.

### 2) FUNCTIONS OF MAJOR SECTIONS

**Item numbers are based on the type M1.**

The functions of the spool (3) are to receive the supply oil pressure from the hydraulic pump at its port P, and to change over oil paths to determine whether the pressure oil of port P is led to output ports 1, 2, 3 & 4 or the output port pressure oil to tank port T.

The spring (5) works on this spool to determine the output pressure.

The change the deflection of this spring, the push rod (9) is inserted and can slide in the plug (8).

For the purpose of changing the displacement of the push rod through the swash plate (16) and adjusting nut (17) are provided the handle assy (20) that can be tilted in any direction around the fulcrum of the universal joint (15) center.

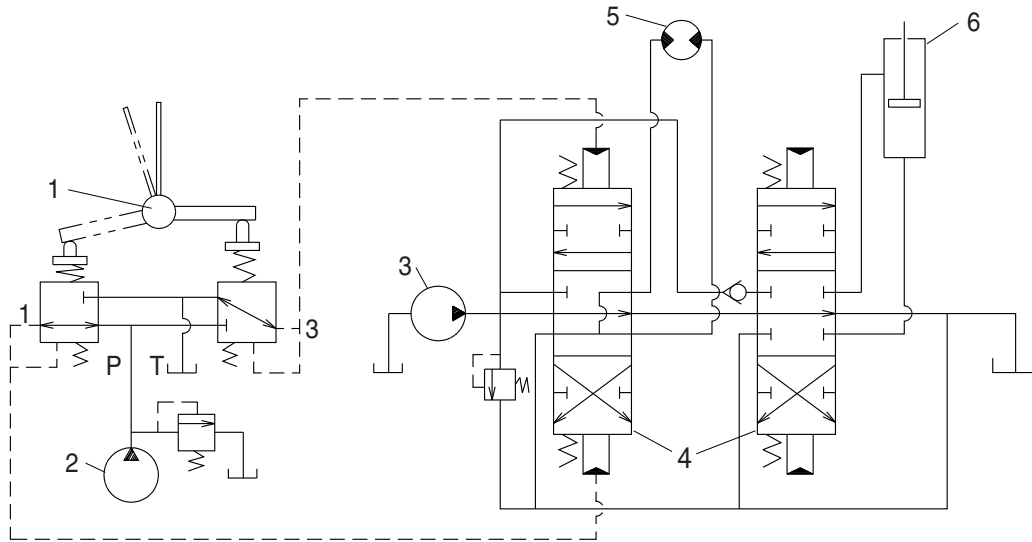
The spring (7) works on the case (1) and spring seat (6) and tries to return the push rod (9) to the zero-displacement position irrespective of the output pressure, securing its resetting to the center position.

This also has the effect of a reaction spring to give appropriate control feeling to the operator.

### 3) OPERATION

The operation of the pilot valve will be described on the basis of the hydraulic circuit diagram shown below and the attached operation explanation drawing.

The diagram shown below is the typical application example of the pilot valve.



2-70

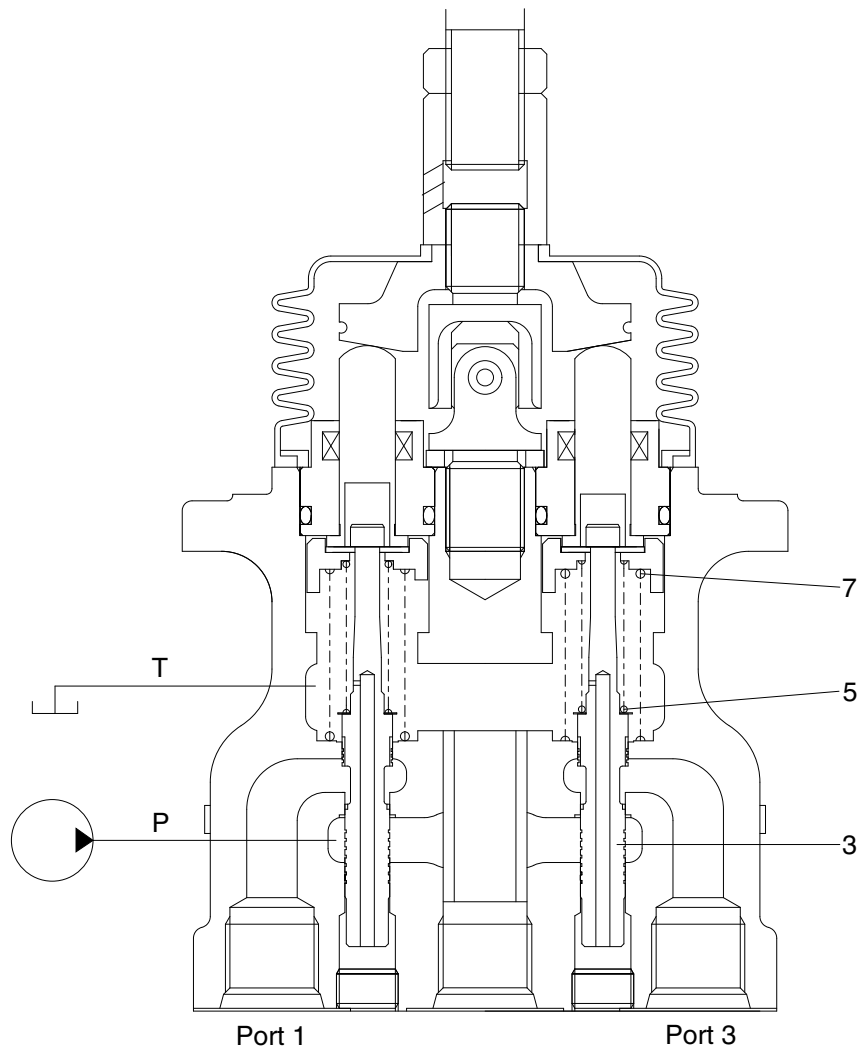
- 1 Pilot valve
- 2 Pilot pump

- 3 Main pump
- 4 Main control valve

- 5 Hydraulic motor
- 6 Hydraulic cylinder



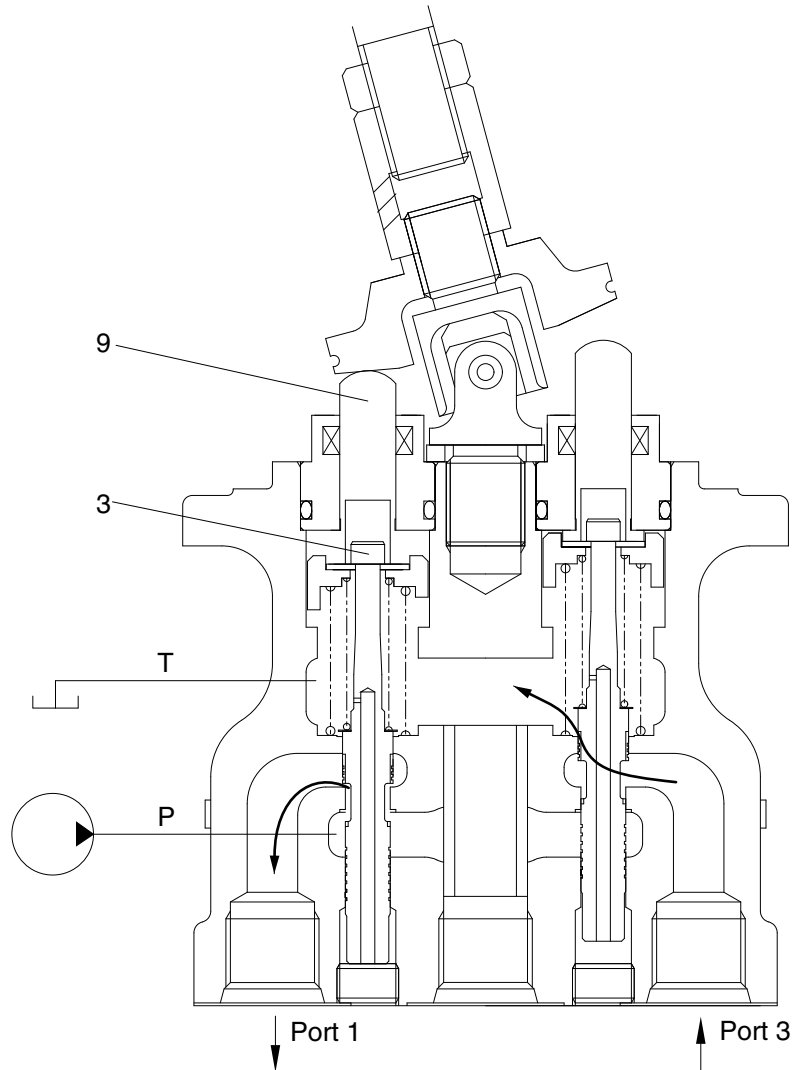
(1) Case where handle is in neutral position



300L2RL03

The force of the spring (5) that determines the output pressure of the pilot valve is not applied to the spool (3). Therefore, the spool is pushed up by the spring (7) to the position of port (1, 3) in the operation explanation drawing. Then, since the output port is connected to tank port T only, the output port pressure becomes equal to tank pressure.

**(2) Case where handle is tilted**



300L2RL04

When the push rod (9) is stroked, the spool (3) moves downwards.

Then port P is connected with port (1) and the oil supplied from the pilot pump flows through port (1) to generate the pressure.

When the pressure at port (1) increases to the value corresponding to the spring force set by tilting the handle, the hydraulic pressure force balances with the spring force. If the pressure at port (1) increases higher than the set pressure, port P is disconnected from port (1) and port T is connected with port (1). If it decreases lower than the set pressure, port P is connected with port (1) and port T is disconnected from port 1.

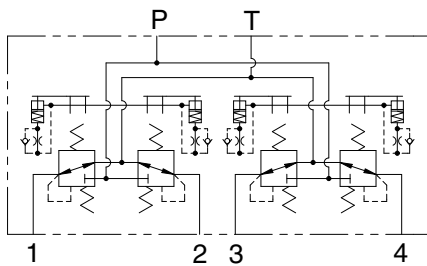
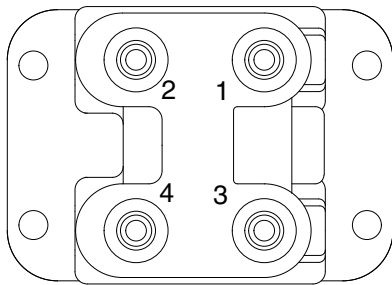
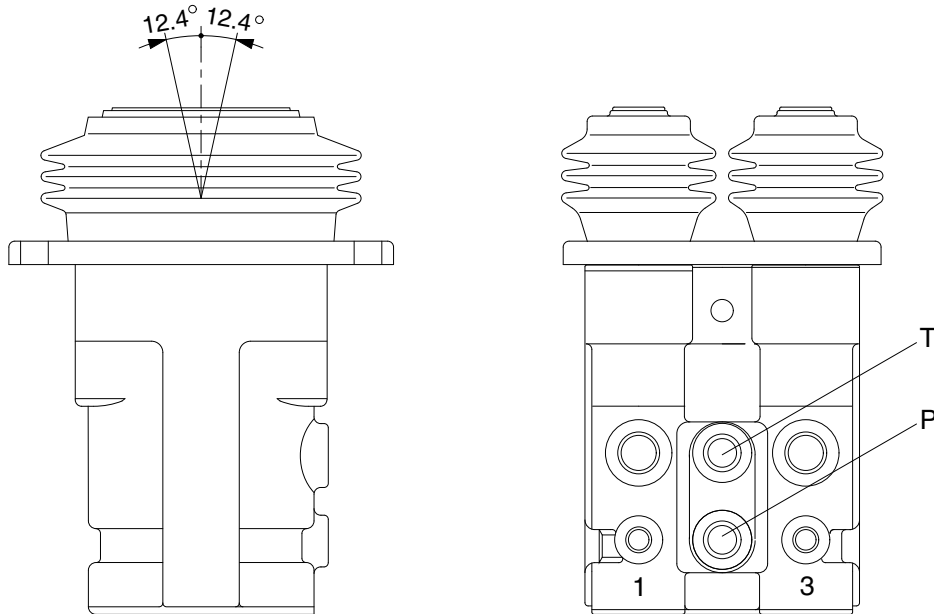
In this manner the secondary pressure is kept at the constant value.

Besides, in some type, when the handle is tilted more than a certain angle, the upper end of the spool contacts with the inside bottom of the push rod and the output pressure is left to be connected with port P.

## GROUP 6 RCV PEDAL

### 1. STRUCTURE

The casing (spacer) has the oil inlet port P (primary pressure), and the oil outlet port T (tank). In addition the secondary pressure is taken out through ports 1, 2, 3 and 4 provided at the bottom face.



Hydraulic circuit

Port	Port	Port size
P	Pilot oil inlet port	PF 1/4
T	Pilot oil return port	
1	Travel (LH, Forward)	
2	Travel (LH, Backward)	
3	Travel (RH, Forward)	
4	Travel (RH, Backward)	

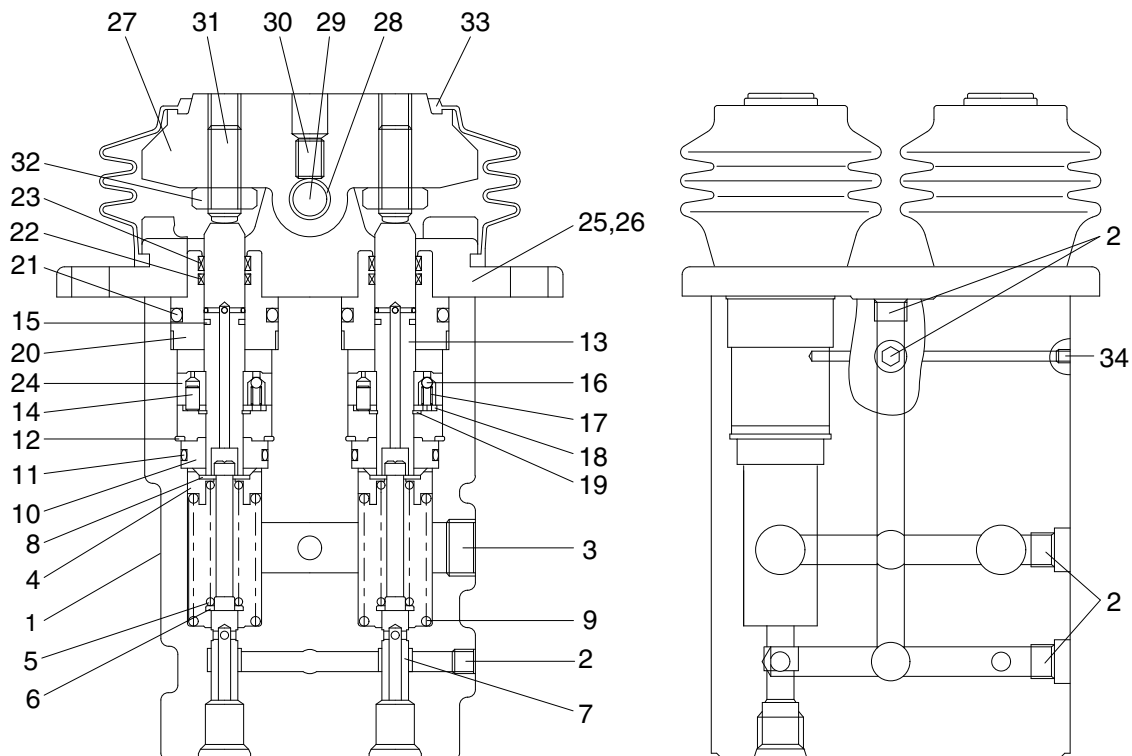
480A2RP01

## CROSS SECTION

The construction of the RCV pedal is shown in the below drawing. The casing has vertical holes in which reducing valves are assembled.

The pressure reducing section is composed of the spool kit (7), spring (5) for setting secondary pressure, return spring (9), stopper (8), and spring seat (6). The spring for setting the secondary pressure has been generally so preset that the secondary pressure is  $6.3 \pm 1$  to  $24.9 \pm 1.5$  kgf/cm<sup>2</sup> (depending on the type). The spool is pushed against the push rod (13) by the return spring.

When the push rod is pushed down by tilting pedal, the spring seat comes down simultaneously and changes setting of the secondary pressure spring.



480A2RP02

1	Body	13	Push rod	25	Cover
2	Plug	14	Spring pin	26	Socket bolt
3	Plug	15	Seal	27	Cam
4	Spring seat	16	Steel ball	28	Bushing
5	Spring	17	Spring	29	Cam shaft
6	Spring seat	18	Plate	30	Set screw
7	Spool kit	19	Snap ring	31	Set screw
8	Stopper	20	Plug	32	Hex nut
9	Spring	21	O-ring	33	Bellows
10	Rod guide	22	Oil seal	34	Expand
11	O-ring	23	Dust seal	36	Cap
12	Snap ring	24	Piston		

## 2. FUNCTION

### 1) FUNDAMENTAL FUNCTIONS

The pilot valve is a valve controls the spool stroke, direction, etc of a main control valve. This function is carried out by providing the spring at one end of the main control valve spool and applying the output pressure (secondary pressure) of the pilot valve to the other end.

For this function to be carried out satisfactorily, the pilot valve is composed of the following elements.

- (1) Inlet port (P) where oil is supplied from hydraulic pump.
- (2) Output port (1, 2, 3 & 4) to apply pressure supplied from inlet port to ends of control valve spools.
- (3) Tank port (T) necessary to control the above output pressure.
- (4) Spool to connect output port to inlet port tank port.
- (5) Mechanical means to control output pressure, including springs that work on the above spools.

### 2) FUNCTIONS OF MAJOR SECTIONS

The functions of the spool (7) are to receive the supply oil pressure from the hydraulic pump at its port P, and to change over oil paths to determine whether the pressure oil of port P is led to output ports 1, 2, 3 & 4 or the output spool to determine the output pressure.

The spring (5) works on this spool to determine the output pressure.

The change the deflection of this spring, the push rod (13) is inserted and can slide in the plug (20). For the purpose of changing th displacement of the push rod through the cam (27) and adjusting nut (32) are provided the pedal that can be tilted in any direction around the fulcrum of the cam (27) center.

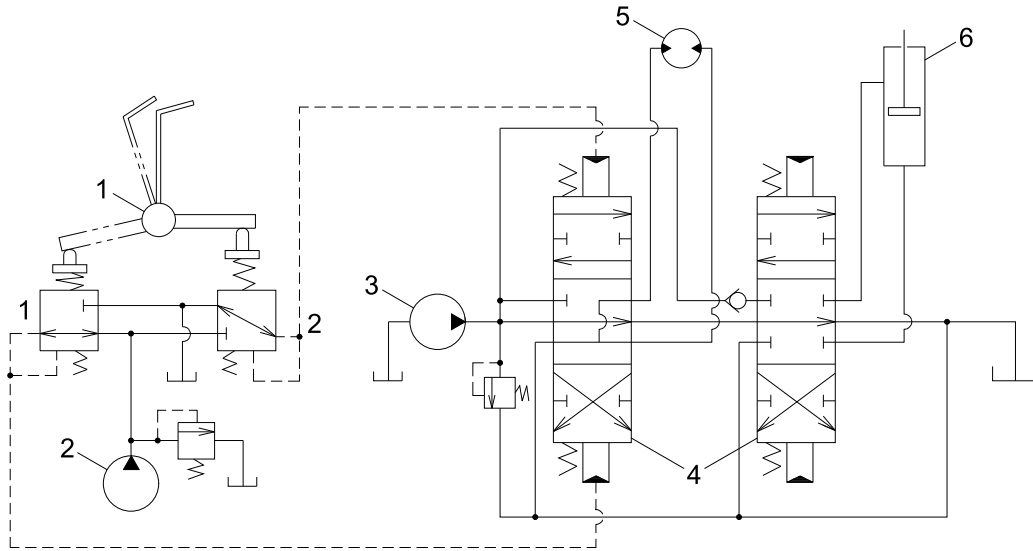
The spring (9) works on the body (1) and spring seat (6) and tries to return the push rod (13) to the zero-displacement position irrespective of the output pressure, securing its resetting to the center position.

This also has the effect of a reaction spring to give appropriate control feeling to the operator.

### 3) OPERATION

The operation of the pilot valve will be described on the basis of the hydraulic circuit diagram shown below and the attached operation explanation drawing.

The diagram shown below is the typical application example of the pilot valve.



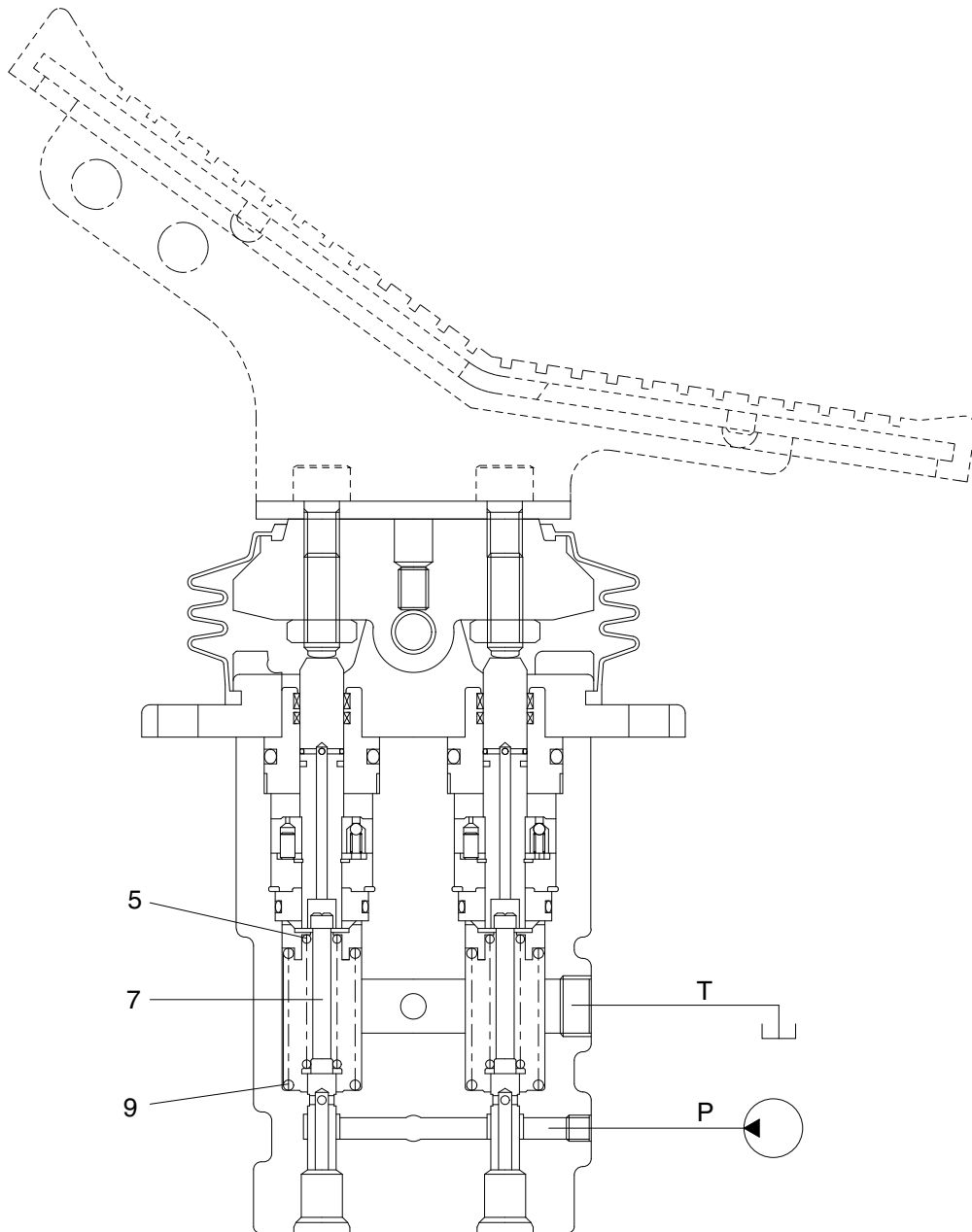
36072SF01

1 Pilot valve  
2 Pilot pump

3 Main pump  
4 Main control valve

5 Hydraulic motor  
6 Hydraulic cylinder

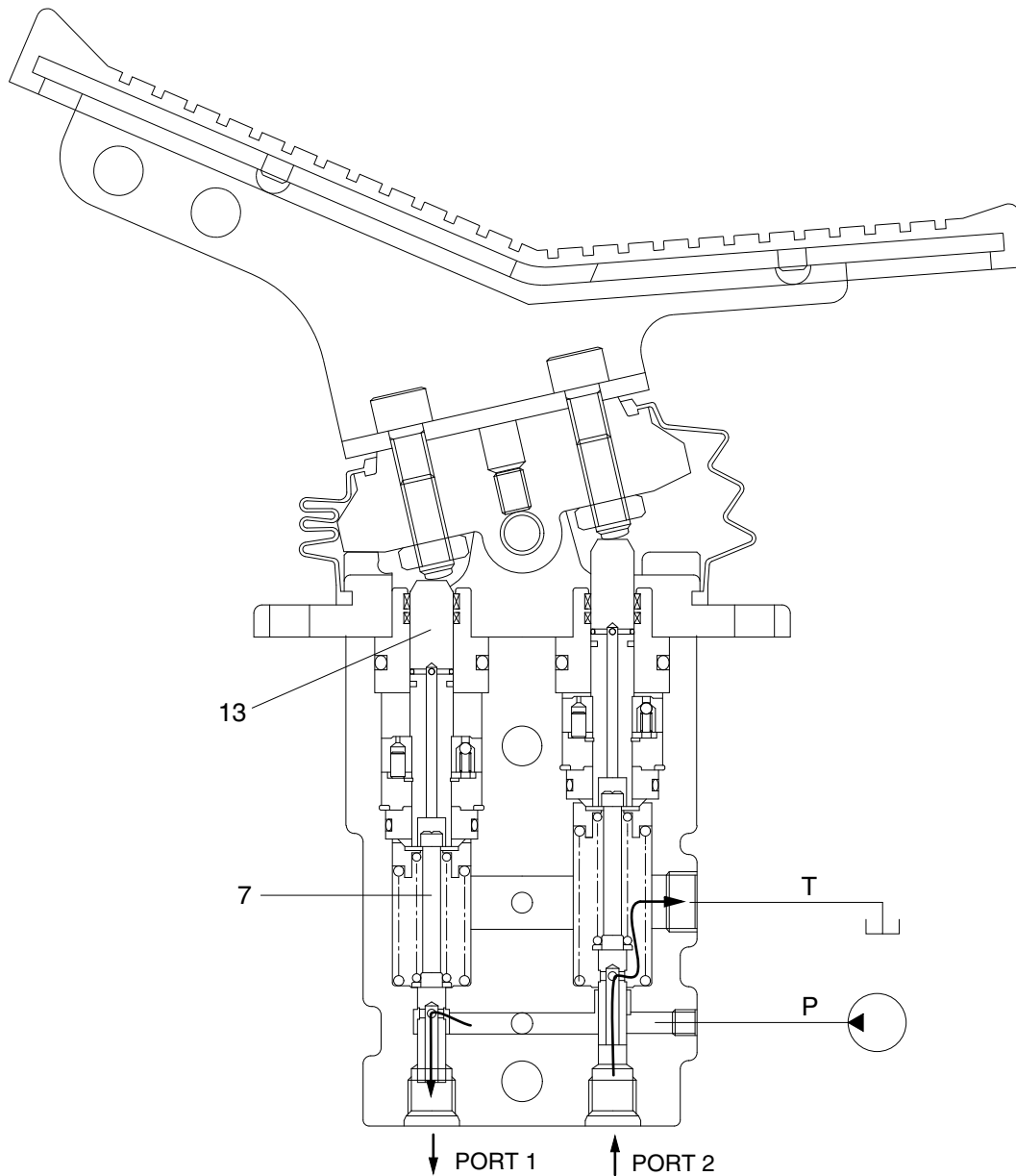
(1) Case where pedal is in neutral position



130ZF2RP03

The force of the spring (5) that determines the output pressure of the pilot valve is not applied to the spool kit (7). Therefore, the spool is pushed up by the spring (9) to the position of 1 and port 2. Then, since the output port is connected to tank port T only, the output port pressure becomes equal to tank pressure.

## (2) Case where pedal is tilted



220F2RP04

When the push rod (13) is stroked, the spool kit (7) moves downwards.

Then port P is connected with port 1, and the oil supplied from the pilot pump flows through port 1 to generate the pressure.

When the pressure at port 1 increases to the value corresponding to the spring force set by tilting the handle, the hydraulic pressure force balances with the spring force. If the pressure at port 1 increases higher than the set pressure, port P is disconnected from port 1 and port T is connected with port 1. If it decreases lower than the set pressure, port P is connected with port 1 and port T is disconnected from port 1.

In this manner the secondary pressure is kept at the constant value.

Besides, in some type, when the handle is tilted more than a certain angle, the upper end of the spool contacts with inside bottom of the push rod and the output pressure is left to be connected with port P.